

FIBERGLASS PIPE GROUP

## Installation of Suspended Bondstrand Pipe

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### **Designing the Bondstrand system**

This guide contains general information for designing suspended Bondstrand piping systems. This information, in conjunction with good general engineering practice and the designer's good judgment, must all be applied to complete a successful and economical piping system.

The guide considers the following:

- Criteria for selecting Bondstrand products for a given application
- Expansion and contraction
- Span between supports and support location
- Connections to other materials and equipment
- Coating Bondstrand products
- Suggested details for guides, supports and anchors

While Bondstrand performs in many applications just like metallic systems, the designer must recognize some important differences:

- Bondstrand pipe weighs only about <sup>1</sup>/<sub>7</sub> as much as Schedule 40 carbon steel pipe. This means that pipe and piping assemblies even in 16-inch diameters can be lifted into place using any light lifting equipment. In the smaller diameters, no lifting equipment is necessary. This reduces on-site installation costs.
- The longitudinal modulus of Bondstrand is much less than that of carbon steel pipe a characteristic that limits spans where deflection is important but also reduces thrust due to temperature change.
- Thermal expansion is 60% greater than for carbon steel. However, by taking advantage of the Bondstrand's flexibility, you can provide for this expansion economically, often without using expansion joints.
- Bondstrand fiberglass pipe requires protection against potential external abrasion or crushing at points where steel supports are located. Such protection is easy and economical.
- Effective modulus values vary with temperature. Recommended spans and estimated thrusts are given to help the designer detail his project for long-time operation at ambient and elevated temperatures.

Recognition of these and other differences dealt with in this guide is the key to successful installations. While this information is likely to prove most helpful to those designing Bondstrand systems for the first time, experienced Bondstrand customers will also find new and useful information.

Be aware that the reinforced thermosetting resin piping products offered by other manufacturers may differ significantly from Bondstrand. Resin systems, manufacturing processes and joining systems are important variables affecting the mechanical and physical properties of these products. The recommendations and suggestions given are based on Ameron's test and field experience and should be applied only to Bondstrand products.

### Selecting Bondstrand pipe, fittings and adhesives

A choice of either epoxy or vinyl ester Bondstrand products is available for different chemical and thermal environments. For information to guide your selection, refer to the Bondstrand Corrosion Guide, FP132. This publication provides recommendations for different chemicals and other fluid materials, including food products, as well as guidance for selecting the appropriate Bondstrand adhesive.

### Filament-wound versus molded products

In smaller pipe sizes, you have a choice between molded and filament-wound fittings. In general, filament-wound fittings should be used in applications where fittings in loops, turns or branches are intended to flex, where temperature changes exceed 100°F in restrained or blocked systems, or where the system is exposed to mechanical vibration or hydraulic surge. Filament wound fittings would be used, also, in systems where a liner is required. Some sizes and types of fittings are not available in both molded and filament-wound styles, so check the Bondstrand Fittings Dimensions, FP282, for availability when making your choice.

### General (cont)

### Energy savings

Remember when selecting pipe diameter that Bondstrand's low frictional values (Hazen-Williams C = 150) will reduce your pumping energy requirements compared to those for carbon steel pipe. In most systems these low frictional values will be maintained for the life of the system.

Note also that the slightly larger inside diameter of Bondstrand pipe compared to Schedule 40 or 80 carbon steel pipe, will further reduce your pumping costs. Handy charts in the Bondstrand engineering guides show the head loss expected for both pipe and fittings.

### Insulated systems

Bondstrand may be insulated in the field. Bondstrand pipe is also available from many pipe insulators with efficient built-in insulation. If you use insulated Bondstrand, be sure to check your support spacings for the operating temperature to accommodate the added weight of the insulation and jacket.

Series 2000M-FP is manufactured with a factory applied, reinforced coating which provides impact resistance and thermal insulation in addition to its fire protection properties. Unless indicated otherwise, values presented in the tables for Series 2000 can be used for Series 2000M-FP.

### Other application information

Where containment is required for your piping system, Ameron can supply Bondstrand II pipe with a variety of joining and performance options.

Ameron has prepared a number of publications with valuable information pertaining to specific types of service, including marine applications, fire protection systems and steam condensate returns. Just call your local Bondstrand distributor or your nearest Ameron sales office, and let us know your application. Give us the temperature, pressure, liquid or gas to be carried, and other pertinent conditions.

In addition, Ameron has computer programs for deflection and stress analysis of Bondstrand systems. For a nominal fee, Ameron Engineering Department will be pleased to utilize one of these programs to analyze your specific systems. Experience shows, however, that such analysis is required only for the more demanding or complicated conditions and that the generalized procedures presented herein will usually suffice.

2 Designing for expansion and contraction

### **General principles**

Suspended pipe generally performs best where it is permitted to move freely. In these systems, anchors serve only to keep the pipe properly positioned between loops and turns. Center the anchor in the run between loops if possible. An anchor should be placed between loops and between loops and turns. Except for the one anchor per run, supports should carry the pipe and maintain the intended drainage slope but should not restrain the pipe against axial movement. At turns, the supports should also permit lateral movement. Supports should not fall directly on fittings.

If the piping system cannot be designed to move freely, see next section on DESIGNING FOR RESTRAINED SYSTEMS.

Pipe changes length in a free system as a result of changes in temperature and pressure. Since both can increase or decrease concurrently, the resulting changes in length must be combined for loop design. Length-change formulas and examples appear in Appendix A, but the following paragraphs will provide all you need for most pipeline designs.



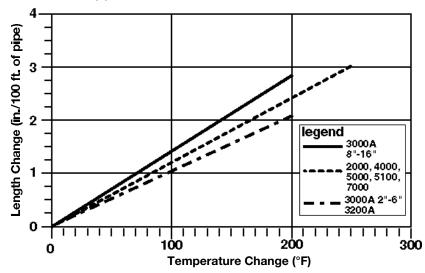
Figure 1

Length changes for Bondstrand Series 2000,

2000M-FP, 4000, 5000, 5100, 7000, 3000A, and 3200A

### Length change due to temperature

Tests show that the amount of linear expansion varies directly with temperature. Figure 1 shows the length change for Series 2000, 3000A, 3200A, 4000, 5000, 5100 and 7000 Bondstrand pipe.



### Length change due to pressure

The amount of length change occurring because of internal pressure depends on wall thickness, diameter, Poisson's ratio and the effective modulus of elasticity in both axial and circumferential directions at the operating temperature. In Bondstrand pipe, some of these factors tend to cancel each other, and the correction becomes relatively simple. For each 100 feet in a straight, freely supported run of Bondstrand pipe (Table 1) provides length changes which are suitable throughout the indicated range of temperatures. You need only correct this value for the pressure of your system by using a direct pressure-ratio correction.

			Inc	hes per	100 fee	t of pipe	(mm per	<sup>.</sup> 100 m d	of pipe) f	rom 100	psi (1 MF	Pa) inter	nal pres	sure	
	ninal neter	Series	s 2000	Series	3000A	Series	3200A	Series	s 4000	Series 5	6000, 5100	Series	s 7000	Series 2	000M-FP
in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	mm	in.	тт	in.	mm
1 1.5 2 3 4 5 6 8 10 12 14 16	25 40 50 80 125 150 200 250 300 350 400	0.1 0.2 0.3 0.4 0.4 0.5 0.7 0.8 0.8 0.8	11 18 23 36 35 44 54 63 80 96 100 100	- 0.2 0.3 0.4 - 0.4 1.3 1.4 1.4 1.5 1.5	- 27 39 49 - 53 158 165 168 176 182	- 0.2 0.3 0.4 - 0.4 0.5 0.6 0.6 0.6 0.6	- 27 39 49 - 53 66 69 70 74 76	$\begin{array}{c} 0.1 \\ 0.2 \\ 0.2 \\ 0.4 \\ 0.3 \\ 0.4 \\ 0.5 \\ 0.6 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.9 \\ 0.9 \end{array}$	14 23 29 46 42 53 64 74 94 112 107 107	0.3 0.5 0.6 1.0 0.9 1.2 1.4 1.6 2.0 2.4 2.3 2.3	37 60 77 122 110 140 170 195 247 295 282 281	$\begin{array}{c} 0.1 \\ 0.2 \\ 0.3 \\ 0.3 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \end{array}$	10 16 20 32 32 40 49 49 49 49 50 50	$\begin{array}{c} 0.1 \\ 0.1 \\ 0.2 \\ 0.3 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \\ 0.4 \end{array}$	11 18 23 36 35 44 54 52 52 52 52 52 52

#### Anchoring for branches and valves

Both vertical and horizontal branches can add complexity to a system intended to move freely. Unless a branch can move both axially and laterally, such as a short stub-out to a nozzle or flexible hose connection, it will require special consideration to avoid undue bending stresses. Sometimes the best solution is to anchor both the branch and the run at the tee, accommodating the pipe length changes at turns or loops in each of the three connecting lines. For example, a vertical branch connecting to buried pipe may include a Z-loop; the tee may be rotated 90° to permit an L-loop; or the vertical line may be treated as a restrained pipe as described in Designing for Restrained Systems.

Valves should be anchored and supported directly, especially in diameters six inches and larger. Valve weight in the larger sizes and torque on valve handles in all sizes are the primary concerns. Generally, butterfly valves with manual lever handle actuators do not require separate supports. Other types of actuators can add too much torque or weight if they are not separately supported.

### Table 1 Length increase due to a 100 psi (7 bar) internal pressure in an unrestrained system.

Values given for Series 2000, 2000M-FP and 4000 are valid to  $250^\circ$ F (121°C). Values for Series 3000A, 3200A, 5000, 5100 and 7000 are valid to  $200^\circ$ F (93°C).

### **Designing for** expansion and contraction (cont'd)

### Using expansion loops

Loops are recommended for relieving longitudinal stress between anchors in a suspended pipeline. Table 2 gives minimum expansion loop dimensions for all Bondstrand pipe series. First, determine how much total length change due to temperature and pressure must be absorbed. Use the appropriate table for the pipe series you are using. Select the pipe diameter and total length change to determine the required leg length for a U-loop design. As an example, assume that a Series 2000 eight-inch line is installed and will change a total of two inches in length. Table 2 for Series 2000 and Series 4000 shows that the length of loop leg required to accommodate the length change is 9 feet (2.8m).

