

Problem 4.18

Using Gauss's law in differential form: $\nabla \vec{D} = \rho_v$

a) In rectangular coordinates $\rho_v = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z} \Rightarrow \rho_v = 8y + 0 = 8y$

b) In cylindrical coordinates $\rho_v = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z}$

$$\Rightarrow \rho_v = \frac{1}{\rho} \frac{\partial}{\partial \rho} (4\rho^2 \sin \phi) + \frac{1}{\rho} \frac{\partial (2\rho \cos \phi)}{\partial \phi} + \frac{\partial (2z^2)}{\partial z} \Rightarrow \rho_v = 8 \sin \phi - 2 \sin \phi + 4z$$

c) In spherical coordinates $\rho_v = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (D_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial D_\phi}{\partial \phi}$

$$\Rightarrow \rho_v = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \frac{2 \cos \theta}{r^3}) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\frac{\sin \theta}{r^3} \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial 0}{\partial \phi}$$

$$= \frac{1}{r^2} 2 \cos \theta (-r^{-2}) + \frac{1}{r^4 \sin \theta} (2 \sin \theta \cos \theta)$$

$$= -\frac{2 \cos \theta}{r^4} + \frac{2 \cos \theta}{r^4}$$

$$\therefore \rho_v = 0$$

Problem 4.22

$$a) \rho_v = \frac{\partial(2xy)}{\partial x} + \frac{\partial(x^2)}{\partial y} + \frac{\partial(0)}{\partial z} = 2y$$

$$b) \psi = \int_S \vec{D} \cdot d\vec{s} \Rightarrow \psi = \int_S \vec{D} \cdot (dx dz \vec{a}_y) = \int_S D_y dx dz = \int_{x=0}^1 \int_{z=0}^1 x^2 dx dz$$

$$\therefore \psi = \frac{1}{3} C / m^3$$

c) Method 1: Using $Q = \int_V \rho_v dv$

$$Q = \int_{x=0}^1 \int_{y=0}^1 \int_{z=0}^1 (2y) dx dy dz = 1C$$

Method 2: Using Gauss's law in integral form $Q = \oint_S \vec{D} \cdot d\vec{s}$

$$Q = \int_{\text{top}} \vec{D} \cdot d\vec{s} + \int_{\text{bottom}} \vec{D} \cdot d\vec{s} + \int_{\text{left}} \vec{D} \cdot d\vec{s} + \int_{\text{right}} \vec{D} \cdot d\vec{s} + \int_{\text{back}} \vec{D} \cdot d\vec{s} + \int_{\text{front}} \vec{D} \cdot d\vec{s}$$

$$= \int_{\text{top}} \vec{D} \cdot (dx dy \vec{a}_z) + \int_{\text{bottom}} \vec{D} \cdot (-dx dy \vec{a}_z) + \int_{\text{left}} \vec{D} \cdot (-dx dz \vec{a}_y) + \int_{\text{right}} \vec{D} \cdot (dx dz \vec{a}_y) + \int_{\text{back}} \vec{D} \cdot (-dy dz \vec{a}_x) + \int_{\text{front}} \vec{D} \cdot (dy dz \vec{a}_x)$$

Since \vec{D} does not have a z-component, then the surface integral over the "top" and "bottom" surfaces give zeros. Therefore,

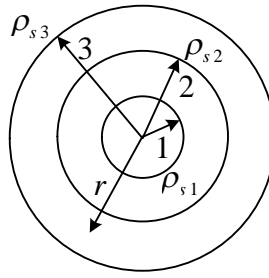
$$Q = - \int_{\text{left}} x^2 dx dz + \int_{\text{right}} x^2 dx dz - \int_{\text{back}} 2xy dy dz + \int_{\text{front}} 2xy dy dz$$

$$= - \int_{x=0}^1 \int_{z=0}^1 x^2 dx dz \Big|_{y=0} + \int_{x=0}^1 \int_{z=0}^1 x^2 dx dz \Big|_{y=1} - \int_{y=1}^1 \int_{z=0}^1 2xy dy dz \Big|_{x=0} + \int_{z=0}^1 \int_{y=0}^1 2xy dy dz \Big|_{x=1}$$

$$= -\frac{1}{3} + \frac{1}{3} - 0 + 1 = 1$$

$\therefore Q = 1C$ (the same answer as in method 1).

Problem 4.25



a) Using Gauss's law in integral form $\psi = \oint_S \vec{D} \cdot d\vec{s} = Q$

The electric flux through the closed surface $r = 1.5 \Rightarrow \psi = Q = \rho_{s1}S_1 = 2 \times 10^{-6}(4\pi \times 1^2) = 8\pi 10^{-6} \text{ C}$

The flux through $r = 2.5 \Rightarrow \psi = Q = \rho_{s1}S_1 + \rho_{s2}S_2 = 2 \times 10^{-6}(4\pi \times 1^2) - 4 \times 10^{-6}(4\pi \times 2^2) = -56\pi 10^{-6} \text{ C}$

b) From the symmetry of the problem, we conclude that \vec{D} has only a radial component. Thus $\vec{D} = D_r \vec{a}_r$.

