

**KING FAHD UNIVERSITY OF PETROLEUM & MINERALS**

**ELECTRICAL ENGINEERING DEPARTMENT**

**EE 463 – Term 131**

**HW # 1: Basic Concepts**

**Key Solution**

**From Text:** 2.3; 2.5; 2.15; 3.11; 3.13; 3.15

**Extra Problems:**

**Problem # 1)**

An industrial plant consisting primarily of induction motor loads absorbs 1000kW at 0.7 power factor lagging.

- (a) Compute the required kVA rating of a shunt capacitor to improve the power factor to 0.9 lagging.
- (b) Calculate the resulting power factor if a synchronous motor rated 1000 hp with 90% efficiency operating at rated load and at unity power factor is added to the plant instead of the capacitor.

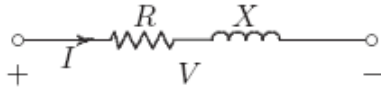
**Due Dates:**

UTR Classes: Sep. 15th 2013.

MW Classes: Sep. 16th 2013

**From Text:**

2.3. An inductive load consisting of  $R$  and  $X$  in series feeding from a 2400-V rms supply absorbs 288 kW at a lagging power factor of 0.8. Determine  $R$  and  $X$ .



**FIGURE 5**

An inductive load, with  $R$  and  $X$  in series.

$$\theta = \cos^{-1} 0.8 = 36.87^\circ$$

The complex power is

$$S = \frac{288}{0.8} \angle 36.87^\circ = 360 \angle 36.87^\circ \text{ kVA}$$

The current given from  $S = VI^*$ , is

$$I = \frac{360 \times 10^3 \angle -36.87^\circ}{2400 \angle 0^\circ} = 150 \angle -36.87^\circ \text{ A}$$

Therefore, the series impedance is

$$Z = R + jX = \frac{V}{I} = \frac{2400 \angle 0^\circ}{150 \angle -36.87^\circ} = 12.8 + j9.6 \ \Omega$$

Therefore,  $R = 12.8 \ \Omega$  and  $X = 9.6 \ \Omega$ .

2.5. Two loads connected in parallel are supplied from a single-phase 240-V rms source. The two loads draw a total real power of 400 kW at a power factor of 0.8 lagging. One of the loads draws 120 kW at a power factor of 0.96 leading. Find the complex power of the other load.

$$\theta = \cos^{-1} 0.8 = 36.87^\circ$$

The total complex load is

$$\begin{aligned} S &= \frac{400}{0.8} \angle 36.87^\circ = 500 \angle 36.87^\circ \text{ kVA} \\ &= 400 \text{ kW} + j300 \text{ kvar} \end{aligned}$$

The 120 kW load complex power is

$$\begin{aligned} S &= \frac{120}{0.96} \angle -16.26^\circ = 125 \angle -16.26^\circ \text{ kVA} \\ &= 120 \text{ kW} - j35 \text{ kvar} \end{aligned}$$

Therefore, the second load complex power is

$$S_2 = 400 + j300 - (120 - j35) = 280 \text{ kW} + j335 \text{ kvar}$$

2.15. Three loads are connected in parallel across a 12.47 kV three-phase supply.

Load 1: Inductive load, 60 kW and 660 kvar.

Load 2: Capacitive load, 240 kW at 0.8 power factor.

Load 3: Resistive load of 60 kW.

(a) Find the total complex power, power factor, and the supply current.

(b) A Y-connected capacitor bank is connected in parallel with the loads. Find the total kvar and the capacitance per phase in  $\mu\text{F}$  to improve the overall power factor to 0.8 lagging. What is the new line current?

$$S_1 = 60 \text{ kW} + j660 \text{ kvar}$$

$$S_2 = 240 \text{ kW} - j180 \text{ kvar}$$

$$S_3 = 60 \text{ kW} + j0 \text{ kvar}$$

(a) The total complex power is

$$S = 360 \text{ kW} + j480 \text{ kvar} = 600\angle 53.13^\circ \text{ kVA}$$

The phase voltage is

$$V = \frac{12.47}{\sqrt{3}} = 7.2\angle 0^\circ \text{ kV}$$

The supply current is

$$I = \frac{600\angle -53.13^\circ}{(3)(7.2)} = 27.77\angle -53.13^\circ \text{ A}$$

The power factor is  $\cos 53.13^\circ = 0.6$  lagging.