Loops should be horizontal whenever possible to avoid entrapping air or sediment and to facilitate drainage.

- For upward loops, air relief valves aid air removal and improve flow. In pressure systems, air removal for both pressure testing and normal operation is required for safety as well.
- For downward loops, air pressure equalizing lines may be necessary to permit drainage.
- In both cases, special taps are necessary for complete drainage.

Loops using 90° elbows absorb length change better than those using 45° elbows. Unlike a 90° turn, a 45° turn carries a thrust component through the turn which can add axial stress to the usual bending stress in the pipe and fittings. Alignment and deflection are also directly affected by the angular displacement at 45° turns and demand special attention for support design and location.

A 45° elbow at a free turn with the same increment of length change in each leg will be displaced 86% more than a 90° elbow. The relative displacement in the plane of a loop is also more of a problem. Figure 2 illustrates the geometry involved. Design information is not provided because it is beyond the scope of this manual and loops with 45° elbos are generally not recommended. Consult Ameron if a situation requires the use of 45° elbows.

5.0/125

т

1.9 2.2 2.2 2.8 3.1 3.4 3.7 4.0 4.6 4.9 5.2 5.5

2.6a 90° elbow 45° elbow a Relative displacement of elbows permitted to move freely in a pipe run.

				Series	2000	and Ser	ies 40	00 lengt	th cha	nge (in./	mm)
to		ninal	1.	0/25	2.	0/50	3.	0/75	4.0	0/100	5.
	in.	e Size mm	ft	т	ft.	т	ft.	т	ft.	т	ft.
	1 1.5 2 3 4 5 6 8 10 12 14 16	25 40 50 80 100 125 150 200 250 300 350 400	3 3 4 4 5 5 5 6 7 7 8 8	1.0 1.3 1.3 1.6 1.6 1.6 1.9 2.2 2.5 2.5	4 5 6 6 7 8 9 9 10 11 11	1.3 1.6 1.9 2.2 2.5 2.8 2.8 3.1 3.4 3.4	4 5 6 7 8 9 10 12 12 13 14	1.3 1.6 2.2 2.5 2.5 2.8 3.1 3.7 4.0 4.3	5 6 7 8 9 10 10 12 13 14 15 16	1.6 1.9 2.2 2.5 2.8 3.1 3.1 3.7 4.0 4.3 4.6 4.9	6 7 9 10 11 12 13 15 16 7 8

			Series 5000 and 5100 length change (in./mm)           1.0/25         2.0/50         3.0/75         4.0/100         5.0/125														
Nomin		1.	0/25	2.	0/50	3.	0/75	4.0	)/100	5.0	/125						
Pipe Siz	ze nm	ft	2 0.7		т	ft.	т	ft.	т	ft.	т						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	25 40 50 80 25 50 50 50 50 50 50	233444556677	0.7 1.0 1.3 1.3 1.3 1.6 1.6 1.9 2.2 2.2	3 4 4 5 5 6 7 7 8 9 9 10	1.0 1.3 1.6 1.6 1.9 2.2 2.5 2.8 2.8 3.1	4 5 6 7 8 9 10 11 11 12	1.3 1.6 1.9 2.2 2.5 2.8 3.1 3.4 3.4 3.7	4 5 6 7 8 9 10 11 12 13 14	1.3 1.6 1.9 2.2 2.5 2.5 2.8 3.1 3.4 3.7 4.0 4.3	5 6 7 8 9 10 11 13 14 14 15	1.6 1.9 2.2 2.5 2.8 3.1 3.4 4.0 4.3 4.3 4.6						

Figure 2 Comparison of displacement in 90° vs. 45° elbows caused by a unit length change

Table 2 Expansion loop design: Length of loop leg required to accommodate listed length changes

### 2 Designing for expansion and contraction (cont'd)

 
 Table 2
 Expansion loop design: Length of loop leg required to accommodate listed length changes

		5	Series 20	-M000	FP and S	Series	7000 lei	ngth c	hange (	n./ <i>mm</i>	)
	ninal	1.	0/25	2.	0/50	3.	0/75	4.0	)/100	5.0	/125
Pipe in.	e Size mm	ft m 3 1.0		ft.	т	ft.	т	ft.	т	ft.	т
1 2 3 4 5 6 8 10 12 14 16	25 40 50 80 100 125 150 200 250 300 350 400	334455567888	1.0 1.3 1.3 1.6 1.6 1.6 1.9 2.2 2.5 2.5 2.5	4 5 6 7 8 9 10 10 11 12	1.3 1.6 1.9 2.2 2.5 2.8 3.1 3.1 3.4 3.7	4 5 6 7 8 9 10 12 13 13 14	1.3 1.6 1.9 2.2 2.5 2.5 2.8 3.1 3.7 4.0 4.0 4.3	567890 102135516	1.6 1.9 2.2 2.5 2.8 3.1 3.7 4.0 4.6 4.6 4.9	6 7 9 10 11 12 13 15 16 17 18	1.9 2.2 2.8 3.1 3.4 3.7 4.0 4.6 5.2 5.5

				Seri	es 3000/	A leng	th chang	ge (in./	'mm)		
	ninal	1.	0/25	2	.0/50	3.	.0/75	4.0	0/100	5.0	/125
Pipe in.	e Size mm	ft	т	ft.	т	ft.	т	ft.	т	ft.	т
1	25	-	-	-	-	-	-	1	-	-	-
1.5	40	-	-	-	-	-	-	-	_	-	-
2	50	3	1.0	3	1.0	4	1.3	5	1.6	5	1.6
3	80	3	1.0	4	1.3	5	1.6	5	1.6	6	1.9
4	100	3	1.0	5	1.6	5	1.6	6	1.9	7	2.2
5	125	-	-	_		-	-	-	-	-	-
6	150	4	1.3	5	1.6	6	1.9	7	2.2	8	2.5
8	200	4	1.3	6	1.9	7	2.2	8	2.5	9	2.8
10	250	5	1.6	õ	1.9	8	2.5	9	2.8	10	3.1
12	300	5	1.6	7	2.2	8	2.5	9	2.8	10	3.1
14	350	5	1.6	7	2.2	9	2.8	10	3.1	11	3.4
16	400	6	1.9	8	2.5	9	2.8	11	3.4	12	3.7

			Seri	es 3200/	A lengt	h chang	ge (in./	mm)		
Nominal	1.	0/25	2	.0/50	3.	0/75	4.0	)/100	5.0	/125
Pipe Size in. mm	ft <i>m</i>		ft.	т	ft.	т	ft.	т	ft.	т
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	333 - 445566	- 1.0 1.0 1.0 - 1.3 1.3 1.6 1.6 1.9 1.9		- 1.0 1.3 1.6 - 1.6 1.9 2.2 2.2 2.5 2.5		- 1.3 1.6 1.6 - 1.9 2.2 2.5 2.8 2.8 3.1		- 1.6 1.9 - 2.2 2.5 2.8 3.1 3.4 3.4	- 5 6 7 - 8 9 10 11 12 13	- 1.6 1.9 2.2 - 2.5 2.8 3.1 3.4 3.7 4.0

### **Expansion joints**

Instead of a loop, an expansion joint may be used to relieve longitudinal stress. The type selected must be fairly flexible, such as a Teflon bellows which is activated by the thrust of low modulus materials (see Note , Table 3).

Supports for expansion joints must be carefully designed and placed to maintain controlled deflection. Besides adding weight, most of these joints act as partial structural hinges which afford only limited transfer of moment and shear. Where the expansion joint relies on elastomers or thermoplastics for strength, the structural discontinuity or hinging effect at the joint increases with increases in temperature.

When using an expansion joint in a pipeline carrying solids, consider the possibility that it may stiffen or fail to function due to sedimentation in the expansion joint. Failure of the expansion joint may cause excessive pipe deflection.

### **3** Designing for restrained systems

Caution: In restrained systems, pipe fittings can be damaged by faulty anchoring or by untimely release of anchors. Damage to fittings in service can be caused by bending or slipping of an improperly designed or installed anchor. Also, length changes due to creep are induced by high pressures or temperatures while pipe is in service. When anchors must later be released, especially in long pipe runs, temporary anchors may be required to avoid excessive displacement and overstress of fittings.

### **General principles**

The layout of a system occasionally makes it impossible to allow the pipe to "move freely." Sometimes it may be necessary to block certain runs of an otherwise free system. In a fully restrained pipe (blocked against movement at both ends), the designer must deal with thrust rather than length change. Both temperature and pressure produce thrust which must be resisted at turns, branches, reducers and ends. Knowing the magnitude of this thrust enables the designer to select satisfactory anchors . Remember that axial thrust on anchors is independent of anchor spacing. Formulas and examples are found in Appendix B.

In practice, the largest compressive thrust is normally developed on the first positive temperature cycle. Subsequently, the pipe develops both compressive and tensile loads as it is subjected to temperature and pressure cycles. Neither compressive nor tensile loads, however, are expected to exceed the thrust on the first cycle unless the ranges of the temperature and pressure change.

### Thrust due to temperature

In a fully restrained Bondstrand pipe, length changes induced by temperature change are resisted at the anchors and converted to thrust. The thrust developed depends on the thermal coefficient of expansion, the cross-sectional area, the modulus of elasticity and the temperature change, t. Table 3 gives the maximum axial thrust in anchored lines for each series of Bondstrand pipe at three elevated temperatures. The table assumes a fully relaxed initial pipe length at 60°F, with short-time modulus of elasticity values as shown.

