

Problem-1:-

(1)

Given :- 25 kVA 1-Phase transformer

$$a = \frac{2400}{240} = 10$$

Measurement of open-circuit test are taken at the Secondary side.

$$V_{oc_s} = 240 \text{ V} \quad I_{oc_s} = 3.2 \text{ A} \quad P_{oc_s} = 165 \text{ W}$$

$$PF = \frac{P_{oc_s}}{V_{oc_s} I_{oc_s}} = \frac{165}{240 \times 3.2} = 0.2148$$

$$\Rightarrow \theta_{oc} = \cos^{-1}(0.2148) = 77.59^\circ$$

Shunt excitation admittance

$$|Y_{oc_s}| = \frac{I_{oc_s}}{V_{oc_s}}$$

$$= \frac{3.2}{240} = 0.01333 \text{ S}$$

$$\therefore Y_{oc_s} = 0.01333 \angle -77.59^\circ \text{ S}$$

$$\Rightarrow Y_{oc_s} = 0.002865 - j0.0130021$$

$$\Rightarrow R_{c_s} = \frac{1}{0.002865} = 349.65 \Omega$$

$$X_{m_s} = \frac{1}{0.0130021} = 76.796 \Omega$$

The excitation elements are now referred to the primary side as

$$R_{cp} = a^2 R_{cs} = (10)^2 (349.65) = 34.904 \text{ k}\Omega$$

$$X_{mp} = a^2 X_{ms} = (10)^2 (76.796) = 7.6796 \text{ k}\Omega$$

The measurement of short-circuit test are taken on the primary side.

$$P_{scp} = 375 \text{ W} \quad V_{scp} = 55 \text{ V} \quad I_{scp} = 10.4 \text{ A}$$

Compute  $I_p^{\text{rated}}$

$$I_p^{\text{rated}} = \frac{S_{\text{rated}}}{V_p} = \frac{25 \times 10^3}{2400} = 10.4 \text{ A}$$

Hence the short-circuit test is carried on full-load primary current.

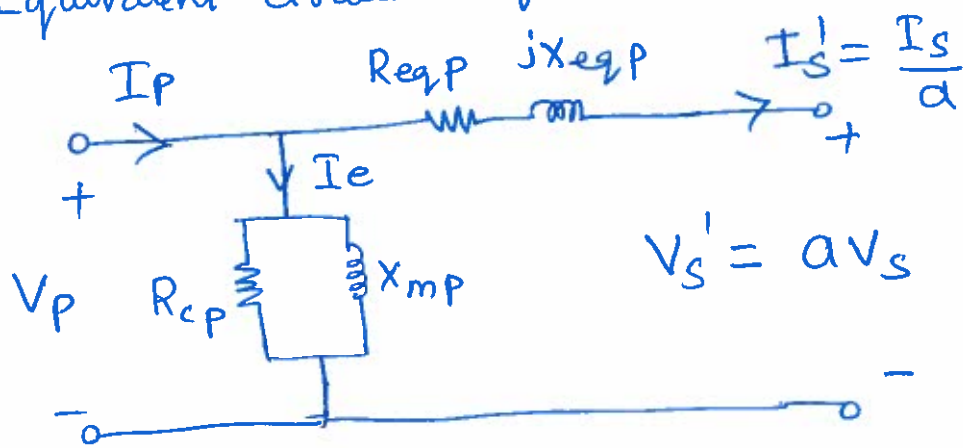
$$\text{Now } PF = \frac{P_{scp}}{V_{scp} \cdot I_{scp}} = \frac{375}{55 \cdot 10.4} = 0.65559$$

$$\Rightarrow \theta = \cos^{-1}(0.65559) = 49.035^\circ$$

$$Z_{scp} = \frac{V_{scp} \angle \theta}{I_{scp}} = \frac{55 \angle 49.035^\circ}{10.4}$$

