### 3. STATE VARIABLE MODELS (cont.)

ALTERNATIVE SIGNAL-FLOW GRAPH MODELS (CONT.)

**Diagonal Form** 

Consider the transfer function:

 $\frac{Y(s)}{R(s)} = \frac{30(s+1)}{s^3 + 9s^2 + 26s + 24} = \frac{30(s+1)}{(s+5)(s+2)(s+3)}$ 

It is clear that the transient response of the system has three modes, These modes are indicated by the partial fraction expansion as

$$\frac{Y(s)}{R(s)} = \frac{k_1}{(s+5)} + \frac{k_2}{(s+2)} + \frac{k_3}{(s+3)}$$

The coefficients  $k_1, k_2$ , and  $k_3$  are called residues and are evaluated by multiplying through by the denominator factor of  $\frac{30(s+1)}{(s+5)(s+2)(s+3)}$  corresponding to  $k_i$  and setting s equal to the root.

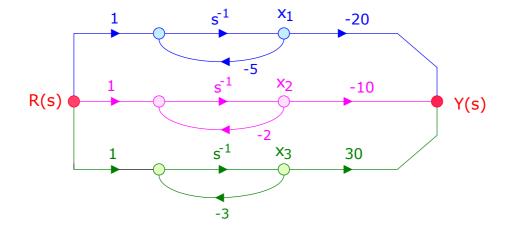
Evaluating  $k_1, k_2$ , and  $k_3$  we have

$$k_{1} = \left[ (s+5) \frac{30(s+1)}{(s+5)(s+2)(s+3)} \right] \Big|_{s=-5} = -20$$
  

$$k_{2} = \left[ (s+2) \frac{30(s+1)}{(s+5)(s+2)(s+3)} \right] \Big|_{s=-2} = -10$$
  

$$k_{3} = \left[ (s+3) \frac{30(s+1)}{(s+5)(s+2)(s+3)} \right] \Big|_{s=-3} = 30$$

$$\frac{Y(s)}{R(s)} = \frac{-20}{(s+5)} + \frac{-10}{(s+2)} + \frac{30}{(s+3)}$$



Using the above SFG to derive the set of first-order differential equations, we obtain:

$$\begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \\ \dot{x}_{3} \end{bmatrix} = \begin{bmatrix} -5 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -3 \end{bmatrix} \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} u(t)$$
$$y = \begin{bmatrix} -20 & -10 & 30 \end{bmatrix} \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix}$$

THE TRANSFER FUNCTION FROM STATE EQUATIONS

Given the state variable equations, we can obtain the transfer function using a signal-flow graph model and applying Mason's rule. We will now derive a formula for the transfer function of a single-input, single-output system.

Given

 $\dot{\mathbf{x}} = A\mathbf{x} + B\mathbf{u}$ ;  $y = C\mathbf{x}$  [*D* is assumed = 0]

The Laplace transforms of the above equations are

$$s\mathbf{X}(s) = A\mathbf{X}(s) + BU(s)$$
;  $Y(s) = C\mathbf{X}(s)$ 

 $(sI - A)\mathbf{X}(s) = BU(s)$ 

 $\boldsymbol{X}(\boldsymbol{S}) = (\boldsymbol{S}\boldsymbol{I} - \boldsymbol{A})^{-1}\boldsymbol{B}\boldsymbol{U}(\boldsymbol{S})$ 

 $Y(s) = CX(s) = C(sI - A)^{-1}BU(s)$ 

 $Y(s) = C\Phi(s)BU(s)$ 

Therefore the transfer function is  $G(s) = C\Phi(s)B$ 

If  $D \neq 0$ , the transfer function is  $G(s) = C(sI - A)^{-1}B + D = C\Phi(s)B + D$ 

*Example* 

Determine the transfer function of the system described by:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & \frac{-1}{C} \\ \frac{1}{L} & \frac{-R}{L} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{1}{C} \\ 0 \end{bmatrix} u(t); \quad y(t) = \begin{bmatrix} 0 & R \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

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Note that we do not include initial conditions, since we seek the transfer function.

