

### Problem 1

A 9 kVA, 208 V, 1200 rpm, three phase, 60 Hz, Y-connected synchronous generator has a field winding resistance of  $4.5 \Omega$  and armature winding impedance of  $0.3 + j5 \Omega$  per phase. When the generator operates at its full load and 0.8 PF lagging, the field winding current is 5 A. The rotational loss is 500 W. Determine:

- The voltage regulation
- Efficiency
- The torque applied by the prime mover

Solution

$$V_{\phi} = \frac{208 \text{ V}}{\sqrt{3}} = 120 \text{ V}$$

$$I_a = \frac{S}{3 V_{\phi}} = \frac{9 \text{ kVA}}{3 \times 120} = 25 \text{ A}$$

→ For 0.8 PF lagging  $I_a = 25 \angle -36.87^\circ \text{ A}$

→ The Generated voltage  $E_A =$

$$\begin{aligned} E_A &= V_{\phi} + I_a (R_a + jX_s) \\ &= 120 \angle 0^\circ + 25 \angle -36.87^\circ [0.3 + j5] \\ &= 222.534 \angle 25.414^\circ \text{ V} \end{aligned}$$

$$(a) \quad \%R = \frac{V_{NL} - V_{FL}}{V_{FL}} \times 100\%$$

$$= \frac{222.534 - 120}{120} \times 100\% = 85.45\%$$

$$(b) \quad \eta = \frac{P_{out}}{P_{in}}$$

$$\begin{aligned} P_{out} &= 3 \sqrt{3} I_a \cos \theta \\ &= 3 \times 120 \times 25 \times 0.8 \\ &= 7.2 \text{ kW} \end{aligned}$$

$$\begin{aligned} \text{Copper loss} &= 3 \times I_a^2 R_a \\ &= 3 \times 25^2 \times 0.3 \\ &= 562.5 \text{ W} \end{aligned}$$

$$\text{Power developed: } P_{dev} = 7.2 \text{ kW} + 0.562 \text{ kW} = 7.76 \text{ kW}$$

$$\begin{aligned} \text{The constant loss} &= P_{rotational} + P_{field\ wdg} \\ &= 500 + 5^2 \times 4.5 = 0.6125 \text{ kW} \end{aligned}$$

$$\begin{aligned} \text{Total } P_{input} = P_{input} &= P_{out} + \text{losses} \\ &= 7.76 \text{ kW} + 0.6125 \text{ kW} = 8.375 \text{ kW} \end{aligned}$$

$$\eta = \frac{7.2 \text{ kW}}{8.375 \text{ kW}} = 0.86 = 86\%$$

$$\begin{aligned} (c) - P_{input(\text{mechanical})} &= P_{dev} + P_{rotational} \\ &= 7.76 \text{ kW} + 0.5 \text{ kW} = 8.263 \text{ kW} \end{aligned}$$

$$T_{pin} \times \omega = P_{in}$$

$$T_{pin} = \frac{P_{in}}{\omega} = \frac{8.263 \text{ kW}}{\frac{2\pi}{60} \times 1200} = 65.75 \text{ N-m}$$

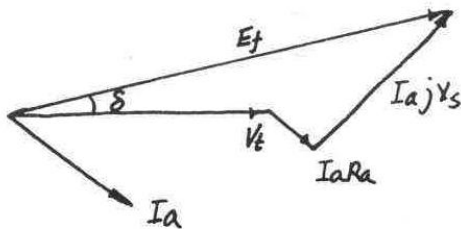
## Problem 2

A three phase, 14 kV, 10 MVA, 60 Hz, two pole, 0.85 PF lagging, star connected, synchronous generator has  $X_s = 20 \Omega$  per phase and  $R_a = 2 \Omega$  per phase. The generator is connected to an infinite bus.

- Determine the excitation voltage at the rated condition. Draw the phasor diagram for this condition.
- Determine the torque angle at the rated condition.
- If the field current is kept constant, determine the maximum power the generator can supply. Neglect  $R_a$ .
- For the condition in part (c), determine the generator current and the power factor. Draw the phasor diagram for this condition.