$$Z_{scp} = 3.467 + j3.993 \Omega$$

Equivalent circuit referred to the primary side



(b)  $\cos\theta = 0.85$  lagging

$$P_{out} = 25 \times 0.85 = 21.25 \text{ kW}$$

$$\theta_s = \cos^{-1}(0.85) = 31.788^\circ$$

$$\begin{aligned} \text{Now } \bar{I}_s &= \frac{P_{out} (= P_s)}{V_s \cos\theta_s} \\ &= \frac{21.25 \times 10^3}{240 \times 0.85} \end{aligned}$$

$$\bar{I}_s = 104.166 \text{ A}$$

$$\therefore \bar{I}_s = 104.166 \angle -31.788^\circ \text{ A}$$

$$\text{Now, } \bar{V}_p = \bar{V}_s' + \bar{I}_s (R_{eqP} + jX_{eqP})$$

(4)

$$= aV_s + \frac{P_s}{a} (R_{eqp} + jX_{eqf})$$

$$= (10)(240\angle 0^\circ) + \frac{104.166}{10} \angle -31.788^\circ (3.467 + j3.993)$$

$$V_p = 2452.66 \angle 0.381^\circ \text{ V}$$

$$\therefore V_{\text{regulation}} = \frac{(|V_p| - |V_s'|)}{|V_s'|} \times 100$$

$$= \frac{2452 - (10)(2400)}{(10)(2400)} \times 100$$

$$= 2.194 \%$$

Efficiency :

$$\eta = \frac{P_{\text{out}}}{P_{\text{in}}} \times 100 \%$$

$$= \frac{P_{\text{out}}}{P_{\text{out}} + P_{\text{cu}} + P_{\text{core}}} \times 100 \%$$

$$P_{\text{core}} = \frac{|V_P|^2}{R_{CP}} = \frac{(2452.66)^2}{34.904 \times 10^3} = 172.345 \text{ W} \quad (5)$$

$$P_{cu} = I_s'^2 \cdot R_{eqP}$$
$$= \left( \frac{104.166}{10} \right)^2 \cdot 3.47$$

$$P_{cu} = 376.188 \text{ W}$$

$$P_{in} = 376.188 + 172.343 + 21250$$

---

$$= 21798.53 \text{ W}$$

$$\eta = \frac{21250}{21798.53} \times 100$$

$$\eta = 97.48\%$$

C. Condition for max. efficiency,  $P_{core} = P_{cu}$  &  $PF = 1$

$$P_{core} = P_{cu} = 165 \text{ W} = I_s^2 R_{e\%s} \quad , \quad R_{e\%s} = \frac{3.467}{100} = 0.03467$$

$$I_s = \sqrt{\frac{165}{0.03467}} = 68.98 \text{ A}$$

Power output at  $\eta_{max}$

$$P_{out} = V_s I_s \cos \phi_s$$

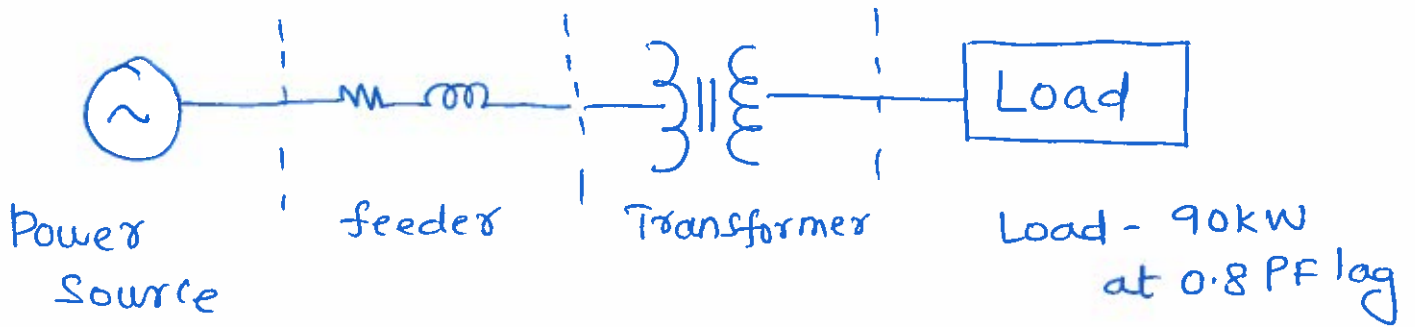
$$= 240 \times 68.98 = 16.556 \text{ kW}$$

$$\eta_{max} = \frac{P_{out}}{P_{out} + 2P_c} = \left( \frac{16.556 \text{ kW}}{16.556 \text{ kW} + 2(165)} \right) * 100\%$$