Table 3 Initial temperature-induced thrusts (pounds-force) in fully restrained Bondstrand pipe at various operating temperatures

		Initial Te	mperature	e Induced	Thrusts (p	oounds-for	e) in a Fully R	estrained Bon	dstrand F	Pipe at Va	arious Oper	ating Tem	peratures	S
Nominal Diameter	S	eries 200	0	Series 200	0M-FP &	Series 7000	Series 3000A	Series 3200A	S	Series 400	0	Seri	es 5000 8	§ 5100
in. mm	m 150°F 200°F 250°F 150°F 200°F 250°F				200°F	200°F	150°F	200°F	250°F	140°F	170°F	200°F		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	880 1300 1610 2390 3980 4940 5920 8600 10760 12780 14770 19090	1070 1560 1940 2890 4800 5950 7130 10370 12970 15410 17810 23020	1210 1780 2200 3290 5470 6780 8120 11800 14760 17540 20270 26200	880 1300 1610 2390 3980 4940 5920 10430 16250 22850 26450 34590	1070 1560 1940 2890 4800 5950 7130 12570 12570 27540 31880 41700	1210 1780 2200 3290 5470 6780 8120 14310 22300 31350 36290 47470	- 1850 2890 3800 - 7420 8160 12030 16350 20060 25140	- 1850 2890 3800 - 7420 10000 14750 20040 24600 30820	730 1060 1310 1950 3410 4220 5060 7480 9340 11100 13880 18000	880 1280 1580 2350 4110 5090 6100 9010 11260 13380 16730 21700	1000 1460 1800 2670 4680 5800 6940 10260 12820 15230 19040 24700	490 710 870 1300 2270 2820 3370 4980 6230 7400 9250 12000	560 810 1490 2610 3230 3860 5710 7140 8480 10600 13750	370 540 660 980 2140 2560 3780 4720 5610 7020 9100

		Initial	Temperat	ure Induce	d Thrust	s (Newtons)	in a Fully Res	trained Bonds	trand Pip	e at Vari	ous Operati	ng Tempe	ratures	
Nomina Diamete		Series 200	00	Series 20	00M-FP &	Series 7000	Series 3000A	Series 3200A	S	eries 400	00	Seri	es 5000 8	§ 5100
in. mn	0500	93°C	121°C	65°C	93°C	121°C	93°C	93°C	65°C	93°C	121°C	60°C	77°C	93°C
1 25 1.5 40 2 50 3 80 4 100 5 125 6 150 8 200 10 255 12 300 14 350 16 400	5710           7070           10540           17540           21740           26050           37880           47360           56280           56280           65040	4720 6930 8580 12800 26390 31610 57480 68310 78940 102030	5390 7910 9800 14610 24300 30130 36090 52480 65610 77980 90110 116470	3890 5710 7070 10540 21740 26050 45900 71570 100590 116440 152320	4720 6930 8580 21290 26390 31610 55710 86860 122080 141320 184850	5390 7910 9800 14610 24300 30130 36090 63600 99150 139370 161330 211030	- 8200 12790 16860 - 32910 36170 53360 72510 89000 111520	- 8200 12790 16860 - 32910 44330 65390 88870 109080 136670	3210 4680 5780 8580 15020 18600 22260 32920 41130 48860 61110 79250	3900 5680 7010 10410 18230 22570 27020 39950 49920 59300 74160 96180	4450 6490 8000 11880 20820 25770 30840 45610 56990 67690 84660 109800	2170 3160 3900 5790 10140 12550 15020 22220 27760 32970 41240 53480	2500 3640 4490 6670 11680 14460 17300 25590 31970 37980 47490 61590	1640 2390 2940 4370 7660 9480 11340 16780 20960 24900 31140 40380

Note: in tables above, thrusts are calculated assuming a fully relaxed initial length at 60°F (16°C) and short term modulus of elasticity values as follows. For 2 - 6 inch Series 3000A, use modulus of elasticity values from Series 3200A.

Coefficient of thermal expansion is 10 x 10<sup>-6</sup> in./in./°F (18 x 10<sup>-6</sup> mm/mm/°C) for all but Series 3000A and 3200A which are 8.5 x 10<sup>-6</sup> in./in./°F (15.3 x 10<sup>-6</sup> mm/mm/°C) for 2 - 6 inch Series 3000A and all Series 3200A sizes, and 12 x 10<sup>-6</sup> in./in./°F (21.6 x 10<sup>-6</sup> mm/mm/°C) for 8 - 16 inch Series 3000A.

							Modulus o	f Elasticity						
	Series 2000			Series 2000N	И-FP & Se	eries 7000	Series 3000A	Series 3200A	Se	ries 4000		Series	5000 &	5100
10 <sup>6</sup> psi	1.6	1.2	1.0	1.6	1.2	1.0	1.3	2.3	1.6	1.2	1.0	1.2	1.0	0.5
GPa	11.03	8.55	7.17	11.03	8.55	7.17	8.97	15.52	11.03	8.55	7.17	8.28	6.90	3.59

# **3** Designing for restrained systems (cont'd.)

### Thrust due to pressure

Thrust due to internal pressure in a suspended but restrained system is theoretically more complicated. This is because in straight, restrained pipelines with all joints bonded, the Poisson effect produces considerable tension in the pipe wall. As internal pressure is applied, the pipe expands circumferentially and at the same time contracts longitudinally. This tensile force is important because it acts to reduce the hydrostatic thrust on anchors at turns.

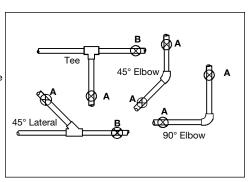
For the designer of a restrained Bondstrand pipeline, however, the problem can be greatly simplified. Table 4 provides the recommended design thrusts and locations for anchors at various fittings.

#### Table 4 Thrust at anchors due to 100 psi (690 kPa) internal pressure in restrained Bondstrand systems

T	hrust at	Anchors Due to	o <b>100 psi (</b> 690 k	Pa) Internal Pre	ssure in Restra	ined Bondstrar	d Systems
	ninal	Series 200	00/4000/7000	Series 50	000/5100	Series 30	00A/3200A
Pipe in.	e Size mm	lb-force	Ν	lb-force	Ν	lb-force	Ν
1	25	50	225	45	170	-	-
1.5	40	115	515	115	440	-	-
2	50	180	810	190	725	240	1060
3	80	420	1865	460	1755	540	2400
4	100	695	3085	755	2900	915	4070
5	125	1080	4805	1200	4605	-	-
6	150	1565	6955	1765	6760	2000	8895
8	200	2680	11925	3035	11710	4045	11995
10	250	4220	18780	4830	18645	6365	28320
12	300	5990	26645	6890	26640	8890	39545
14	350	7215	32100	8305	32105	11535	51320
16	400	9425	41935	10855	41965	15070	67035

Notes:

- 1. Pipe anchors (A) such as shown in figure 8, Section 8 are used in restrained systems at each end of a run and just before a change in direction, and must resist the tabulated thrusts.
- Pipe anchors (B) such as shown in figure 7, Section 8 are light-duty in-line anchors usually located between two pipe anchors (A) or midway between loops or turns in systems not restrained.
- Pipe anchors (A and B) at elbows and branches should be located a distance of five to ten times the pipe diameter from the bend. Other anchor locations may require a flexibility analysis.
- No appreciable thrust on anchors is developed due to internal pressure in the pipe at in-line reducers.



### Using guides for alignment control

A suspended line which is restrained from movement may need extra supports or guides to maintain alignment, especially when the pipeline is exposed to a wide temperature range. Guides as shown in Figure 6 may permit the pipe to move axially but not laterally. Without guides, restrained pipe may not deflect uniformly and, in some cases, may deflect excessively. Tables 5 to 9 (Tables 10 to 14 for metric) give recommended guide spacing to avoid buckling deflection between anchors.

Supplying this lateral support by using guides at the normal support locations or even at every other support is often sufficient, especially in the larger diameters. To check, compare the recommended span for your operating temperature as determined from the section entitled SUPPORT LOCATIONS AND SPANS with the guide spacings from Tables 5 to 9 (Tables 10 to 14, metric). Be sure that guide and support spacing meet both requirements.

As an example for determining guide spacing, assume that a three-inch Bondstrand Series 2000 line is installed at 70°F and is to operate at 250°F (T = 180°F). Table 5 shows that guides should be installed at intervals of 7 feet.

### **Designing for** restrained systems (cont'd.)

Table 5

Maximum guide spacing (ft.) required for temperature change	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$																			
(°F) Bondstrand Series 2000 & 4000		-	0 2	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190
Bondstrand Series 2000 & 4000	2       50       19       14       11       10       9       8       7       7       6       6       6       5       7 <th>4 7 9 11 13 17 21 25 28</th>													4 7 9 11 13 17 21 25 28						
Maximum guide spacing (ft.) required for temperature change	Degrees of formpolations of ango (1)																			
(°F)	in. <i>n</i>	1 1	0 2	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190
Bondstrand Series 5000 & 5100	1.5 4 2 5 3 8	0 1 0 2 0 2 0 3 0 5 0 5 0 7 0 7 0 10 0 10 0 11	5 1 <sup>1</sup> 9 13 8 20 6 20 5 33 4 30 1 50 9 65 75 6 82	9 3 11 16 21 2 26 3 31 2 41 3 51 6 61 2 67	8 9	7 8	6 8	6 7	5 7	5 6	5 6	5 6	4 5	4 5	4 5	4	4	4 5	4 4	3 4

### Table 6 Maximum guide spacing (ft.) required for temperature cha (°F)

Table 7	Maximum guide spacing (ft.) required for temperature change (°F)
	Bondstrand Series 2000M-FP & 7000

Nominal Pipe Size						[	Degre	es of	Tem	perat	ure C	hang	e (°F)						
in. <i>mm</i>	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190
$\begin{array}{ccccccc} 1 & 25 \\ 1.5 & 40 \\ 2 & 50 \\ 3 & 80 \\ 4 & 100 \\ 5 & 125 \\ 6 & 150 \\ 8 & 200 \\ 10 & 250 \\ 12 & 300 \\ 12 & 300 \\ 14 & 350 \\ 16 & 400 \end{array}$	11 16 20 31 40 47 59 79 99 119 128 146	8 12 14 22 8 33 42 56 70 84 91 104	6 9 12 23 27 34 57 69 74 85	6 8 10 23 20 39 50 59 64 73	5 7 9 14 18 27 35 44 53 57 65	57 8 13 16 19 24 32 41 49 52 60	4 6 8 12 15 18 20 38 45 48 55	4 7 11 14 17 21 28 35 42 52	4 5 7 10 13 16 20 26 33 40 43 49	3 5 10 13 15 19 25 31 38 40 46	3 5 9 12 14 18 24 30 36 39 44	3 5 9 11 14 17 23 34 37 42	3 5 6 8 11 13 16 22 83 36 41	3 4 5 8 11 13 16 21 27 32 34 39	3 4 5 8 10 12 15 20 31 33 38	3 4 5 8 10 12 15 20 32 37	3 4 5 7 10 11 14 29 31 36	3 4 5 7 9 11 19 23 28 30 35	34 57 91 14 18 23 27 34