## Problem 2 Solution

$$(a) V_t |_{\text{rated}} = \frac{14 \times 10^3}{\sqrt{3}} = 8083 \text{ V/phase} \quad I_a |_{\text{rated}} = \frac{10 \times 10^6}{\sqrt{3} \times 14 \times 10^3} = 412.4 \text{ A}$$
$$\theta = \cos^{-1} 0.85 = 31.8^\circ$$
$$E_f = 8083 \angle 0^\circ + (412.4 \angle -31.8^\circ) \times 2 + (412.4 \angle -31.8^\circ) \times 20 \angle 90^\circ$$
$$= 8083 + 700 - j434.6 + 4346.3 + j7009.9 = 13129.3 + j6575.3 = 14,683.8 \angle 26^\circ \text{ V}$$

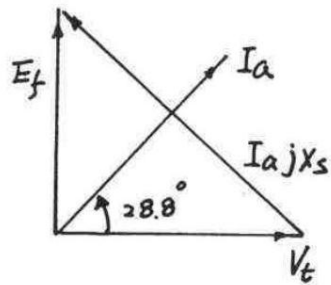


(b) The torque angle  $\delta = 26^\circ$

$$(c) P_{max} = \frac{3 \times 8083 \times 14683}{20} = 817.8 \text{ MW}$$

$$(d) I_a = \frac{14683 \angle 90^\circ - 8083 \angle 0^\circ}{20 \angle 90^\circ} = \frac{j14683 - 8083}{j20} = \frac{16760.83 \angle 118.8^\circ}{20 \angle 90^\circ} \\ = 838.04 \angle 28.8^\circ \text{ A}$$

$$\text{PF} = \cos 28.8^\circ = 0.876 \text{ (leading)}$$



### Problem 3

A three phase, 120 MVA, 12 kV, 60 Hz, two pole, 0.85 PF lagging, Y-connected steam turbine driven alternator(synchronous generator) has a stator resistance of  $R_a = 0.018 \Omega$  and a synchronous reactance of  $X_s = 1.02 \Omega$ . At full load (rated) condition, the efficiency is 92% (the field winding loss is neglected). At this condition, determine

- (a) The synchronous speed
- (b) The power loss in the armature resistance
- (c) The rotational loss (Neglect
- (d) The torque applied to the shaft by the steam turbine prime mover

$$(a) \quad \omega_s = \frac{120 * 60}{2} = 3600 \text{ rpm}$$

$$V_\phi = \frac{12 \text{ kV}}{\sqrt{3}} = 6928.4 \text{ V}$$

$$I_a = \frac{120 \text{ MVA}}{6928.4 \text{ V}} = 5773.7 \text{ A}$$

$$(b) \quad P_{Ra} = 3 * I_a^2 R_a = 3 * 5773.7^2 * 0.018 = 1.8 \text{ MW}$$

$$P_{out} = 120 * 0.85 = 102 \text{ MW}$$

$$\text{Turbine power } P_{in} = \frac{102}{0.92} = 110.8696 \text{ MW}$$

$$\text{Total loss} = 110.8696 - 102 = 8.896 \text{ MW}$$

$$(c) \quad \text{Rotational loss} = 8.896 - 1.8 = 7.0696 \text{ MW}$$

$$(d) \quad \text{Torque} = \frac{110.8696 \text{ MW}}{(3600 * 2\pi) / 60} = 294.09 \text{ kN} - \text{M}$$

### Problem 4

A 208-V Y-connected synchronous motor is drawing 40 A at unity power factor from a 208-V power system. The field current flowing under these conditions is 2.7 A. Its synchronous reactance is  $0.8 \Omega$ . Assume a linear open-circuit characteristic.

- Find the torque angle  $\delta$ .
- How much field current would be required to make the motor operate at 0.8 PF leading?
- What is the new torque angle in part (b)?

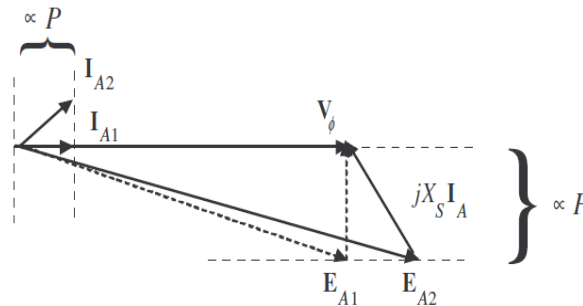
SOLUTION

(a) The phase voltage of this motor is  $V_\phi = 120 \text{ V}$ , and the armature current is  $\mathbf{I}_A = 40\angle 0^\circ \text{ A}$ . Therefore, the internal generated voltage is

$$\begin{aligned} \mathbf{E}_A &= \mathbf{V}_\phi - R_A \mathbf{I}_A - jX_S \mathbf{I}_A \\ \mathbf{E}_A &= 120\angle 0^\circ \text{ V} - j(0.8 \Omega)(40\angle 0^\circ \text{ A}) \\ \mathbf{E}_A &= 124\angle -14.9^\circ \text{ V} \end{aligned}$$

The torque angle  $\delta$  of this machine is  $-14.9^\circ$ .

