

Question No.1

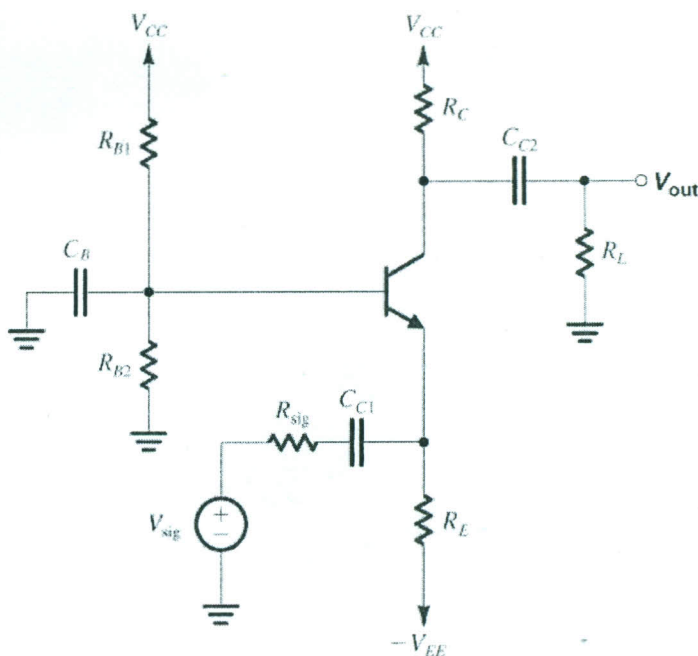
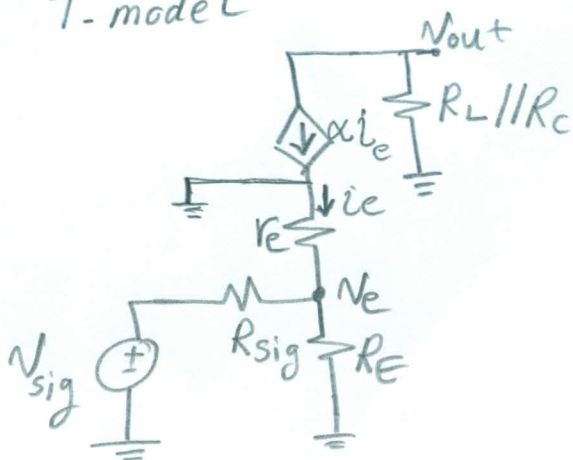
Consider the CB amplifier circuit shown below, neglect r_o and r_x ,

A. Drive the expression for medium-frequency voltage gain (V_{out}/V_{sig}). [5 points]

B. Drive the expressions for all low frequency poles. [12 point]

C. Does this amplifier suffer from Miller's effect? [1 point] Without calculations how does this influence the frequency response of the amplifier? [2 points]

A. T-model



$$\frac{V_{out}}{V_{sig}} = \frac{V_e}{V_{sig}} \cdot \frac{V_{out}}{V_e}$$

$$= \frac{r_e \parallel R_E}{(r_e \parallel R_E) + R_{sig}} \cdot \frac{-\alpha i_e (R_L \parallel R_C)}{-i_e r_e} = \frac{r_e \parallel R_E}{r_e \parallel R_E + R_{sig}} \cdot \frac{R_L \parallel R_C}{r_e}$$

5

$$\omega_{L1} = \frac{1}{C_B R_{CB}} ; R_{CB} = R_{B1} \parallel R_{B2} \parallel [(\beta+1)(r_e + R_{sig} \parallel R_E)]$$

$$\omega_{L2} = \frac{1}{C_{C1} R_{C1}} ; R_{C1} = R_{sig} \parallel [R_E \parallel r_e] \cdot \frac{r_e \parallel R_E}{\beta+1}$$