Maximum guide spacing (ft.) required for temperature change (°F) Table 8 **Bondstrand Series 3000A** 

Nominal Pipe Size						[	Degre	es of	Tem	perat	ure C	hang	e (°F)						
in. <i>mm</i>	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 21 31 40 59 64 81 96 109 125	- 15 22 28 - 42 45 57 68 77 88	- 12 18 23 - 34 37 47 55 63 72	- 10 15 20 30 32 40 48 55 62	- 9 14 26 29 36 43 49 56	- 8 12 16 24 26 33 39 45 51	- 8 12 15 - 22 24 30 36 41 47	- 7 11 23 28 34 39 44	- 7 10 13 - 20 21 27 32 36 42	- 6 10 13 - 19 20 25 30 34 39	- 6 9 12 - 18 19 24 29 33 38	- 6 9 11 - 17 18 23 28 31 36	- 6 8 11 - 16 18 22 27 30 35	- 5 8 11 - 16 17 22 26 29 33	- 5 8 10 - 15 16 21 25 28 32	- 5 8 10 - 15 16 20 24 27 31	- 5 7 10 - 14 15 20 23 26 30	- 5 79 14 15 20 29	579-14151822529

Table 9 Maximum guide spacing (ft.) required for temperature change (°F) **Bondstrand Series 3200A** 

Nominal Pipe Size						[	Degre	es of	Tem	perat	ure C	hang	e (°F)						
in. <i>mm</i>	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180	190
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 21 31 40 - 59 76 96 114 130 148	- 15 22 42 54 80 92 105	- 12 18 23 - 34 45 66 75 86	- 10 15 20 30 38 48 57 65 74	- 9 14 18 26 34 51 58 66	- 8 12 16 24 39 46 53 61	- 8 12 15 22 29 36 49 56	- 7 11 21 27 34 40 52	- 7 10 13 20 25 32 38 43 49	- 6 10 13 - 19 24 30 36 41 47	- 9 12 18 23 29 34 39 45	- 9 11 17 22 33 37 43	- 6 8 11 16 21 27 32 36 41	- 5 8 11 16 20 26 30 35 40		- 5 8 10 - 15 19 24 28 32 37	- 5 7 10 - 14 18 23 28 31 36	- 5 7 9 14 18 23 27 31 35	- 5 7 9 14 17 22 30 34

### Designing for restrained systems (cont'd.) B

Table 10	Maximum guide spacing (m) required for temperature change	Nomina Pipe Si						[	Degre	es of	Temp	oerati	ure Cl	hange	e (°C)						
	(°C) Bondstrand Series 2000 & 4000	in. <i>n</i>	nm g	5 10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	95
		1.5 4 2 5	25       15.0         50       18.0         50       23.1         50       29.1         50       35.1         50       38.1	3.5 4.2 6.5 8.5 10.5	3.5 5.2 7.0 8.5 10.2 13.5 17.0 20.2 22.2	14.8 17.5 19.2	17.2	2.5 3.8 4.8 6.0 7.2 9.5 12.0 14.2 15.8	14.5	13.5	1.0 1.5 2.0 3.0 4.0 5.0 6.0 7.8 9.8 11.8 12.8 14.8	12.0	11.5	0.8 1.2 1.8 2.5 3.5 4.2 5.0 6.8 8.5 10.0 11.0 12.8	6.5 8.0 9.8 10.5	0.8 1.2 2.5 3.0 4.0 4.8 6.2 7.8 9.2 10.2 11.8	0.8 1.2 2.2 3.0 3.8 4.5 6.0 7.5 9.0 9.8 11.2	0.8 1.2 2.2 3.0 3.8 4.5 5.8 7.2 8.8 9.5 11.0	0.8 1.0 2.2 3.5 4.2 5.5 7.0 8.5 9.2 10.8	0.8 1.0 2.8 3.5 4.2 5.5 6.8 8.2 9.0 10.2	0. 1. 2. 2. 3. 4. 5. 6. 8. 8. 10.
Table 11	Maximum guide spacing (m) required for temperature change	Nomina Pipe Si						[	Degre	es of	Tem	perat	ure C	hang	e (°C)	)					
	(°C)			5 10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	9
	Bondstrand Series 5000 & 5100	1.5 4	25 14. 50 17. 50 22. 50 28. 50 33. 50 37.	8 3.2 0 4.2 0 6.2	2.8 3.5 5.0 6.8 8.2 10.0 13.0 16.2 19.5 21.5	2.2 3.0 4.5 5.8 7.2 8.5 11.2 14.2 16.8 18.5	2.5 4.0 5.0 6.5 7.8 10.0 12.8 15.0 16.5	2.2 3.5 4.8 5.8 7.0 9.2 11.5 13.8 15.2	2.2 3.2 5.5 6.5 10.8 12.8 14.0	13.0	2.0 3.8 4.8 5.8 7.5 9.5 11.2 12.2	1.0 1.5 2.8 3.5 5.5 9.0 10.5 11.8 13.5	0.8 1.2 2.5 3.5 4.2 5.2 6.8 8.5 10.0 11.2 12.8	1.2 1.8 2.5 3.2 4.0 5.0 6.5 8.0 9.8 10.8	6.2 7.8 9.2 10.2	0.8 1.2 1.5 2.2 3.0 3.8 4.5 6.0 7.5 9.0 9.8 11.2	3.8 4.5 5.8 7.2 8.8 9.5	0.8 1.0 2.2 2.8 3.5 4.2 5.5 7.0 8.2 9.2 10.5	3.5 4.0 5.5 6.8 8.0	1.0 1.2 2.0 2.8 3.2 4.0 5.2 6.5 8.0 8.8	1 1 2 2 3 4 5 6 7 8
Table 12	Maximum guide spacing (m) required for temperature change	Nomina Pipe Si		<u> </u>					Degre	es of	Tem	oerati	ure Cl	hange	e (°C)	•				•	
	(°C) Bondstrand Series 2000M-FP &		nm 5	i 10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	ç
	7000	1.5 4	25       15.0         50       19.0         50       25.1         50       31.0         50       38.0         50       41.0	2 3.5 5 4.5 8 6.8 9 9.0 0 10.5 0 13.2	3.0 3.8 5.5 7.2 8.5 11.0 14.5 18.2 22.0 23.8	20.5	14.2 17.0 18.2	2.5 4.0 5.0 7.8 10.2 13.0 15.5 16.8	15.5	4.5 5.2 6.5 8.8 11.2 13.5 14.5	4.2 5.0 6.2 8.2 10.5 12.5 13.5	4.0 4.8 6.0 7.8 10.0 12.0 13.0	3.8 4.5 5.5 7.5 9.5 11.5 12.2	1.8 2.8 3.5 4.2 5.5 7.2 9.0 11.0 11.8	3.5 4.0 5.2 7.0 8.8 10.5 11.2	11.0	1.5 2.2 3.8 4.8 6.5 8.0 9.8 10.5	10.2	0.8 1.2 2.2 3.0 3.5 6.0 7.5 9.2 9.8 11.2	3.5 4.2 5.8 7.5 9.0 9.5	1122345780
Table 13	Maximum guide spacing (m)	Nomina	al					[	Degre	es of	Tem	oerati	ure Cl	hange	e (°C)						
	required for temperature change (°C)	Pipe Si in. n		10	15	20	25	30	35	40	45	50	55	60	65	70	75	80	85	90	ç
	Bondstrand Series 3000A		25 -	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		2 5 3 8 4 10 5 12 6 15 8 20 10 25 12 30 14 35	25 – 50 19.0 50 20.5 50 25.8 50 30.5 50 35.0	6.8 9.0 - 13.2	5.5 7.2 - 10.8 11.8 14.8 17.5 20.0	10.2 12.8 15.2 17.5	- 2.8 4.2 5.5 - 8.5 9.0 11.5 13.5 15.5	10.5 12.5 14.2	- 2.2 3.5 4.8 - 7.0 7.8 9.8 11.5 13.0	- 2.2 3.2 4.5 - 6.5 7.2 9.0 10.8 12.2	- 2.0 3.2 4.0 - 6.2 6.8 8.5 10.0 11.5	- 2.0 3.0 4.0 - 6.0 6.2 8.0 9.5 11.0	- 1.8 2.8 3.8 - 5.5 6.0 7.8 9.2 10.5	- 1.8 2.8 3.5 - 5.2 5.8 7.2 8.8 10.0	- 1.8 2.5 3.5 - 5.2 5.5 7.0 8.5 9.5	- 1.8 2.5 3.2 - 5.0 5.2 6.8 8.0 9.2	- 1.5 2.5 3.2 - 4.8 5.2 6.5 7.8 9.0	- 1.5 2.2 3.0 - 4.8 5.0 6.2 7.5 8.8	- 1.5 2.2 3.0 - 4.5 4.8 6.2 7.2 8.2 9.5	- 1.5 2.2 3.0 - 4.2 4.8 6.0 7.0 8.2 9.2	
Table 14	Maximum guide spacing (m)	16 40		20.2	23.0	20.0	11.0			es of							10.2	10.0	9.0	3.2	_
	required for temperature change (°C)	Pipe Si		10	15	20	25	-	35	40	45	50	55	60	65	70	75	80	85	90	ę
	Bondstrand Series 3200A	1.5 4 2 5 3 8	25 – 40 – 50 6.3	- - 4.5 8 6.8	- - 3.8 5.5	- - 3.2 4.8	- 2.8 4.2	- - 2.5 4.0	- - 2.2 3.5	- 2.2 3.2	- 2.0 3.2	- 2.0 3.0	- - 1.8 2.8	- - 1.8 2.8	- - 1.8 2.5	- - 1.8 2.5	- - 1.5 2.5	- - 1.5 2.2	- - 1.5 2.2	- - 1.5 2.2	
		4 10 5 12 6 15 8 20 10 25 12 30 14 35 16 40	25 – 50 19.0 50 24.2 50 30.8 50 36.8	- ) 13.2	- 10.8 14.0 17.8 21.0	12.0 15.2 18.2	- 8.5 10.8 13.8 16.2	- 7.8 9.8 12.5 14.8	4.8 - 9.0 11.5 13.8 15.5 18.0	4.5 - 8.5 10.8 12.8 14.5 16.8	12.0	4.0 - 7.5 9.5 11.5 13.0 15.0	3.8 - 5.5 9.2 11.0 12.5 14.2	- 5.2 7.0 8.8 10.5	3.5 - 5.2 6.8 8.5 10.0 11.5 13.0	- 5.0 6.5 8.0 9.8	- 4.8 6.2 7.8 9.2	3.0 - 4.8 6.0 7.5 9.0 10.2 11.8	3.0 - 5.8 7.2 8.8 10.0 11.5	3.0 - 4.2 5.8 7.2 8.5 9.8 11.0	10

Spans and support locations

### Span recommendations

Recommended maximum spans for Bondstrand pipe at various operating temperatures are given in Table 15. These spans are intended for normal horizontal piping arrangements, i.e., those which have no fittings, valves, vertical runs, etc., but which may include flanges and non-uniform support spacings. The tabular values represent a compromise between continuous and simple spans. When installed at the support spacings indicated in Table 15, the weight of the pipe full of water will produce a long-time deflection of about ½ inch, which is usually acceptable for appearance and adequate drainage.