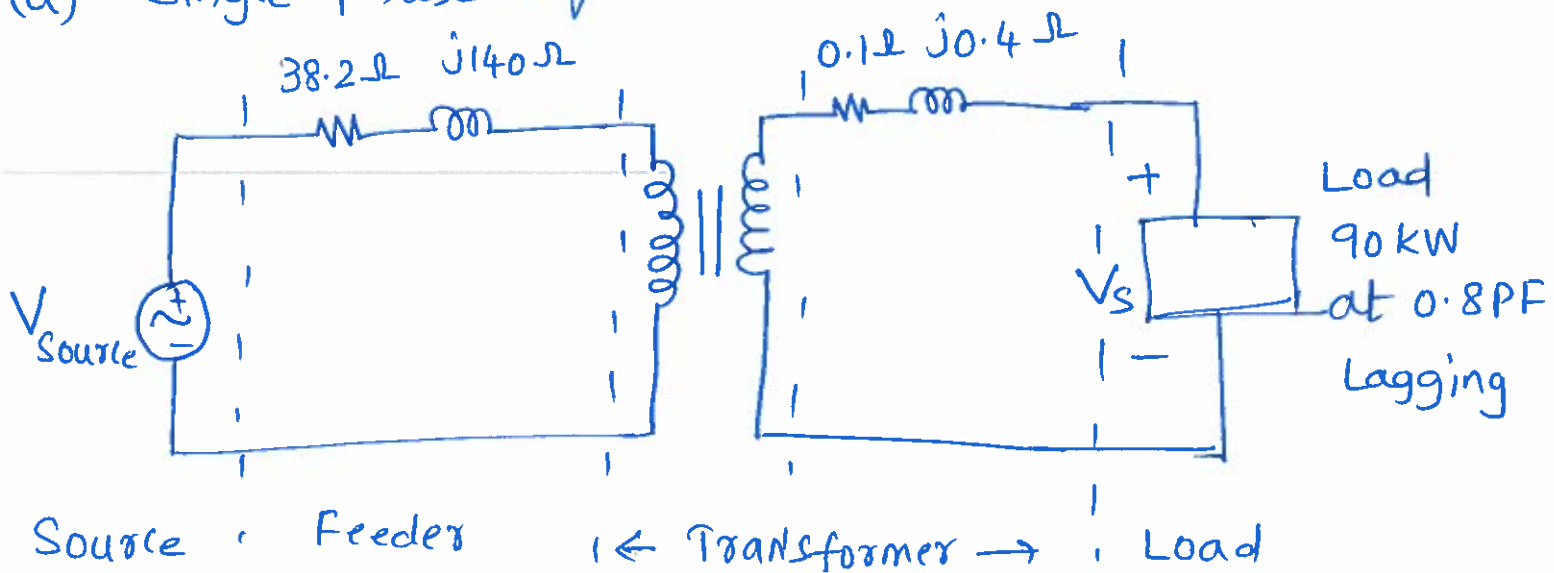
$$= \underline{\underline{98.04\%}}$$

Problem-2 :-

Single-phase distribution system



(a) Single-phase equivalent circuit of the power-system



(b) To solve this problem, we will refer the circuit to the secondary (low-voltage) side.

