

Solution Problem 1

a) Machine constant K_a

$$\phi = 15 \text{ mwb} \quad Z = 330 \quad p = 4 \quad a = 2$$

$$K_a = \frac{Zp}{2\pi a} = \frac{330 \times 4}{2\pi \times 2} = 105.04$$

b) Generated voltage E_a

$$E_a = K_a \phi \omega_m$$
$$= 105.04 \times 15 \times 10^{-3} \times \frac{1150 \times 2\pi}{60}$$

$$E_a = 189.74 \text{ V}$$

c) Conductor current I_c

Since, the armature is wave connected.

$$\text{Conductor current } I_c = \frac{I_a}{a} = 125 \text{ A.}$$

d) Electromagnetic torque T_e

$$T_e = K_a \phi I_a$$
$$= 105.04 \times 15 \times 10^{-3} \times 250$$

$$T_e = 393.99 \text{ N-m}$$

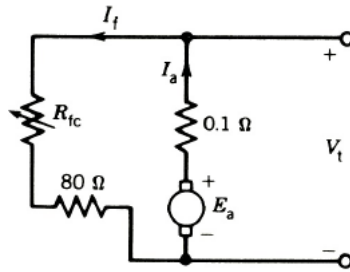
e) Power developed, P_{dev} , by the armature

$$P_{dev} = E_a I_a$$
$$= 189.74 \times 250$$

$$P_{dev} = 47.43 \text{ kW}$$

Solutions HW4
EE306 171

Solution Problem 2



- (a) The maximum voltage will be generated at the lowest value of the field circuit resistance, $R_{fc} = 0$. Draw a field resistance line (see Fig. 3 provided) for $R_f = R_{fw} = 80 \Omega$. The maximum generated voltage is

$$E_a = 111 \text{ volts}$$

- (b)

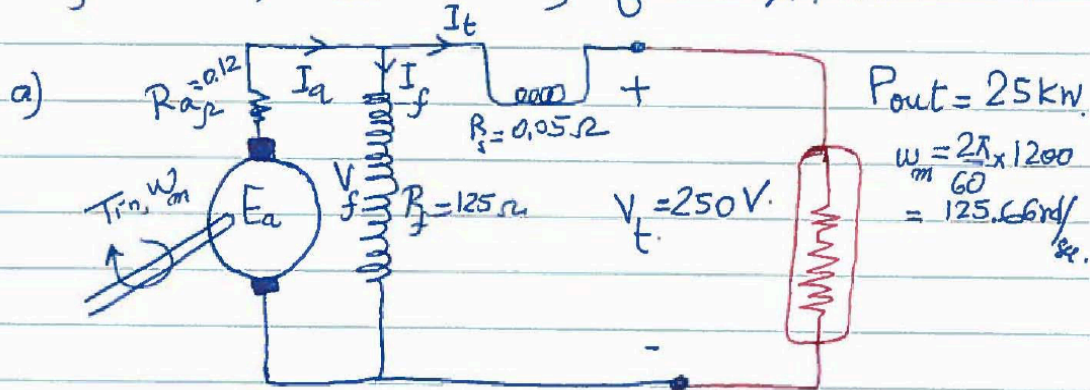
$$\begin{aligned} V_t &= E_a - I_a R_a \\ &\simeq E_a \\ &= 100 \text{ V} \end{aligned}$$

Draw a field resistance line that intersects the magnetization curve at 100 V (see Fig. 3 provided). For this case,

$$\begin{aligned} I_f &= 1 \text{ A} \\ R_f &= \frac{100}{1} = 100 \Omega = R_{fw} + R_{fc} \\ R_{fc} &= 100 - 80 = 20 \Omega \end{aligned}$$