Fully continuous spans may be used with support spacings up to 20 percent greater than those shown in Table 15; in simple spans, support spacings should be 20 percent less than those shown in Table 15.

For this purpose, continuous spans are defined as interior spans (not end spans), which are uniform in length and free from structural rotation at supports. Simple spans are supported only at the ends and are hinged or free to rotate at the supports. Special conditions described below are not covered.

The pipe is assumed to be free to move axially. Suspended piping, which is restrained or anchored against longitudinal movement, represents a special case and guides may be required as discussed under the previous section, Use of Guides for Alignment.

Series 2000 Series 2000M-FP Series 4000 Series 5000 151°F to 67°C to 151°F to 67°C to 151°F to 67°C to up to 151°F to 67°C to up to Nominal Pipe Size 150°F 66°C 250°F 121°C 150°F 66°C 250°F 121°C 150°F 66°C 250°F 121°C 150°F 66°C 200°F 93°C ft m ft. т ft т ft. m ft. т ft m ft m ft. т in. mm 25 10.2 3.1 8.9 2.7 8.7 2.7 7.6 2.3 9.7 3.0 8.7 2.7 9.4 2.9 5.6 1.7 1 1.9 2.0 2.3 2.9 3.1 3.6 3.2 3.4 3.8 6.2 6.6 7.5 1.5 40 11.4 3.5 3.7 4.2 10.0 3.0 10.4 9.1 2.8 3.0 10.8 3.3 3.5 4.0 10.4 3.2 9.7 50 80 12.2 13.9 10.7 12.2 3.2 3.7 3.4 3.9 10.3 11.7 11.0 12.5 2 3 11 1 9.7 11.5 11.3 3.4 13.1 12.9 100 125 150 4.8 5.1 5.4 4.2 4.5 4.7 4.6 4.9 5.2 4.1 4.4 4.6 8.6 9.3 9.7 2.6 2.8 3.0 4.5 4.9 4.0 4.3 15.2 16.1 17.0 13.6 14.4 15.2 4.4 4.7 4 5 6 8 10 12 14 16 14.9 14.4 15.8 13.8 13.0 16.8 17.7 14.7 15.9 14.0 15.5 16.2 15.5 16.9 5.2 14.8 4.5 4.9 18.9 20.1 21.0 22.3 23.8 200 250 300 6.0 6.4 6.7 5.2 5.6 5.8 6.0 6.8 7.5 5.8 6.1 6.4 5.1 5.5 5.7 18.0 19.2 20.1 5.5 5.8 6.1 10.8 11.5 12.0 3.3 3.5 3.7 19.6 20.8 17.2 18.2 5.3 6.0 16.9 17.9 19.8 17.3 22.3 19.5 21.8 24.5 21.5 6.5 18.8 19.1 350 400 22.7 24.2 6.9 7.4 19.9 21.2 6.1 6.5 25.5 27.2 7.8 22.3 23.8 6.8 7.3 6.8 7.3 19.9 21.3 6.1 6.5 21.3 22.7 6.5 6.9 12.8 13.6 3.9 4.2

		Series	s 5100			Series	7000			Serie	s 3000A			Serie	s 3200A	1
Nominal Pipe Size	up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 99°C	up to 150°F	up to 66°C	151°F to 210°F	67°C to 99°C
in. <i>mm</i>	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 8.1\\ 9.0\\ 9.5\\ 10.8\\ 12.4\\ 13.4\\ 14.0\\ 15.6\\ 16.6\\ 17.4\\ 18.4\\ 19.6\end{array}$	2.5 2.7 2.9 3.3 3.8 4.1 4.3 4.7 5.1 5.3 5.6 6.0	5.6 6.2 6.6 9.3 9.7 10.8 11.5 12.0 12.8 13.6	1.7 1.9 2.3 6 2.8 3.0 3.5 3.5 3.7 3.9 4.2	10.1 11.4 12.4 14.3 16.2 17.2 20.8 23.3 25.3 26.2 28.0	3.1 3.5 3.8 4.4 4.9 5.2 5.5 6.4 7.1 7.7 8.0 8.5	8.9 9.9 10.8 12.5 14.2 15.1 15.9 18.3 20.4 22.2 23.0 24.6	2.7 3.3 3.8 4.3 4.6 4.8 5.6 6.2 6.8 7.0 7.5	- 12.8 14.5 15.6 - 18.7 16.8 18.6 20.2 21.3 22.6	- 3.9 4.4 4.8 - 5.7 5.7 5.7 6.2 6.5 6.9	- 11.9 13.5 14.6 17.4 15.7 17.3 18.8 19.8 21.0	- 3.6 4.1 5.3 4.8 5.3 5.7 6.0 6.4	- 12.8 14.5 15.6 - 18.7 20.0 22.2 24.0 25.3 26.8	- 3.9 4.4 4.8 - 5.7 6.1 6.8 7.3 7.7 8.2	- 11.9 13.5 14.6 - 17.4 18.6 20.6 22.3 23.6 25.0	- 3.6 4.1 5.3 5.7 6.8 7.6

### Support spacings for special conditions

Piping designers may calculate deflections or determine support spacings for their own particular geometry and loadings using the effective beam stiffness factors given in Appendix C. In such an analysis, the effects of non-uniform spacing, turns and branches, vertical or inclined runs, special joints which may act as a hinge, heavy liquids, external loads such as insulation, thrust in restrained lines and dynamic loads may be considered, often using a computer program.

Table 15 Recommended maximum support spacings in feet for Bondstrand pipe at various operating temperatures (fluid specific gravity=1.0)

### Spans and support locations (cont'd)

Table 16 Permissible service loads as limited by hanger and support details, horizontal piping

### Loads on hangers and supports

Table 16 gives maximum service loads for horizontal piping on hangers and supports. Do not exceed the total support or hanger load given in the table for sustained operation.

Nominal Diameter in. mm	Load on Support Fitter Maximum per linear inch	( )
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	100 100 100 100 100 100 130 200 340 400 650 800	100 120 160 200 200 330 600 1050 1430 1720 2320

### **Support locations**

Supports that permit pipe movement are usually under pipe, not under fittings. Be sure that pipe movement is not obstructed either axially or laterally by a flange or fitting near the support. In general, supports may be located at convenient nearby structures, just as for steel pipe, provided the support spacings indicated in Table 15 are not exceeded.

Anchors on pipe are indicated in Table 4 for restrained piping. Except at flanged connections, above-ground anchors are usually found on pipe rather than fittings. Anchors in lines free to move should be located where necessary to control movement into loops or turns. See Figures 7 through 10 for typical anchor details.

### Supports for vertical runs

Install a single support anywhere along the length of a vertical pipe run more than about ten feet long. See Figure 10 for suggested details. If the run is supported near its base, use loose collars as guides as shown in Figure 10b, spaced as recommended in Table 17.

Series	Pipe Diameter		Fluid Tem	oerature (°I	=)
	Inches	100	150	200	250
2000	1, 1.5	20	15	10	10
<b>}</b>	2, 3, 4, 5	25	20	15	10
4000 J	6, 8, 10, 12, 14, 16	30	25	20	15
3000A l	2, 3, 4, 6,	25	20	15	†
3200A J	8, 10, 12, 14, 16	35	30	25	†
ר 5000	1, 1.5	20	15	10	+
5100 }	2, 3, 4, 5	25	20	10	÷
	6, 8, 10, 12, 14, 16	30	25	15	t

† not recommended Vertical runs less

than ten feet long may usually be supported as part of the horizontal piping. In either case be sure the layout makes sufficient provision for horizontal and vertical movement at the top and bottom turns.

Accommodate length changes in vertical pipe runs by allowing free movement of fittings at either top, bottom or both. For each  $\frac{1}{8}$  inch of anticipated vertical length change, provide 2 feet of horizontal pipe between the elbow and the first support, but not less than 6 feet nor more than 20 feet of horizontal pipe.

Treat columns more than 100 feet high (either hanging or standing) as special designs. Support and provision for length change are important. The installer should be especially careful to avoid movement due to wind or support vibration while joints are curing.