Solution

$$[sI-A] = \begin{bmatrix} s & \frac{1}{C} \\ \frac{-1}{L} & (s+\frac{R}{L}) \end{bmatrix}; \Delta(s) = |sI-A| = \begin{vmatrix} s & \frac{1}{C} \\ \frac{-1}{L} & (s+\frac{R}{L}) \end{vmatrix} = s^2 + \frac{R}{L}s + \frac{1}{LC}$$
$$\Phi(s) = [sI-A]^{-1} = \begin{bmatrix} s & \frac{1}{C} \\ \frac{-1}{L} & (s+\frac{R}{L}) \end{bmatrix}^{-1} = \frac{1}{\Delta(s)} \begin{bmatrix} \left(s+\frac{R}{L}\right) & \frac{-1}{C} \\ \frac{1}{L} & s \end{bmatrix}$$

Then the transfer function is

$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 0 & R \end{bmatrix} \frac{1}{\Delta(s)} \begin{bmatrix} \left(s + \frac{R}{L}\right) & \frac{-1}{C} \\ \frac{1}{L} & s \end{bmatrix} \begin{bmatrix} \frac{1}{C} \\ 0 \end{bmatrix}$$
$$\frac{Y(s)}{U(s)} = \frac{\frac{R}{LC}}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$

EVALUATION OF THE STATE TRANSITION MATRIX

For higher order systems, evaluating  $\Phi(s)$  using the formula  $\Phi(s) = [sI - A]^{-1}$  is generally inconvenient. The usefulness of the signal-flow graph state model for obtaining the state transition matrix is highlighted.

Consider the system  $\dot{\mathbf{x}} = A\mathbf{x} + Bu$ ; The solution for the above system, when u(t) = 0, is  $\mathbf{x}(t) = \Phi(t)\mathbf{x}(o)$ 

Taking the Laplace transformation of the above equation, we have  $X(s) = \Phi(s)x(0)$ 

Therefore we can evaluate the Laplace transform of the transition matrix from the signal-flow graph by determining the relation between a state variable  $X_i(s)$  and the state initial conditions  $[x_1(0), x_2(0)...x_n(0)]$ , using Mason's gain formula.

Thus for a second-order system, we would have

 $X_1(s) = \varphi_{11}(s)X_1(0) + \varphi_{12}(s)X_2(0)$  $X_2(s) = \varphi_{21}(s)X_1(0) + \varphi_{22}(s)X_2(0)$ 

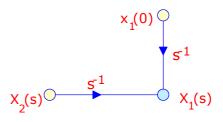
Note that all the elements of the state transition Matrix  $\varphi_{ij}(s)$ , can be obtained by evaluating the individual relationships between  $X_i(s)$  and  $x_j(0)$  from the state model flow graph.

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How to show Initial Conditions on the SFG

Consider the equation  $\dot{x}_1 = x^2$ ;  $x_1(0)$ Taking Laplace transform yields  $sX_1(s) - x_1(0) = X_2(s)$ The above equation becomes  $X_1(s) = s^{-1}x_1(0) + s^{-1}X_2(s)$ , which is algebraic and can be represented by a signal flow graph as shown.



Note that the initial condition of the state  $x_1$  appears as an input to the node representing the state with a branch gain of  $s^{-1}$ .

## **Example**

Determine  $\Phi(s)$  for the system given by  $A = \begin{bmatrix} 0 & -2 \\ 1 & -3 \end{bmatrix}$ ,  $B = \begin{bmatrix} 2 \\ 0 \end{bmatrix}$ ,  $C = \begin{bmatrix} 0 & 3 \end{bmatrix}$  using two different methods.