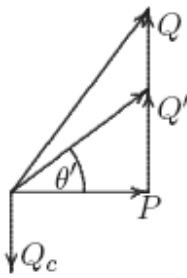
(b) The net reactive power for 0.8 power factor lagging is

$$Q' = 360 \tan 36.87^\circ = 270 \text{ kvar}$$

Therefore, the capacitor kvar is  $Q_c = 480 - 270 = 210 \text{ kvar}$ , or  $S_c = -j210 \text{ kVA}$ .

$$X_c = \frac{|V_L|^2}{S_c^*} = \frac{(12.47 \times 1000)^2}{j210000} = -j740.48 \Omega$$

$$C = \frac{10^6}{(2\pi)(60)(740.48)} = 3.58 \mu\text{F}$$



**FIGURE 14**

The power diagram for Problem 2.15.

$$I = \frac{S^*}{V^*} = \frac{360 - j270}{(3)(7.2)} = 20.835 \angle -36.87^\circ \text{ A}$$

**3.11.** A three-phase, Y-connected, 75-MVA, 27-kV synchronous generator has a synchronous reactance of  $9.0 \Omega$  per phase. Using rated MVA and voltage as base values, determine the per unit reactance. Then refer this per unit value to a 100-MVA, 30-kV base.

The base impedance is

$$Z_B = \frac{(KV_B)^2}{MVA_B} = \frac{(27)^2}{75} = 9.72 \Omega$$

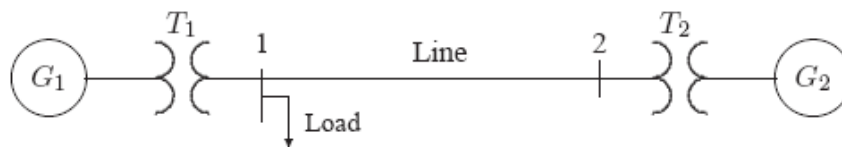
$$X_{pu} = \frac{9}{9.72} = 0.926 \text{ pu}$$

The generator reactance on a 100-MVA, 30-kV base is

$$X_{pu_{new}} = 0.926 \left( \frac{100}{75} \right) \left( \frac{27}{30} \right)^2 = 1.0 \text{ pu}$$

**3.13.** Draw an impedance diagram for the electric power system shown in Figure 26 showing all impedances in per unit on a 100-MVA base. Choose 20 kV as the voltage base for generator. The three-phase power and line-line ratings are given below.

$G_1$ :	90 MVA	20 kV	$X = 9\%$
$T_1$ :	80 MVA	20/200 kV	$X = 16\%$
$T_2$ :	80 MVA	200/20 kV	$X = 20\%$
$G_2$ :	90 MVA	18 kV	$X = 9\%$
Line:		200 kV	$X = 120 \Omega$
Load:		200 kV	$S = 48 \text{ MW} + j64 \text{ Mvar}$



**FIGURE 26**

One-line diagram for Problem 3.13

The base voltage  $V_{BG1}$  on the LV side of  $T_1$  is 20 kV. Hence the base on its HV side is

$$V_{B1} = 20 \left( \frac{200}{20} \right) = 200 \text{ kV}$$

This fixes the base on the HV side of  $T_2$  at  $V_{B2} = 200 \text{ kV}$ , and on its LV side at

$$V_{BG2} = 200 \left( \frac{20}{200} \right) = 20 \text{ kV}$$

The generator and transformer reactances in per unit on a 100 MVA base, from (3.69) and (3.70) are

$$G: \quad X = 0.09 \left( \frac{100}{90} \right) = 0.10 \text{ pu}$$

$$T_1: \quad X = 0.16 \left( \frac{100}{80} \right) = 0.20 \text{ pu}$$

$$T_2: \quad X = 0.20 \left( \frac{100}{80} \right) = 0.25 \text{ pu}$$

$$G_2: \quad X = 0.09 \left( \frac{100}{90} \right) \left( \frac{18}{20} \right)^2 = 0.081 \text{ pu}$$