(b) A phasor diagram of the motor operating at a power factor of 0.78 leading is shown below.



Since the power supplied by the motor is constant, the quantity  $I_A \cos \theta$ , which is directly proportional to power, must be constant. Therefore,

$$I_{A2}(0.8) = (40 \text{ A})(1.00)$$

$$\mathbf{I}_{A2} = 50\angle 36.87^\circ \text{ A}$$

The internal generated voltage required to produce this current would be

$$\mathbf{E}_{A2} = \mathbf{V}_\phi - R_A \mathbf{I}_{A2} - jX_S \mathbf{I}_{A2}$$

$$\mathbf{E}_{A2} = 120\angle 0^\circ \text{ V} - j(0.8 \Omega)(50\angle 36.87^\circ \text{ A})$$

$$\mathbf{E}_{A2} = 147.5\angle -12.5^\circ \text{ V}$$

The internal generated voltage  $E_A$  is directly proportional to the field flux, and we have assumed in this problem that the flux is directly proportional to the field current. Therefore, the required field current is

$$I_{F2} = \frac{E_{A2}}{E_{A1}} I_{F1} = \frac{147 \text{ V}}{124 \text{ V}} (2.7 \text{ A}) = 3.20 \text{ A}$$

(c) The new torque angle  $\delta$  of this machine is  $-12.5^\circ$ .

### Problem 5

A 480-V, 100-kW, 50-Hz, four-pole, Y-connected synchronous motor has a rated power factor of 0.85 leading. At full load, the efficiency is 91%. The armature resistance is  $0.08 \Omega$ , and the synchronous reactance is  $1.0 \Omega$ . Find the following quantities for this machine when it is operating at full load:

- (a) Output torque
- (b) Input power
- (c)  $n_m$  (Mechanical speed of the machine)
- (d)  $E_A$
- (e)  $|\mathbf{I}_A|$
- (f)  $P_{\text{conv}}$
- (g) Rotational loss =  $P_{\text{mech}} + P_{\text{core}} + P_{\text{stray}}$

SOLUTION

(a) Since this machine has 8 poles, it rotates at a speed of

$$n_m = \frac{120f_e}{P} = \frac{120(50 \text{ Hz})}{4} = 1500 \text{ r/min}$$

If the output power is 100 kW, the output torque is

$$\tau_{\text{load}} = \frac{P_{\text{out}}}{\omega_m} = \frac{(100,000 \text{ W})}{(1500 \text{ r/min}) \frac{2\pi \text{ rad}}{1 \text{ r}} \frac{1 \text{ min}}{60 \text{ s}}} = 637 \text{ N} \cdot \text{m}$$

(b) The input power is

$$P_{\text{IN}} = \frac{P_{\text{OUT}}}{\eta} = \frac{100 \text{ kW}}{0.91} = 110 \text{ kW}$$

(c) The mechanical speed is

$$n_m = 1500 \text{ r/min}$$

(d) The armature current is

$$I_A = I_L = \frac{P}{\sqrt{3} V_T \text{ PF}} = \frac{110 \text{ kW}}{\sqrt{3}(480 \text{ V})(0.85)} = 156 \text{ A}$$

$$\mathbf{I}_A = 156 \angle 31.8^\circ \text{ A}$$

Therefore,  $\mathbf{E}_A$  is

$$\mathbf{E}_A = \mathbf{V}_\phi - R_A \mathbf{I}_A - jX_s \mathbf{I}_A$$

$$\mathbf{E}_A = (277 \angle 0^\circ \text{ V}) - (0.08 \Omega)(156 \angle 31.8^\circ \text{ A}) - j(1.0 \Omega)(156 \angle 31.8^\circ \text{ A})$$

$$\mathbf{E}_A = 375 \angle -21.8^\circ \text{ V}$$

(e) The magnitude of the armature current is 375 A.

(f) The power converted from electrical to mechanical form is given by the equation  $P_{\text{conv}} = P_{\text{IN}} - P_{\text{CU}}$

$$P_{\text{CU}} = 3I_A^2 R_A = 3(156 \text{ A})^2 (0.08 \Omega) = 5.8 \text{ kW}$$

$$P_{\text{conv}} = P_{\text{IN}} - P_{\text{CU}} = 110 \text{ kW} - 5.8 \text{ kW} = 104.2 \text{ kW}$$

(g) The mechanical, core, and stray losses are given by the equation

$$P_{\text{mech}} + P_{\text{core}} + P_{\text{stray}} = P_{\text{conv}} - P_{\text{OUT}} = 104.2 \text{ kW} - 100 \text{ kW} = 4.2 \text{ kW}$$