$$\omega_{L3} = \frac{1}{C_{C2} R_{C2}} ; R_{C2} = R_L + R_C$$

C. No, CB does not suffer from miller. Base is grounded. [1]

Thus C_B & C_{C1} are grounded,

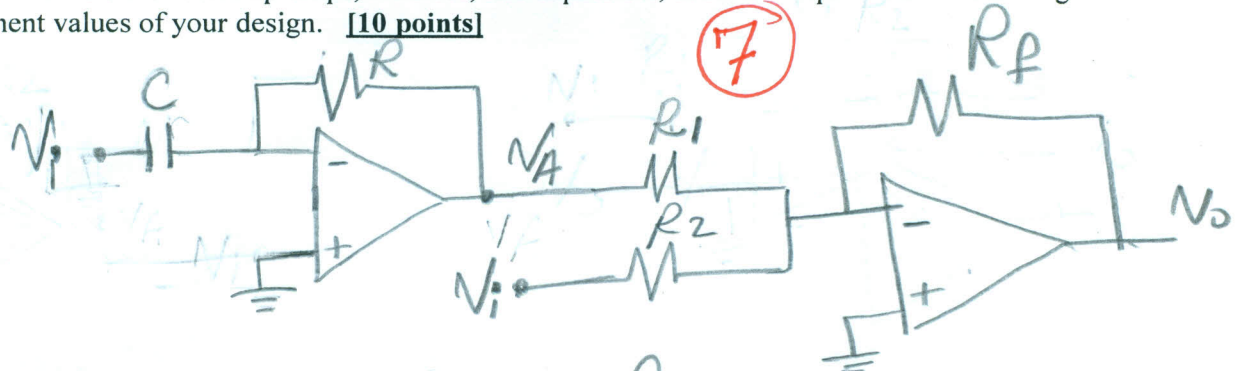
Due to this, it has wide bandwidth. [2]

Question No.2

A. Design a circuit to implement the following function:

$$v_o = 4 \frac{dv_i}{dt} - 3v_i$$

Use minimum number of ideal op-amps, resistors, and capacitors, draw a complete circuit showing the component values of your design. **[10 points]**



$$V_A = -CR \frac{dV_i}{dt} ; V_o = -\frac{R_f}{R_1} V_A - \frac{R_f}{R_2} V_i$$

$$V_o = CR \frac{R_f}{R_1} \frac{dV_i}{dt} - \frac{R_f}{R_2} V_i ; \begin{cases} \frac{R_f}{R_2} = 3 \Rightarrow R_2 = 3.33k\Omega \\ R_f = 10k\Omega \\ CR \frac{R_f}{R_1} = 4 \Rightarrow C = 10\mu F, R = 40k\Omega \\ R_f = 10k\Omega, R_1 = 1k\Omega \end{cases}$$

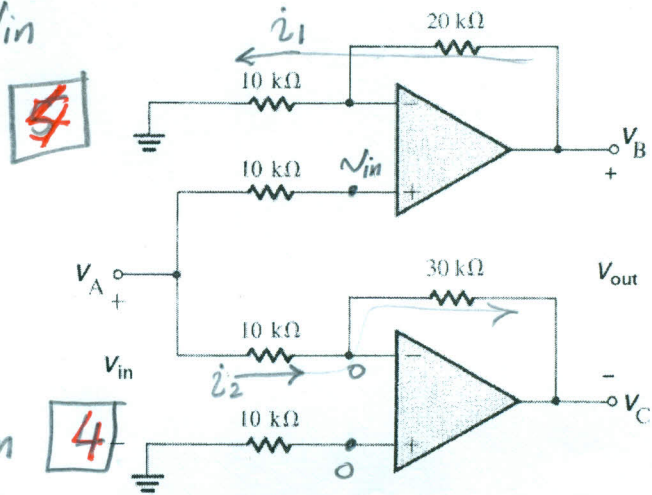
B. For the circuit showing below, assuming ideal op amps find the voltage gain V_{out}/V_{in} **[10 points]**