The base impedance for the transmission line is

$$Z_{BL} = \frac{(200)^2}{100} = 400 \ \Omega$$

The per unit line reactance is

$$\text{Line:} \quad X = \left( \frac{120}{400} \right) = 0.30 \text{ pu}$$

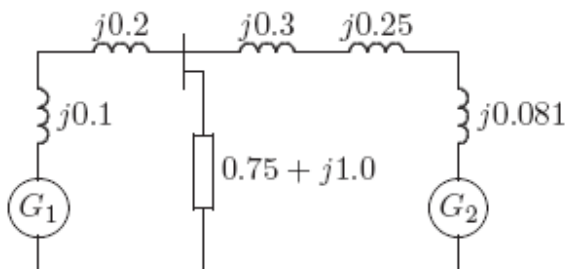
The load impedance in ohms is

$$Z_L = \frac{(V_{L-L})^2}{S_{L(3\phi)}^*} = \frac{(200)^2}{48 - j64} = 300 + j400 \ \Omega$$

The load impedance in per unit is

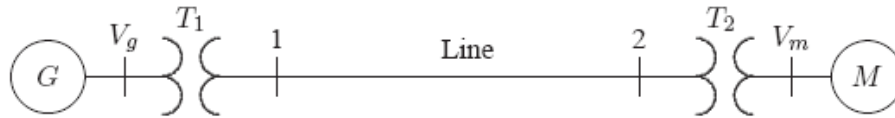
$$Z_{L(pu)} = \frac{300 + j400}{400} = 0.75 + j1.0 \text{ pu}$$

The per unit equivalent circuit is shown in Figure 27.



**FIGURE 27**  
Per unit impedance diagram for Problem 3.11.

3.15. The three-phase power and line-line ratings of the electric power system shown in Figure 30 are given below.



**FIGURE 30**  
One-line diagram for Problem 3.15

$G_1$ :	60 MVA	20 kV	$X = 9\%$
$T_1$ :	50 MVA	20/200 kV	$X = 10\%$
$T_2$ :	50 MVA	200/20 kV	$X = 10\%$
$M$ :	43.2 MVA	18 kV	$X = 8\%$
Line:		200 kV	$Z = 120 + j200 \Omega$

(a) Draw an impedance diagram showing all impedances in per unit on a 100-MVA base. Choose 20 kV as the voltage base for generator.

(b) The motor is drawing 45 MVA, 0.80 power factor lagging at a line-to-line terminal voltage of 18 kV. Determine the terminal voltage and the internal emf of the generator in per unit and in kV.

The base voltage  $V_{BG1}$  on the LV side of  $T_1$  is 20 kV. Hence the base on its HV side is

$$V_{B1} = 20 \left( \frac{200}{20} \right) = 200 \text{ kV}$$

This fixes the base on the HV side of  $T_2$  at  $V_{B2} = 200$  kV, and on its LV side at

$$V_{Bm} = 200 \left( \frac{20}{200} \right) = 20 \text{ kV}$$

The generator and transformer reactances in per unit on a 100 MVA base, from (3.69) and (3.70) are

$$G: \quad X = 0.09 \left( \frac{100}{60} \right) = 0.15 \text{ pu}$$

$$T_1: \quad X = 0.10 \left( \frac{100}{50} \right) = 0.20 \text{ pu}$$

$$T_2: \quad X = 0.10 \left( \frac{100}{50} \right) = 0.20 \text{ pu}$$

$$M: \quad X = 0.08 \left( \frac{100}{43.2} \right) \left( \frac{18}{20} \right)^2 = 0.15 \text{ pu}$$