#### Table 17 Minimum guide spacing (feet) for vertical runs supported from the bottom

Connect	tions to	Connections to other piping
<b>O</b> other ma	aterials	Where possible, connect Bondstrand to either metallic or thermoplastic piping using flanges drilled to the 150 psi standards of ANSI B16.5. Bondstrand filament-wound epoxy flanges and Bondstrand heavy-duty molded flanges may be bolted directly against raised-face steel flanges These flanges also seal well against lined stee configurations. All flanges, including Bondstrand standard molded flanges, epoxy and vinyl ester, provide sealing against flat-faced flanges. Use a full-faced 1/8-including thick elastomer with a Shore A hardness of 60 ±5 for best results.
		Flanged valves and other equipment are frequently supplied with different flange facings. The configuration of these facings may vary widely. Unless it has been demonstrated that these facings are compatible with the face of Bondstrand flanges, consult Ameron Fiberglass Pipe Group Engineering Department.
		Where Bondstrand is connected to metallic pipe, securely anchor the metallic pipe at the point of connection so that expansion and contraction or weight of the meta line is not transferred to the Bondstrand line.
		Small-diameter metallic connections
		Outlets for instrumentation are best made using orifice flanges with ½-inch orifices Threaded reducer bushings mounted in saddles, blind flanges and fittings plugs offer connections up to 1½-inches in diameter for a wide range of applications. The most commonly used metal bushing material is Type 316 stainless steel, bu Ameron can furnish other materials on special order.
		Gravity flow connections
		There are different ways to make gravity-flow connections to floor drains, cast iror pipe, etc. For example, a four-inch by six-inch tapered body reducer will enlarge the receiving end of a Bondstrand four-inch pipe and serve as a packing chamber fo the cast iron end of a floor drain or other fitting.
		Conversely, Bondstrand pipe can be packed and sealed into a cast iron bell. In any case, avoid packing materials which must be applied at temperatures above 200°F Mechanical couplings are available through other manufacturers to connec Bondstrand to clay, concrete, cast iron or other non-metallic pipe.
Connect		Equipment vibration
O equipme	ent	Bondstrand pipe will safely absorb vibration from pumping or other conditions if (1 stresses are controlled within reasonable limits, and (2) pipe is protected from external abrasion by saddles or sleeves where it contacts supports and othe objects. In general, pipeline vibration is severe only when the generating frequency is at, or near, the natural resonance frequency of the pipeline. This frequency is a function of the support system, layout geometry, temperature, mass, and pipe stiff ness, and is often difficult to predict.

There are two principal ways to control stress caused by vibration. You can usually observe the stability of the system during initial operation and add restraints or supports as required to reduce effects of equipment vibration. Where necessary, guides illustrated in Figure 6 will effectively hold pipe from lifting or moving laterally.

In special cases where source vibration is excessive (such as that resulting from pumps running unbalanced), an elastomeric expansion joint or other vibration absorber should be considered. If an expansion joint is considered, refer to EXPANSION JOINTS.

### **Connections to tanks**

The wall flexure of a tank as it is filled and emptied produces movements at nozzles which must be accommodated in the design. These movements can be absorbed by a loop or turn, or by an expansion joint. Avoid direct, straight-line connections between tanks.

## 7 Other design considerations

### **Coating Bondstrand**

Exposure to direct sunlight will eventually degrade the surface of Bondstrand piping. Although no failures are known to have resulted from this superficial degradation, it does cause a dull, grey appearance which many users wish to avoid.

Ameron products are available to prevent or arrest this effect, or for color coding. Based on studies at the factory, a five-mil single coat of Ameron Amershield<sup>®</sup> single coat polyurethane protective coating will provide suitable protection for either epoxy or vinyl ester pipe and fittings.

Adhesion of the coating is improved by delaying the application until the pipe surface has begun to weather. Pipe must be thoroughly cleaned before applying the coating.

For further information on chemical resistance, coverage rates, equipment and application procedures for coatings, contact Ameron's Protective Coatings Division.

### **Electrical properties**

Bondstrand pipe offers high resistance to stray electrical currents, a common cause of corrosion around valves and pumps. Table 18 gives the results of tests on Bondstrand pipe in a clean, as manufactured, condition at room temperature. Obviously, electrical properties, especially surface resistivity, are greatly affected by contamination and atmospheric conditions.

		ASTM
Property	Value	Test Method
Dielectric constant, at 1 KHz for a 0.22-inch thickness	5.9	D150
Dissipation factor, at 1 KHz for a 0.22 inch thickness	0.016 - 0.021	D150
Dielectric strength, by the short-time test using ¼-inch elec- trodes in oil for a 0.23-inch thickness, volts per mil	>230	D149
Dielectric breakdown voltage, by the short-time test using $\frac{1}{2}$ -inch electrodes in oil for a 0.23-inch thickness, kv	>53.4	D149
Surface resistivity, ohms	10 <sup>10</sup> to 10 <sup>12</sup>	D257
Volume resistivity, for a 0.22-inch thickness	10 <sup>14</sup> to 10 <sup>15</sup>	D257

 
 Table 18
 Electrical properties of Bondstrand Series 2000, 3000A, 3200A, 4000, 5000 and 5100 pipe

Note: All material was tested as manufactured and at room temperature.

High-velocity flow of fluids having low electrical conductivity, such as petroleum distillates, can generate significant amounts of static electricity. In buried pipe these charges are slowly dissipated. Be sure to ground projections or metal appurtenances, especially near discharge nozzles, filters, valves and other areas of high turbulence. Use saddles instead of elastomeric pads at supports to obtain better grounding.

Bondstrand Series 7000 pipe includes electrically conductive elements in the pipe wall which, when properly grounded, prevent accumulation on the exterior of the pipe of dangerous levels of static electricity produced by the flow of fluids inside the pipe.

### **Entrapped gases**

As in all piping systems, high points in the system will trap air or other gases. Trapped gases may create a hazard during test and operation of the system, and may restrict flow or drainage. It is recommended that air release valves be used at high points to permit bleeding out trapped air or other gases. See SMALL-DIAMETER METALLIC CONNECTIONS for suggested method of mounting.

### Steam condensate

Good drainage helps avoid water hammer in steam condensate lines. For further information, see our Bondstrand Guide for Steam Condensate, FP468, available from your local distributor.

### Heat tracing

Heat tracing may be needed to prevent freezing in cold weather or to maintain flow of viscous fluids at ambient temperature.

Wrap heat tracing helically to avoid the pipe deflection caused by heating one side of the pipe. Heat tracing should be directly on the pipe and within the insulation. Do not exceed maximum trace temperatures of 250°F for epoxy products or 200°F for vinyl ester products, and use the maximum trace temperature for the design of the piping system.

## **8** Detailing the supports

The following paragraphs describe and illustrate the different methods and devices used to support Bondstrand pipe and fittings in a suspended system.

Because outside diameters of Bondstrand pipe are the same as those for iron pipe size (IPS) standards, standard pipe supports and hangers often may be used for Bondstrand piping systems. Occasionally, larger supports as given in Table 19 are required to fit over elastomeric pads or saddles, especially at anchors.

#### Table 19 Recommended nominal hanger sizes for Bondstrand pipe

Note: Dimensions shown in parentheses are recommended inside diameters of anchoring device or support, and provide for a  $\frac{1}{4}$ -inch elastomeric pad thickness or a  $\frac{9}{16}$ -inch Bondstrand saddle thickness.

Nominal Diameter in. mm	with S	e Pipe or heet Metal rapper mm		/ith heric Pad <i>mm</i>	Bondstra	Two and 180° Saddles <i>mm</i>
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2 2 2 3 4 5 6 8 10 12 14 16	50 50 75 100 125 150 200 250 300 350 400	$\begin{array}{c} - \\ 2\frac{1}{2} \\ 3\frac{1}{2} \\ (5) \\ (6) \\ (7\frac{1}{2}) \\ (9\frac{1}{2}) \\ (11\frac{1}{2}) \\ (13\frac{1}{2}) \\ (14\frac{3}{2}) \\ (16\frac{3}{2}) \end{array}$	- 63.5 88.9 (125) (150) (181) (232) (286) (337) (375) (425)	- 3 4 5 6 (7 <sup>7</sup> /%) (9 <sup>7</sup> %) (12) (14) (15½) (17½)	- 75 100 125 150 (200) (251) (300) (350) (394) (445)

### **Clamping forces**

Support styles that clamp the pipe, are generally not recommended to ensure that clamping forces do not crush the pipe. Local crushing could result from a poor fit, and all-around crushing could result from over-tightening.

Where the pipe must be held tightly at the support, mount a pair of  $180^{\circ}$  support saddles between clamp and pipe for the ultimate in strength and long life. In some cases with Bondstrand 2000 or 4000, a  $\frac{1}{4}$ -inch thick elastomeric pad (Shore A durometer hardness  $60 \pm 5$ ) placed between clamp and pipe is a suitable alternative.

### Space between pipe

In multiple runs, allow clearance for flanges and other fittings having a diameter greater than the pipe. Table 20 shows the outside radius of standard Bondstrand products. Add space between pipe runs to accommodate length changes at loops and turns. Insulate as necessary to avoid direct exposure to hot pipe or other heat sources.

. г	NI '						
	Nomina	l diameter	Fil	tings lius, R	Fla	anges dius, R	Provide Clearance
	in.	mm	in.	mm	in.	mm	Provide Clearance
	1 2 3 4 5 6 8 10 12 14 16	25 40 50 100 125 150 200 250 300 350 400	$     \begin{array}{r}       1 \frac{1}{4} \\       1 \frac{1}{2} \\       2 \frac{3}{4} \\       2 \frac{3}{4} \\       3 \frac{3}{4} \\       3 \frac{3}{4} \\       4 \frac{3}{4} \\       6 \frac{1}{4} \\       7 \frac{3}{4} \\       9 \\       10 \frac{1}{2}   \end{array} $	32 38 44 57 70 83 95 121 159 197 229 267	$\begin{array}{c} 2\frac{1}{2}\\ 2\frac{3}{4}\\ 3\\ 3\frac{3}{4}\\ 4\frac{1}{2}\\ 4\frac{3}{4}\\ 5\frac{1}{2}\\ 6\frac{3}{4}\\ 8\\ 9\frac{1}{2}\\ 11\\ 13\end{array}$	64 70 76 95 114 121 140 171 203 241 279 330	R R

### Supports permitting pipe movement

Supports allowing pipe to move with relative freedom include:

- hangers which are free to move laterally or longitudinally with the pipe,
- fixed supports over which pipe must slide, allowing longitudinal movement and often lateral movement, and
- guides which permit longitudinal movement of the pipe but restrain lateral movement.

Hangers are free to move on their hanger rods and allow considerable longitudinal and lateral movement. Hanger types include band, ring or clevis type (Figure 3), or roller types (Figure 4) with the roller either suspended freely or held rigidly in a frame.

Fixed supports permit the pipe to move longitudinally and, in some cases, laterally. An ordinary pipe rack made of steel angle is a typical fixed support permitting both longitudinal and lateral movement. Figure 5 shows some typical types of fixed support. Pipe resting in fixed supports requires protection from external abrasion, as described below.