The feeder impedance referred to the secondary side is

$$Z_{line} = (38.2 + j140) \Omega$$

$$a = \frac{14 \text{ kV}}{2.4 \text{ kV}}$$

$$Z'_{line} = \frac{(38.2 + j146) \Omega}{a^2}$$

$$Z'_{line} = (1.12 + j4.11) \Omega$$

To compute the Secondary current  $I_s$

$$P_s = V_s I_s \cos \theta_s$$

$$I_s = \frac{P_s}{V_s \cos \theta_s}$$

---


$$= \frac{90 \times 10^3}{(2400)(0.8)} = 46.88 \text{ A}$$

$$\therefore \bar{I}_s = 46.88 \angle -\cos^{-1}(\text{PF})$$

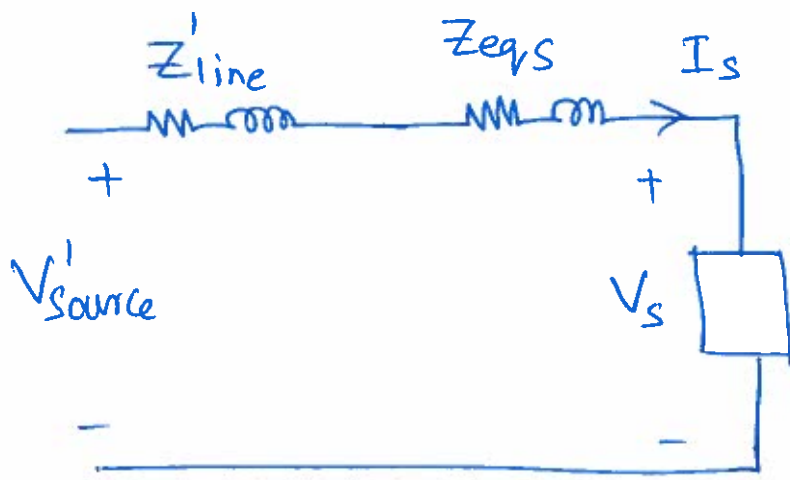
$$\bar{I}_s = 46.88 \angle -36.87^\circ \text{ A}$$

The voltage at the power source of this system (referred to the secondary side) is

$$V'_{source} = V_s + I_s Z'_{line} + I_s Z_{eqs}$$

Taking  $V_s = 2400 \angle 0^\circ \text{ V}$  as reference





$$V'_{source} = V_s + I_s (Z'_{line} + Z_{eqs})$$

$$= 2400 \angle 0^\circ + 46.88 \angle -36.87^\circ (1.12 + j4.11 + 0.1 + j0.4)$$

---


$$V'_{source} = 2576 \angle 3.0^\circ \text{ V}$$

$\therefore$  The voltage at the power source is

$$V_{source} = V'_{source} \cdot a$$

$$= (2576 \angle 3.0^\circ) \left( \frac{14 \text{ kV}}{2.4 \text{ kV}} \right)$$

$$V_{source} = 15.5 \angle 3.0^\circ \text{ kV}$$

(c) To find the voltage regulation of the transformer we must find the voltage at the primary side of the transformer (referred to the secondary side).

$$V_p' = V_s + I_s Z_{eqs}$$

$$= 2400 \angle 0^\circ + (46.88 \angle -36.87^\circ) (0.1 + j0.4)$$

$$V_p' = 2415 \angle 0.3^\circ \text{ V}$$

$\therefore$  voltage regulation is

$$VR = \frac{|V_p'| - |V_s|}{|V_s|} \times 100$$

$$= \frac{2415 - 2400}{2400} \times 100$$

$$VR = 0.63\%$$

(d) The overall efficiency of the power system will be the ratio of the output power to the input power.