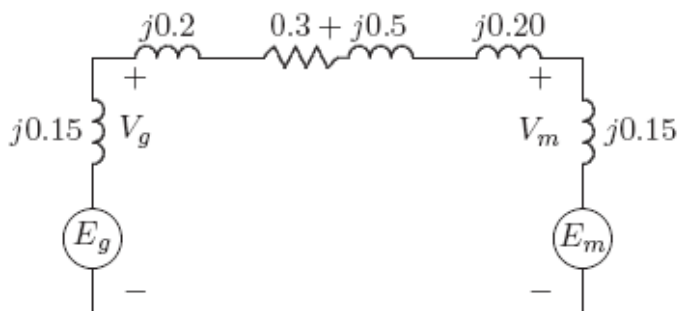
The base impedance for the transmission line is

$$Z_{BL} = \frac{(200)^2}{100} = 400 \ \Omega$$

The per unit line impedance is

$$\text{Line: } Z_{line} = \left( \frac{120 + j200}{400} \right) = 0.30 + j0.5 \text{ pu}$$

The per unit equivalent circuit is shown in Figure 31.



**FIGURE 31**

Per unit impedance diagram for Problem 3.15.

(b) The motor complex power in per unit is

$$S_m = \frac{45 \angle 36.87^\circ}{100} = 0.45 \angle 36.87^\circ \text{ pu}$$

and the motor terminal voltage is

$$V_m = \frac{18 \angle 0^\circ}{20} = 0.90 \angle 0^\circ \text{ pu}$$

$$I = \frac{0.45 \angle -36.87^\circ}{0.90 \angle 0^\circ} = 0.5 \angle -36.87^\circ \text{ pu}$$

$$V_g = 0.90 \angle 0^\circ + (0.3 + j0.9)(0.5 \angle -36.87^\circ) = 1.31795 \angle 11.82^\circ \text{ pu}$$

Thus, the generator line-to-line terminal voltage is

$$V_g = (1.31795)(20) = 26.359 \text{ kV}$$

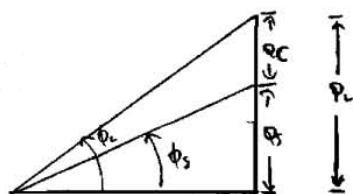
$$E_g = 0.90 \angle 0^\circ + (0.3 + j1.05)(0.5 \angle -36.87^\circ) = 1.375 \angle 13.88^\circ \text{ pu}$$

Thus, the generator line-to-line internal emf is

$$E_g = (1.375)(20) = 27.5 \text{ kV}$$

Extra Problems:

Problem # 1)



$$\phi_L = \cos^{-1} 0.7 = 45.57^\circ$$

$$Q_L = P \tan \phi_L = 1000 \tan (45.57^\circ)$$

$$Q_L = 1020.2 \text{ KVAR}$$

$$Q_S = \cos^{-1} 0.9 = 25.84^\circ$$

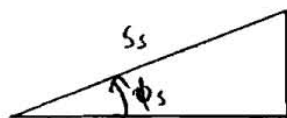
$$Q_S = P \tan \phi_S = 1000 \tan (25.84^\circ) = 484.3 \text{ KVAR}$$

$$Q_C = Q_L - Q_S = 1020.2 - 484.3 = 535.9 \text{ KVAR}$$

$$S_C = Q_C = 535.9 \text{ KVA}$$

b) Synchronous Motor Absorbs  $P_m = \frac{1000 \text{ hp} (0.746) \text{ kW}}{(0.9) (1 \text{ pf})} = 828.9 \text{ kW}$

and  $Q_m = 0 \text{ KVAR}$  (because of unity pf)



$$Q_S = Q_L = 1020.2 \text{ KVAR}$$

$$P_S = P + P_m = 1000 + 828.9 = 1828.9 \text{ kW}$$

$$\text{PF} = \cos \left[ \tan^{-1} \left( \frac{1020.2}{1828.9} \right) \right]$$

$$\text{PF} = 0.873 \text{ lagging}$$