Guides (Figure 6) restrict translational movement but may permit longitudinal and rotational movement. Guides are recommended for lines which are subject to side-loads or uplift. Examples include lines subjected to pressure surges, lines emptied and filled during operation, and lines (especially when empty) which can be lifted or moved by wind or other external loadings. Use guides on vertical runs (see Table 17).

#### Table 20 Radius for determining piping clearance requirements for multiple runs

#### Notes:

- 1. Provide additional clearance between pipe runs to accommodate length changes at loops and turns.
- Provide additional clearance where Bondstrand saddles are used for branching, or where Bondstrand maintenance couplings or other special joining systems are used.

### **8** Detailing the supports (cont'd)

Though no significant longitudinal movement is involved, guides are normally required for restrained systems at spacings given in Table 5 through 14. An inexpensive guide for most applications is a light-duty U-bolt, double-nutted to restrict horizontal and vertical movement but which permits free longitudinal movement.

Abrasion protection must be provided to protect the pipe where it slides through a fixed support or guide. Choose a material compatible with the service environment and budget. Some recommended protective methods include:

- Bondstrand saddles, which provide a clean, corrosion-free surface acting as a stiffening saddle for the pipe. Saddles are bonded to the pipe. In eight-inch pipe and larger, light-duty abrasion protection can be provided by bonding a half section of the same pipe to the line pipe.
- elastomeric material such as rubber or neoprene. This material may be either bonded in place or held by the clamping force of the support device.
- galvanized sheet metal, bonded or banded to the pipe, where the environment is not too corrosive. Recommended minimum metal gauge is:
  - 2- through 6-in. pipe: 16 gauge (0.0598)
  - 8- through 16-in. pipe: 10 gauge (0.1345)

Abrasion protection must be firmly bonded or banded to the pipe wherever movement is possible between the pipe and the support.

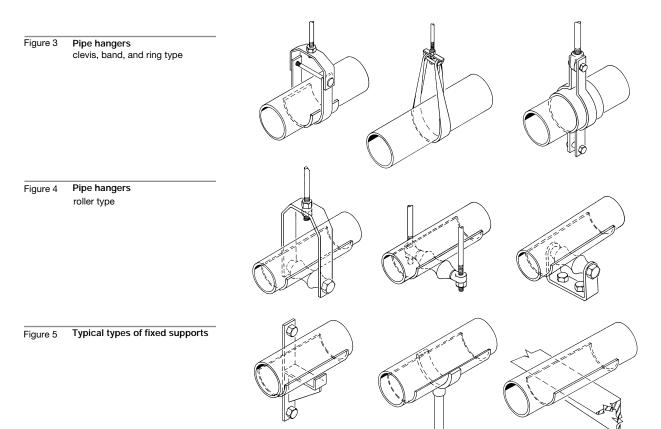
### Supports that anchor pipe

Pipe in a straight run is usually anchored by clamps or split rings. Light anchors intended only to hold pipe in position between loops or turns in a free system may be fixed supports, as shown in Figure 7.

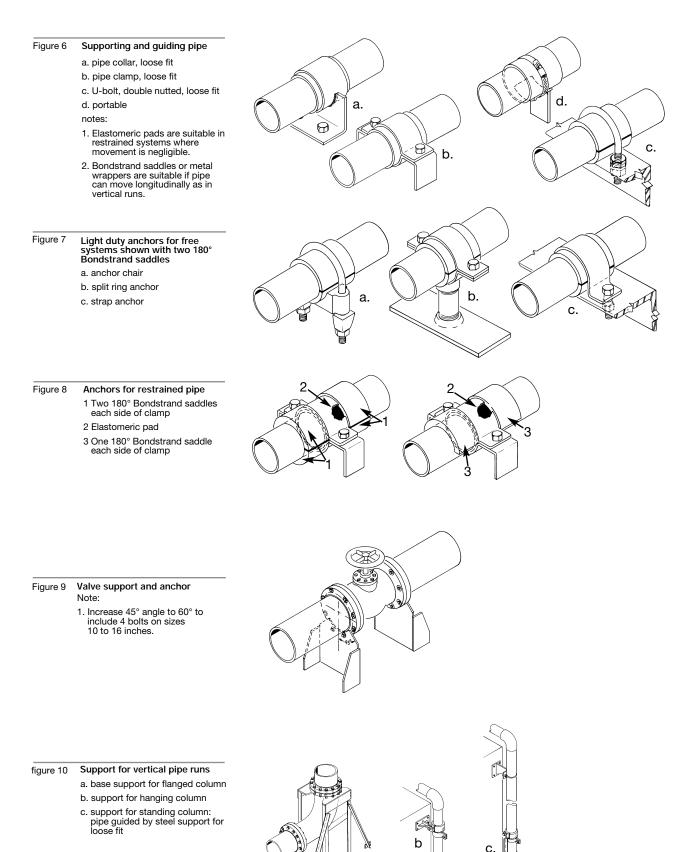
Supports required to resist length changes in restrained systems generally require the use of saddles. Saddles are recommended where pipe is to be held by ring clamps (Figure 8). Bonded saddles also may be used as a shear key along with a loose anchoring ring.

Valves and pumps in Bondstrand lines must be supported independently. Figure 9 shows how supports may be bolted to a flange to support weight, to resist thrust and torque, and to provide electrical grounding.

Vertical pipe runs are usually anchored using bonded saddles or flanges resting on a suitably reinforced and mounted guide or riser clamp (Figure 10).



## Detailing the supports (cont'd)





Appendix A

### Formulas for Calculating Length Change (with examples)

Thermal Expansion in Unrestrained Pipeline

Thermal expansion of a free Bondstrand pipeline is expressed by:

$$\frac{\Delta L}{L} = \alpha \Delta T \qquad \text{where}$$

$$\frac{\Delta L}{\alpha} = \text{change in le}$$

$$\alpha = \text{coefficient of line}$$

$$= \text{length of pix}$$

- L =change in length, in. =coefficient of thermal expansion, in./in./°F
- =length of pipeline, in.
- $\Delta T$  =change in temperature, °F

Here is an example of calculating  $\Delta L$  due to temperature. Assume that  $\Delta T = 150^{\circ}$ F, and  $\alpha = 10 \times 10^{-6}$  in./in./°F, then

 $\frac{\Delta L}{L} = 10 \times 10^{-6} (150) = 0.0015$  in./in. of pipe or 1.8 in./100 ft. of pipe

#### Length Change with Pressure in Unrestrained Pipeline

The length of pipe in a free pipeline will change as internal pressure is applied to the line. The amount of change is reduced by the Poisson effect and is calculated for a free pipeline with closed ends by:

$$\frac{\Delta L}{L} = \frac{p \ \overline{ID}^2}{4t E_{\ell} D_m} \Biggl( 1 - 2 \pi_{\ell \ c} \ \frac{E_{\ell}}{E_c} \Biggr) \ \text{ where }$$

L =length of pipe, in.

p =internal pressure, psi

 $\mu_{\ell c}$ =Poisson's ratio

- E<sub>c</sub> =circumferential modulus of elasticity, psi
- E<sub>1</sub> =longitudinal modulus of elasticity, psi
- D<sub>m</sub> =mean diameter of pipe wall, in.
- ID =inside diameter of pipe wall, in.
- t =thickness of pipe wall, in.

Here is an example of calculating  $\Delta L$  due to pressure. Assume that

p= 100 psi,  $\overline{ID}$  = 6.26 in., t= 0.180 in., D<sub>m</sub> = 6.44 in., E<sub>l</sub> = 1.6 x 10<sup>6</sup> psi,

$$\begin{split} E_c &= 3.6 \times 10^6 \text{ psi, and } \mu_{\ell C} = 0.56 \\ \frac{\Delta L}{L} &= \frac{100(6.26)^2}{4(0.180)(1.6 \times 10^6)(6.44)} \bigg[ 1 - 2(0.56) \bigg(\frac{1.6}{3.6}\bigg) \bigg] = \end{split}$$

0.00027 in./in. of pipe or 0.32 in./100 ft. of pipe

Notes:

Poisson's ratio for filament-wound structures depends on the ratio of the relative modulus of elasticity in the two directions under consideration. Both moduli are basically dependent on their orientation with respect to the glass fibers.

All three values,  $\, {\rm E}_{\ell}, \, {\rm E}_{c}$  and  $\, \mu_{\,\ell\text{C}}$  , used in this equation vary with temperature.

As indicated in Table 1, the effect of temperature on length change due to pressure within normal operating ranges is negligible.

### Appendix B Formulas for Calculating Thrust

Thrust Due To Temperature Change in a Blocked Line

- The thrust due to temperature change in a system fully restrained against length change is calculated by:  $P = a\Delta TA_w E_t = a\Delta TE_t (pD_m t)$ 
  - where P = thrust, lbf
    - $\alpha$  = coefficient of thermal expansion, in./in./°F
      - $\Delta T$  = change in temperature,  $\dot{o}F$
      - $E_{\ell}$  = longitudinal modulus of elasticity, psi
      - $A_w$  = cross-sectional area of the pipe wall, in.<sup>2</sup>
      - $D_m$  = mean diameter of the pipe wall, in.
      - t = thickness of pipe wall, in.