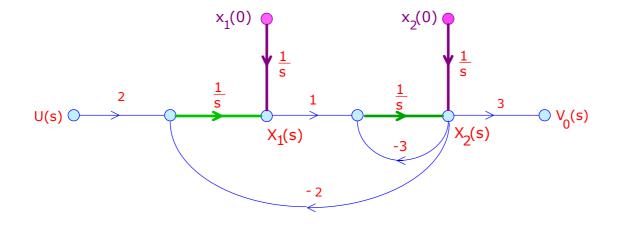
<u>Solution</u>

(1)

$$[sI-A] = \begin{bmatrix} s & 2 \\ -1 & (s+3) \end{bmatrix}; \Delta(s) = |sI-A| = \begin{vmatrix} s & 2 \\ -1 & (s+3) \end{vmatrix} = s^2 + 3s + 2$$

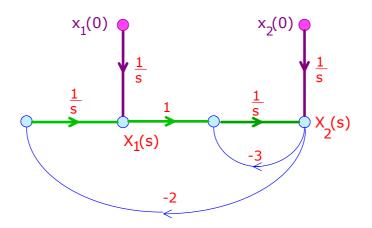
$$\Phi(s) = [sI - A]^{-1} = \begin{bmatrix} s & 2 \\ -1 & (s+3) \end{bmatrix}^{-1} = \frac{1}{(s^2 + 3s + 2)} \begin{bmatrix} (s+3) & -2 \\ 1 & s \end{bmatrix}$$

(2) Draw a signal-flow graph showing all initial conditions



To obtain  $\Phi(s)$ , set U(s) = 0, and redraw the SFG without the input and output nodes because they are not involved in the evaluation of  $\Phi(s)$ .

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## Recall that

 $X_{1}(s) = \varphi_{11}(s)X_{1}(0) + \varphi_{12}(s)X_{2}(0)$  $X_{2}(s) = \varphi_{21}(s)X_{1}(0) + \varphi_{22}(s)X_{2}(0)$ Where  $\Phi(s) = \begin{bmatrix} \varphi_{11}(s) & \varphi_{12}(s) \\ \varphi_{21}(s) & \varphi_{22}(s) \end{bmatrix}$ 

# Using Mason's gain formula, we obtain

$$\varphi_{11}(s) = \left. \frac{X_1(s)}{x_1(0)} \right|_{x_2(0)=0} = \frac{\frac{1}{5}(1+3s^{-1})}{1+3s^{-1}+2s^{-2}} = \frac{s+3}{(s^2+3s+2)}$$
$$\varphi_{12}(s) = \left. \frac{X_1(s)}{x_2(0)} \right|_{x_1(0)=0} = \frac{\frac{1}{5}(-2s^{-1})}{1+3s^{-1}+2s^{-2}} = \frac{-2}{(s^2+3s+2)}$$
$$X_2(s) = \left. \frac{1}{5}(s^{-1}) \right|_{x_1(0)=0} = \frac{1}{5}(s^{-1}) = 1$$

$$\varphi_{21}(s) = \left. \frac{X_2(s)}{X_1(0)} \right|_{X_2(0)=0} = \frac{\overline{s}(s^{-1})}{1+3s^{-1}+2s^{-2}} = \frac{1}{(s^2+3s+2)}$$

$$\varphi_{22}(s) = \left. \frac{X_2(s)}{X_2(0)} \right|_{X_1(0)=0} = \frac{\frac{1}{s}(1)}{1+3s^{-1}+2s^{-2}} = \frac{s}{(s^2+3s+2)}$$

Hence

$$\Phi(s) = \left[\begin{array}{c} \frac{s+3}{(s^2+3s+2)} & \frac{-2}{(s^2+3s+2)} \\ \frac{1}{(s^2+3s+2)} & \frac{s}{(s^2+3s+2)} \end{array}\right]$$

Same answer as (1)

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# **Comments**

• We can now find  $\Phi(t)$  if we wish

$$\Phi(t) = \mathcal{L}^{-1} \Phi(s) = \begin{bmatrix} (2e^{-t} - e^{-2t}) & (-2e^{-t} + 2e^{-2t}) \\ (e^{-t} - e^{-2t}) & (-e^{-t} + 2e^{-2t}) \end{bmatrix}$$

• We can also find the states and the output for any initial conditions. For example when  $x_1(0) = x_2(0) = 1$  and u(t) = 0, we have

$$\begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \Phi(t) \begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} (2e^{-t} - e^{-2t}) & (-2e^{-t} + 2e^{-2t}) \\ (e^{-t} - e^{-2t}) & (-e^{-t} + 2e^{-2t}) \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} e^{-2t} \\ e^{-2t} \end{bmatrix}$$