$$i_1 = \frac{V_{in}}{10k} ; V_B = 20k i_1 + V_{in}$$

$$V_B = 2V_{in} + V_{in} = 3V_{in}$$

$$i_2 = \frac{V_{in}}{10k} ; V_C = -30k i_2$$

$$V_C = -30k \frac{V_{in}}{10k} = -3V_{in}$$



$$V_{out} = V_B - V_C = 3V_{in} - (-3V_{in}) = 6V_{in}$$

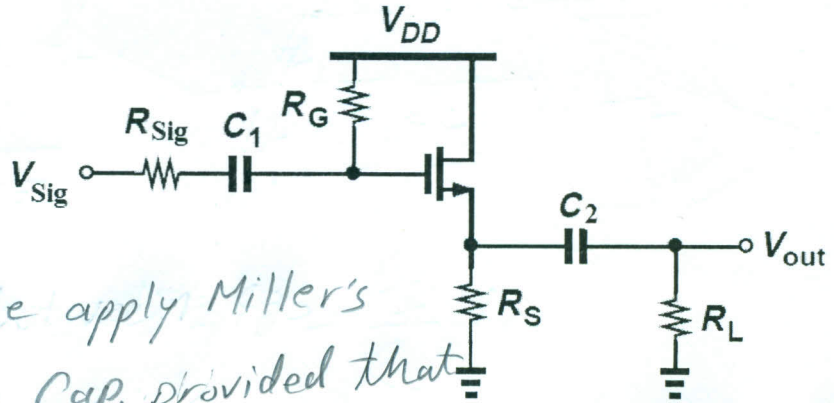
$$\frac{V_{out}}{V_{in}} = 6$$

[2]

Question No. 3

In the circuit shown, $g_m = 3\text{ms}$, $C_{gs} = 10\text{pF}$, $C_{gd} = 1\text{pF}$, $R_{sig} = 1\text{k}\Omega$, $R_G = 4.3\text{k}\Omega$, $R_s = 1.3\text{k}\Omega$ and $R_L = 24\text{k}\Omega$, $C_1 = C_2 = 10\mu\text{f}$.

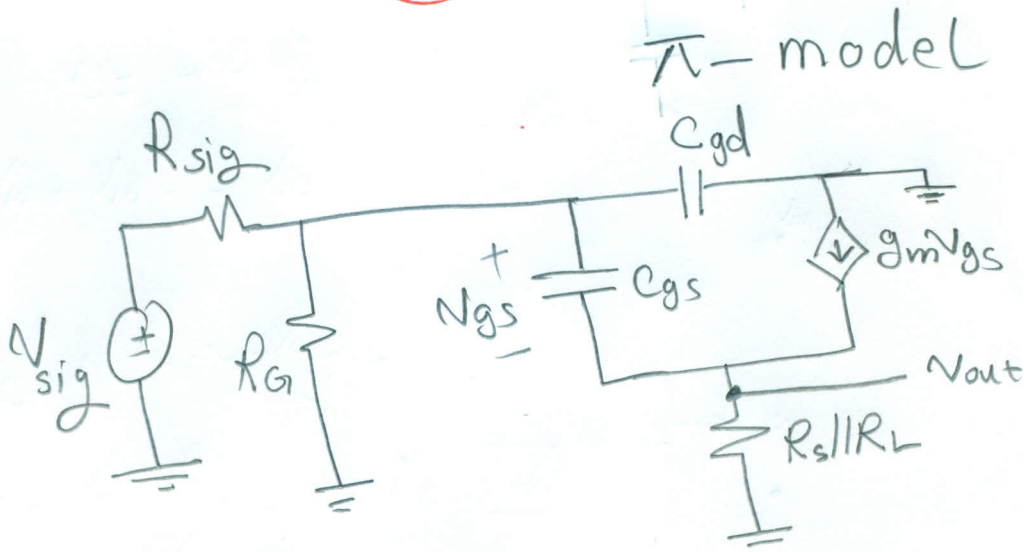
- A. Can you apply Miller's theorem to the capacitor C_{gs} ? Why? [4 points]
- B. Determine and then calculate all of the high frequency poles. [14 points]
- C. Estimate the upper 3dB frequency. [2 points]



A. You can always apply Miller's theorem to bridging Cap. provided that you have K . In this case using π -model analysis will give more accurate answer than miller approach.

(4)

B.



(3)

$$\omega_{H1} = \frac{1}{C_{gd}(R_{sig} || R_G)}$$

(5)

$$\omega_{H1} = 1.235 \text{ G rad/s}$$

$$f_{H1} = 196.6 \text{ MHz}$$

$$\omega_{H2} = \frac{1}{C_{gs} \left[\frac{(R_{sig} || R_G) + (R_s || R_L)}{1 + g_m(R_s || R_L)} \right]}$$

(6)

$$\omega_{H2} = 230 \text{ M rad/s}$$

$$f_{H2} = 36.6 \text{ MHz}$$

C.

$$f_{3dB} = f_{H2} = 36.6 \text{ MHz}$$

(2)