$$\begin{aligned} \text{The output power} &= \text{power supplied to the load} \\ &= 90 \text{ kW} \end{aligned}$$

$$\text{input power } P_{in} = P_{out} + P_{loss}$$

(5)

$$P_{in} = P_{out} + P_{loss}$$

$$= P_{out} + I^2 R$$

$$= (90 \times 10^3) + (46.88)^2 (1.22)$$

$$P_{in} = 92.68 \text{ kW}$$

Therefore the efficiency of the power system is

$$\eta = \frac{P_{out}}{P_{in}} \times 100 \%$$

$$= \frac{90 \times 10^3}{92.68 \times 10^3} \times 100 \%$$

$$\eta = 97.1 \%$$

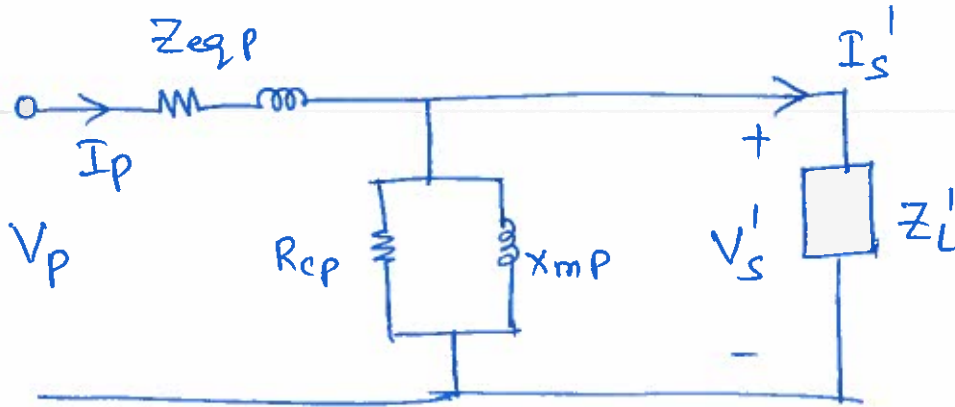
Problem-3:-

$$\text{Turns ratio } a = \frac{8000}{230} = 34.78$$

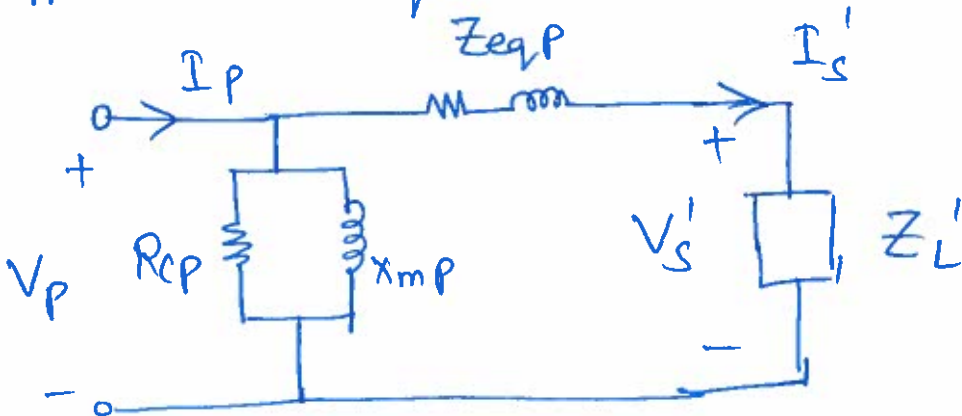
$$Z_{eqP} = (20 + j100) \Omega$$

$$R_{cp} = 100 \text{ k}\Omega \quad X_{mp} = 20 \text{ k}\Omega$$

(a) Equivalent circuit referred to the primary side



Approximate equivalent circuit,



The load impedance referred to the primary side,

(2)

$$Z_L' = a^2 Z_L$$

$$Z_L' = (34.78)^2 (2.0 + j0.7) = 2419 + j847 \Omega$$

The referred secondary current,

$$I_s' = \frac{V_P}{Z_{eqp} + Z_L'}$$

$$= \frac{7967 \angle 0^\circ}{(20 + j100) + (2419 + j847)}$$

$$I_s' = 3.045 \angle -21.2^\circ \text{ A}$$

The referred secondary voltage is,

$$V_s' = I_s' Z_L' = (3.045 \angle -21.2^\circ) (2419 + j847)$$

$$V_s' = 7804 \angle -1.9^\circ \text{ V}$$

The actual secondary voltage is

$$V_s = \frac{V_s'}{a} = \frac{7804 \angle -1.9^\circ}{34.78} = 224.4 \angle -1.9^\circ \text{ V}$$

The voltage regulation is

(3)

$$V_R = \frac{|V_P| - |V_S'|}{|V_S'|} \times 100 \%$$
$$= \frac{7967 - 7804}{7804} \times 100 \%$$

$$V_R = 2.09 \%$$

(b) Now the load is disconnected. Connect a capacitor with  $Z_L = -j3.0 \Omega$  as load.