For example:

- $\alpha = 10 \times 10^{-6}$  in./in./°F,  $\Delta T = 150$ °F, t = 0.18 in., D<sub>m</sub> = 6.44 in.,
- and  $E_{\ell} = 1.6 \times 10^6 \text{ psi}$
- then  $P = (10 \times 10^{-6})(150)(1.6 \times 10^{6})[3.14(6.44)(0.18)] = 8,740 \text{ lbf}$

#### Thrust Due To Pressure in a Blocked System

In a fully restrained system, calculate the thrust between anchors induced by internal pressure using:

$$P = \frac{\pi p D_{\rm m} \overline{ID}}{2} \left( \frac{E_i}{E_c} \right) (-\mu_{ic})$$

where p = internal pressure, psi E<sub>c</sub> = circumferential modulus of elasticity, psi

$$\mu_{ic}$$
 = Poisson's ratio

For example, assume that

 $\overline{\text{ID}}$  = 6.26 in., D<sub>m</sub> = 6.44 in., p = 100 psi, E<sub>i</sub> = 1.6 x 10<sup>6</sup> psi,

$$E_{c}$$
 = 3.6 x 10^{6} psi, and  $\,\mu_{\,/\,C}\,$  = 0.56

then  $P = \frac{3.14(100)(6.44)(6.26)}{2} \left(\frac{1.6}{3.6}\right)(-0.56) = 1,575$  lbf (tension)

#### Thrust Due To Pressure on a Closed End"

Where internal pressure on a closed end exerts thrust on supports, calculate thrust using:

$$P = \frac{p \overline{ID}^2}{4} p$$

For example, if there is 100 psi in a 6-inch (6.26 in.) pipe, thrust is

$$\frac{3.14(6.26)^2}{4} \times 100 = 3,080 \text{ lbf}$$

Stress in the pipe is given in each of the above cases by:

$$f = \frac{P}{A_w}$$

where f = longitudinal stress, psi

In the last example,

$$f = \frac{3,080}{3.64} = 845 \text{ psi}$$



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### Formula for Calculating Support Spacings for Uniformly Distributed Load

Suspended pipe is often required to carry loads other than its own weight and a fluid with a specific gravity of 1.0. Perhaps the most common external loading is thermal insulation, but the basic principle is the same for all loads which are uniformly distributed along the pipeline. The way to adjust for increased loads is to decrease the support spacing, and conversely, the way to adjust for decreased loads is to increase the support spacing. An example of the latter is a line filled with a gas instead of a liquid, and longer spans are indicated if deflection is the controlling factor.

For all such loading cases, support spacings for partially continuous spans with a permissible deflection of 0.5 inch are determined using:

$$L = 0.258 \, \sqrt[4]{\frac{(E I)}{w}}$$

where L = support spacings, ft. (EI) = beam stiffness,  $Ib \bullet in^2$  (from Table C2) w = total uniformly distributed load, Ib/lin in.

For example, calculate the recommended support spacing for 6-inch Bondstrand Series 2000 pipe full of water at  $200^{\circ}F$ :

 $L = 0.258 \, 4 \sqrt{\frac{16,000,000}{(0.25 + 1.1)}} = 15.1 \, \text{ft}.$ 

When using metric units the formula becomes:

### 9 Appendix C (cont'd)

Table C1 Values for use in calculating support spacings

	Uniform Weight of Pipe									
Nominal Pipe Size	Series 2000/4000		2000M-FP		5000		700		3000A/3200A	
in. <i>mm</i>	lb/in	N/m	lb/in	N/m	lb/in	N/m	lb/in	N/m	lb/in	N/m
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0.03\\ 0.06\\ 0.08\\ 0.10\\ 0.17\\ 0.22\\ 0.25\\ 0.36\\ 0.45\\ 0.53\\ 0.62\\ 0.79\\ \end{array}$	5.8 10 13 18 29 38 44 63 79 93 108 139	$\begin{array}{c} 0.09\\ 0.12\\ 0.17\\ 0.24\\ 0.35\\ 0.44\\ 0.53\\ 0.78\\ 1.10\\ 1.38\\ 1.52\\ 2.13 \end{array}$	16 20 42 61 77 92 136 193 241 266 372	$\begin{array}{c} 0.03\\ 0.06\\ 0.08\\ 0.13\\ 0.20\\ 0.22\\ 0.29\\ 0.42\\ 0.52\\ 0.62\\ 0.73\\ 0.93 \end{array}$	5.8 10 15 22 35 38 51 73 90 108 127 163	$\begin{array}{c} 0.04\\ 0.08\\ 0.08\\ 0.10\\ 0.17\\ 0.22\\ 0.25\\ 0.43\\ 0.68\\ 0.92\\ 1.08\\ 1.42 \end{array}$	7.3 13 15 18 29 38 44 76 118 160 190 248	- 0.04 0.06 0.08 - 0.16 0.26 0.38 0.51 0.63 0.78	- 7.3 10 15 - 28 45 66 89 109 137

Nomi	Nominal		Uniform Weight of Fluid										
	Pipe Size		.=1.0	S.G.	.=1.3	S.G.=1.6							
in.	mm	lb/in	N/m	lb/in	N/m	lb/in	N/m						
1 1.5 2 3 4 5 6 8 10 12 14 16	25 40 50 100 125 150 200 250 300 350 400	$\begin{array}{c} 0.3\\ 0.8\\ 0.12\\ 0.29\\ 0.49\\ 0.76\\ 1.1\\ 1.9\\ 3.0\\ 4.3\\ 5.2\\ 6.8\end{array}$	5.6 14 22 51 85 134 195 336 532 757 913 1193	$\begin{array}{c} 0.04\\ 0.10\\ 0.16\\ 0.38\\ 0.63\\ 0.99\\ 1.4\\ 2.5\\ 3.9\\ 5.6\\ 6.8\\ 8.9\end{array}$	7.3 18 28 67 111 174 253 437 691 985 1187 1551	8.3	9.0 22 35 82 136 214 312 537 851 1212 1461 1909						

## Table C2 Effective beam stiffness values for use in calculating support spacings

			Effective Beam Stiffness Factor, EI (million Ib in <sup>2</sup> )•EI (kN m <sup>2</sup> )														
Nominal Series 2000 Pipe Size			Series 2000M-FP			Series 4000				Series 5000							
in.	mm	up to 150°F	67°C to 121°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 200°F	0 67°C to 93°C
1 2 3 4 5 6 8 10 12 14 16	25 40 50 100 125 150 200 250 300 350 400	0.16 0.52 1.0 3.3 9.2 18 30 76 148 250 348 590	0.46 1.5 2.8 9.5 26 51 87 217 426 716 999 1693	$\begin{array}{c} 0.09\\ 0.30\\ 0.58\\ 1.9\\ 5.4\\ 10\\ 18\\ 45\\ 87\\ 147\\ 205\\ 347\\ \end{array}$	0.27 0.87 1.7 5.6 30 51 128 251 421 587 996	0.16 0.52 1.0 3.3 9.2 18 30 93 231 465 624 1066	0.46 1.48 9.5 261 87 268 664 1334 1790 3061	$\begin{array}{c} 0.09\\ 0.30\\ 0.58\\ 1.9\\ 5.4\\ 10\\ 18\\ 55\\ 136\\ 273\\ 367\\ 627\\ \end{array}$	0.27 0.87 1.7 5.6 16 30 51 158 391 784 1053 1800	$\begin{array}{c} 0.13\\ 0.42\\ 0.80\\ 2.7\\ 7.8\\ 15\\ 26\\ 65\\ 128\\ 214\\ 325\\ 554 \end{array}$	0.38 1.21 2.3 7.6 22 43 74 187 366 615 934 1590	0.08 0.27 0.51 1.7 5.0 9.5 16 41 81 136 207 352	0.24 0.77 1.5 4.8 14 27 47 119 233 391 593 1010	.011 0.36 0.69 2.3 6.7 13 22 55 109 182 276 468	0.33 1.04 2.0 6.6 19 37 63 159 312 523 791 1342	$\begin{array}{c} 0.01 \\ 0.05 \\ 0.09 \\ 0.29 \\ 0.86 \\ 1.6 \\ 2.8 \\ 7.1 \\ 14 \\ 23 \\ 35 \\ 60 \end{array}$	0.04 0.13 0.25 2.5 4.7 8.1 20 40 67 102 173
		Series 5100				Series 7000			Series 3000A				Series 3200A				
Nom Pipe		up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 121°C	up to 150°F	up to 66°C	151°F to 250°F	67°C to 99°C	up to 150°F	up to 66°C	151°F to 210°F	67°C to 99°C
in.	mm	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т	ft.	т
1 1.5 2 3 4 5 6 8	25 40 50 80 100 125 150 200	.011 0.36 0.69 2.3 6.7 13 22 55	0.33 1.04 2.0 6.6 19 37 63 159	0.01 0.05 0.09 0.29 0.86 1.6 2.8 7.1	0.04 0.13 0.25 0.85 2.5 4.7 8.1 20	0.18 0.57 1.1 3.7 10 19 33 100	0.50 1.6 3.2 11 29 56 96 288	0.10 0.34 0.65 2.2 5.9 11 20 59	0.30 0.97 1.9 6.3 17 33 56 169	- 1.1 3.8 8.3 - 36 40	- 3.1 11 24 - 104 115	0.81 2.8 6.2 27 30	- 2.3 8.1 18 - 78 86	- 1.1 3.8 8.3 - 36 80	- 3.1 11 24 - 104 230	- 0.81 2.8 6.2 - 27 60	- 2.3 8.1 18 - 78 173

## Notes

## Health and safety information

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DAY OR NIGHT

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202-483-7616 -Washington D.C. collect

### Toxicity of adhesive

Hardener: Irritating to the skin, eyes and respiratory tract: toxic orally; may cause sensitization.

Resin: May be mildly irritating to skin and eyes; may cause sensitization.

### Handling precautions for adhesive

Hardener:	Do not get in eyes, on skin or clothing. Avoid breathing vapor.
	Wash thoroughly after handling. When handling in the field, wear
	gloves and eye protection. When handling in bulk quantities, wear rubber gloves, rubber apron and NIOSH approved respirator.

Resin:

Avoid contact with eyes, skin or clothing. When handling in the field, wear gloves and eye protection. Wash thoroughly after handling.

### First aid for adhesive users

### In case of contact

- **Eyes:** Immediately flush with plenty of water for at least 15 minutes. Call a physician.
- **Skin:** Wash with water and soap if available.
- Clothing: Remove contaminated clothing and wash before reuse.
- Inhalation: Remove to fresh air. Give oxygen or artificial respiration if neces-

sary.

Ingestion: If hardener is swallowed and person is conscious, give plenty of water or milk to drink. Do not induce vomiting. Call a physician.

Important notice

This literature and the information and recommendations it contains are based on data reasonably believed to be reliable. However, such factors as variations in environment, application or installation, changes in operating procedures, or extrapolation of data may cause different results. Ameron makes no representation or warranty, express or implied, including warranties of merchantability or fitness for purpose, as to the accuracy, adequacy or completeness of the recommendations or information contained herein. Ameron assumes no liability whatsoever in connection with this literature or the information or recommendations it contains.





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