Solution Problem 3

$p=6$, Short Shunt Compound Generator.
 $\omega = 1200 \text{ rpm}$, $R_f = 250$, $V_t = 250 \text{ V}$, $R_a = 0.12 \Omega$,
 $R_f = 125 \Omega$, $R_s = 0.05 \Omega$, $\eta_g = 82\%$, $P_{out} = 25 \text{ kW}$



b)

$$\eta = \frac{P_{out}}{P_{in}} \times 100\% \Rightarrow P_{in} = \frac{P_{out}}{\eta} = \frac{25}{0.82} = 30.488 \text{ kW}$$

$$P_{in} = T_{in} \omega \Rightarrow T_{in} = \frac{P_{in}}{\omega} = \frac{30.488 \times 10^3}{125.66} = 242.65 \text{ N.m}$$

c)

$$P_{dev} = E_a I_a, \quad I_t = \frac{P_{out}}{V_t} = \frac{25 \times 10^3}{250} = 100 \text{ A}$$

$$E_a = V_f + I_a R_a, \quad V_f = V_t + I_t R_s = 250 + (100)(0.05)$$

$$V_f = 255 \text{ V}$$

$$I_f = \frac{V_f}{R_f} = \frac{255}{125} = 2.04 \text{ A}, \quad I_a = I_f + I_t = 2.04 + 100 = 102.04 \text{ A}$$

$$I_a = 102.04 \text{ A}, \quad E_a = 255 + (102.04)(0.12) = 267.2448 \text{ V}$$

$$P_{dev} = (267.2448)(102.04) = 27.26965 \text{ kW}$$

$$T_{dev} = \frac{P_{dev}}{\omega} = \frac{27.269.65}{125.66} =$$

$$T_{dev} = 217.011 \text{ N.m}$$

Solution Problem 4

DC Shunt motor

$$R_a = 0.1 \Omega$$

$$R_f = 120 \Omega$$

$$V_t = 120 V$$

$$I_L = 41 A$$

$$V_{\text{brush}} = 2 V$$

$$\omega_m = 200 \text{ rad/sec}$$

a. $I_L = I_a + I_f$

$$I_f = \frac{V_t}{R_f} = \frac{120 V}{120 \Omega} = 1 A$$

$$I_a = I_L - I_f = 41 - 1 = 40 A$$

$$V_t = E_a + I_a R_a + 2 V$$

b. $E_a = V_t - I_a R_a - 2 V$
 $= 120 - 40 * 0.1 - 2 = 114 V$

$$P_{dev} = E_a * I_a$$
$$= 114 * 40 = 4.56 kW$$

$$P_{dev} = T_{dev} * \omega_m$$

$$T_{dev} = \frac{P_{dev}}{\omega_m} = \frac{4.56 kW}{200 \text{ rad/sec}} = 22.8 N-M$$

Solution Problem 5

(a)

$$T = k_1 \times \emptyset \times i = k_2 \times i^2$$

$$\frac{T_1}{T_2} = 0.5 = \frac{i^2}{75^2}$$

$$i^2 = 0.5 \times 75^2 = 2812.5$$

$$i = 53.03 \text{ A}$$

(b)

$$E_{a1} = 600 - 75 \times 0.5 = 600 - 37.5 = 562.5 \text{ V}$$

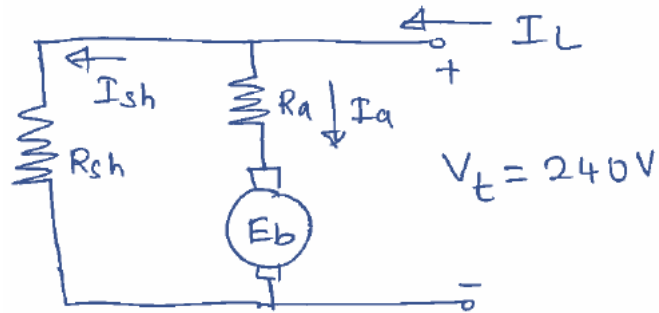
$$E_{a2} = 600 - 53.03 \times 0.5 = 600 - 26.52 = 573.5 \text{ V}$$

$$\frac{n_2}{n_1} = \frac{573.5 \times 75}{562.5 \times 53.03} = 1.44$$

$$n_2 = 1.44 \times 500 = 720.97 \text{ rpm}$$

Solution Problem 6

(a)



(b)