The load impedance referred to the primary side is

$$Z_L' = a^2 Z_L = (34.78)^2 (-j3.0) = -j3629 \Omega$$

The referred secondary current is

$$I_s' = \frac{V_P}{Z_L' + Z_{eqp}}$$
$$= \frac{7967 \angle 0^\circ}{(-j3629) + (20 + j100)}$$

$$I_s' = 2.258 \angle 89.7^\circ \text{ A}$$

The referred Secondary voltage is

$$V_S' = I_S' z_L' = (2.258 \angle 89.7^\circ) (-j3629)$$

$$V_S' = 8194 \angle -0.3^\circ \text{ V}$$

The actual secondary voltage is

$$V_S = \frac{V_S'}{a} = \frac{8194 \angle -0.3^\circ}{34.78} = 235.6 \angle -0.3^\circ \text{ V}$$

The voltage regulation is

$$V_R = \frac{|V_P| - |V_S'|}{|V_S'|} \times 100\%$$

$$= \frac{7967 - 8194}{8194} \times 100\%$$

$$V_R = -10.6\%$$

### Problem 4

Turns ratio:  $a = \frac{2200}{220} = 10$

a-  $R_{esp} = R_p + a^2 R_s = 4 + 10^2 \times 0.04 = 8 \Omega$

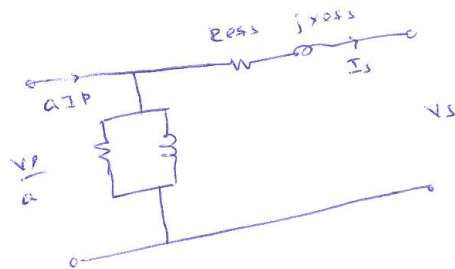
$X_{esp} = X_p + a^2 X_s = 5 + 10^2 \times 0.05 = 10 \Omega$

$Z_{esp} = (8 + j10) \Omega$  - Total series impedance referred to HV side

$Z_{ess} = (0.08 + j0.1) \Omega$  - Total series impedance referred to LV side

b-  $I_s = \frac{10,000}{220} = 45.45$ ,  $\phi = -\cos 0.8 = -36.87^\circ$

$I_s = 45.45 \angle -36.87^\circ$



$\frac{V_p}{a} = V_s + I_s (R_{ess} + jX_{ess})$

$= 220 \angle 0^\circ + 45.45 \angle -36.87^\circ [0.08 + j0.1] = 225.64 \angle 0.36^\circ$

Voltage Regulation  $\%VR = \frac{\frac{V_p}{a} - V_s}{V_s} \times 100\%$

$= \frac{225.64 - 220}{220} \times 100\% = 2.56\%$

c-  $\frac{V_p}{a} = 220 \angle 0^\circ + 45.45 \angle 36.87^\circ [0.08 + j0.1] = 220.258 \angle 1.51^\circ$

$\%VR = \frac{220.258 - 220}{220} \times 100\% = 0.1173\%$



$$d - P_c = 80 \text{ W}$$

$$P_{cu} = I_s^2 R_{efs} = 45.45^2 \times 0.08 \\ = 165.25 \text{ W}$$

$$P_{out} = 10 \times 0.8 = 8 \text{ kW}$$

$$\eta = \frac{P_{out}}{P_{out} + P_{cu} + P_c} = \frac{8000 \text{ W}}{8000 \text{ W} + 80 \text{ W} + 165.25 \text{ W}} \times 100 \% \\ = 97.025 \%$$

It will be the same, because the magnitude of the load current is the same.