No-Load operating condition:-

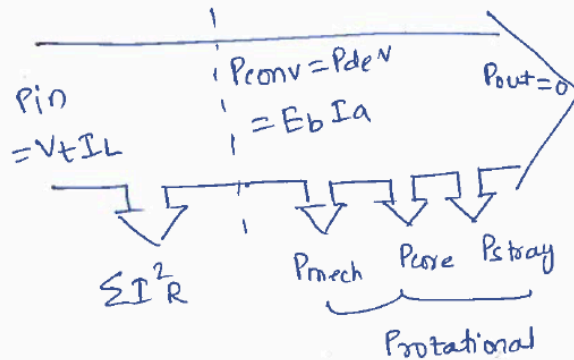
$$P_{rot} = P_{in, NL} - \sum I^2 R \text{ (OR)}$$

$$P_{rot} = P_{conv} = E_b I_{a, NL}$$

Given $I_{L, NL} = 9A$

$$I_{sh, NL} = \frac{V_t}{R_{sh}} = \frac{240}{120} = 2A$$

$$\Rightarrow I_{a, NL} = I_{L, NL} - I_{sh, NL} = 9 - 2 = 7A$$



By KVL,

$$E_{b, NL} = V_t - I_{a, NL} R_a - V_{BY}$$

$$= 240 - 7 \times 0.3 = 237.9V$$

Solutions HW4
EE306 171

$$\text{Now } P_{\text{rot}} = E_{b,NL} \cdot I_{a,NL} \\ = 237.9 \times 7$$

$$P_{\text{rot}} = 1665.3 \text{ W}$$

Full-load operating condition:-

$$P_{\text{in}} = 12 \text{ kW}$$

$$P_{\text{cu}} = \sum I^2 R = I_a^2 R_a + I_{\text{sh}}^2 R_{\text{sh}}$$

$$\text{From, } V_t I_L = 12 \times 10^3 \\ \Rightarrow I_L = \frac{12 \times 10^3}{240} = 50 \text{ A}$$

$$P_{\text{cu}} = (48)^2 \times 0.3 + 2^2 \times 120 =$$

$$P_{\text{cu}} = 1171.2 \text{ W}$$

Now, Efficiency

$$\eta = \frac{P_{\text{in}} - P_{\text{cu}} - P_{\text{rot}}}{P_{\text{in}}} \times 100$$

$$= \frac{12000 - 1665.3 - 1171.2}{12000} \times 100$$

$$\eta = 76.36 \%$$

P:

Solutions HW4
EE306 171

Solution Problem 7

(a)

SOLUTION At no-load conditions, $E_A = V_T = 240 \text{ V}$. The field current is given by

$$I_F = \frac{V_T}{R_{\text{adj}} + R_F} = \frac{240 \text{ V}}{175 \Omega + 75 \Omega} = \frac{240 \text{ V}}{250 \Omega} = 0.960 \text{ A}$$

From Fig.5, this field current would produce an internal generated voltage E_{Ao} of 241 V at a speed n_o of 1200 r/min. Therefore, the speed n with a voltage E_A of 240 V would be

$$\frac{E_A}{E_{Ao}} = \frac{n}{n_o}$$
$$n = \left(\frac{E_A}{E_{Ao}} \right) n_o = \left(\frac{240 \text{ V}}{241 \text{ V}} \right) (1200 \text{ r/min}) = 1195 \text{ r/min}$$

(b)

SOLUTION At full load, the armature current is

$$I_A = I_L - I_F = I_L - \frac{V_T}{R_{\text{adj}} + R_F} = 110 \text{ A} - \frac{240 \text{ V}}{250 \Omega} = 109 \text{ A}$$

The internal generated voltage E_A is

$$E_A = V_T - I_A R_A = 240 \text{ V} - (109 \text{ A})(0.19 \Omega) = 219.3 \text{ V}$$

The field current is the same as before, and there is no armature reaction, so E_{Ao} is still 241 V at a speed n_o of 1200 r/min. Therefore,

$$n = \left(\frac{E_A}{E_{Ao}} \right) n_o = \left(\frac{219.3 \text{ V}}{241 \text{ V}} \right) (1200 \text{ r/min}) = 1092 \text{ r/min}$$

The speed regulation is

$$\text{SR} = \frac{n_{\text{nl}} - n_{\text{fl}}}{n_{\text{fl}}} \times 100\% = \frac{1195 \text{ r/min} - 1092 \text{ r/min}}{1092 \text{ r/min}} \times 100\% = 9.4\%$$