Using $\oint_S \vec{D} \cdot d\vec{s} = Q \Rightarrow D_r 4\pi r^2 = Q \Rightarrow \therefore \vec{D} = \frac{Q}{4\pi r^2} \vec{a}_r$

At $r = 0.5 \Rightarrow \vec{D} = \frac{0}{4\pi(0.5)^2} \vec{a}_r = \vec{0}$

At $r = 2.5 \Rightarrow \vec{D} = \frac{\rho_{s1}S_1 + \rho_{s2}S_2}{4\pi(2.5)^2} \vec{a}_r = \frac{-56\pi 10^{-6}}{4\pi(2.5)^2} \vec{a}_r = -2.24 \vec{a}_r \text{ C/m}^2$

At $r = 3.5 \Rightarrow \vec{D} = \frac{\rho_{s1}S_1 + \rho_{s2}S_2 + \rho_{s3}S_3}{4\pi(3.5)^2} \vec{a}_r$

$$\vec{D} = \frac{2 \times 10^{-6}(4\pi \times 1^2) - 4 \times 10^{-6}(4\pi \times 2^2) + 5 \times 10^{-6}(4\pi \times 3^2)}{4\pi(3.5)^2} \vec{a}_r$$

$$\vec{D} = \frac{124\pi 10^{-6}}{4\pi(3.5)^2} \vec{a}_r = 2.531 \vec{a}_r \text{ C/m}^2$$

Problem 4.27

Using Gauss's law in integral form $\oint_S \vec{D} \cdot d\vec{s} = Q$

From the problem symmetry, we conclude that \vec{D} has a component along the ρ direction only. Thus $\vec{D} = D_\rho \vec{a}_\rho$.

Using a *closed* cylindrical surface S with a *variable* radius ρ and length h :

$$\oint_S \vec{D} \cdot d\vec{s} = Q \quad \Rightarrow \quad D_\rho 2\pi\rho h = Q \quad \Rightarrow \quad D_\rho = \frac{Q}{2\pi\rho h} \quad \Rightarrow \quad \vec{D} = \frac{Q}{2\pi\rho h} \vec{a}_\rho$$

$$\text{For } 1 > \rho \geq 0, \quad \vec{D} = \frac{Q}{2\pi\rho h} \vec{a}_\rho \quad \Rightarrow \quad \vec{D} = \frac{0}{2\pi\rho h} \vec{a}_\rho = \vec{0}$$

$$\text{For } 2 > \rho > 1, \quad \vec{D} = \frac{Q}{2\pi\rho h} \vec{a}_\rho \quad \Rightarrow \quad \vec{D} = \frac{\int \rho_v dv}{2\pi\rho h} \vec{a}_\rho = \frac{\int_{\rho=1}^{\rho} \int_{\phi=0}^{2\pi} \int_{z=0}^h (12\rho \times 10^{-9})(\rho d\rho d\phi dz)}{2\pi\rho h} \vec{a}_\rho$$

$$\vec{D} = \frac{12 \times 10^{-9} \times 2\pi h \times \frac{\rho^3}{3} \Big|_1^\rho}{2\pi\rho h} \vec{a}_\rho = \frac{4 \times 10^{-9} (\rho^3 - 1)}{\rho} \vec{a}_\rho$$

$$\text{For } \rho > 2, \quad \vec{D} = \frac{Q}{2\pi\rho h} \vec{a}_\rho \quad \Rightarrow \quad \vec{D} = \frac{\int \rho_v dv}{2\pi\rho h} \vec{a}_\rho = \frac{\int_{\rho=1}^2 \int_{\phi=0}^{2\pi} \int_{z=0}^h (12\rho \times 10^{-9})(\rho d\rho d\phi dz)}{2\pi\rho h} \vec{a}_\rho$$

$$\vec{D} = \frac{12 \times 10^{-9} \times 2\pi h \times \frac{\rho^3}{3} \Big|_1^2}{2\pi\rho h} \vec{a}_\rho = \frac{4 \times 10^{-9} (8 - 1)}{\rho} \vec{a}_\rho = \frac{28 \times 10^{-9}}{\rho} \vec{a}_\rho$$

Problem 4.41

$$V_{ab} = -\int_a^b \vec{E} \cdot d\vec{l} \quad \Rightarrow \quad W_{ab} = -q \int_a^b \vec{E} \cdot d\vec{l}$$

$$\text{a) } W_{AB} = -q \int_A^B \vec{E} \cdot d\vec{l} = -4 \times 10^{-9} \int_{\rho=1}^4 E_\rho \Big|_{\phi=0, z=0} d\rho = -4 \times 10^{-9} \int_{\rho=1}^4 0 d\rho = 0$$

$$\text{b) } W_{BC} = -q \int_B^C \vec{E} \cdot d\vec{l} = -4 \times 10^{-9} \int_{\phi=0^\circ}^{30^\circ} E_\phi \rho d\phi \Big|_{\rho=4, z=0} = -4 \times 10^{-9} \int_{\phi=0^\circ}^{30^\circ} 4 \cos \phi \times 4 d\phi = -32 \times 10^{-9} = -32 \text{ nJ}$$

$$\text{c) } W_{CD} = -q \int_C^D \vec{E} \cdot d\vec{l} = -4 \times 10^{-9} \int_{z=0}^{-2} E_z \Big|_{\rho=4, \phi=30^\circ} dz = -4 \times 10^{-9} \int_{z=0}^{-2} 4 \sin 30^\circ dz = 16 \times 10^{-9} = 16 \text{ nJ}$$

$$\text{d) } W_{AD} = (0 - 32 + 16) \times 10^{-9} = -16 \text{ nJ}$$

Problem 4.43

$$\vec{E} = -\nabla V$$

a) In rectangular coordinates $\vec{E} = -\left(\frac{\partial V}{\partial x}\vec{a}_x + \frac{\partial V}{\partial y}\vec{a}_y + \frac{\partial V}{\partial z}\vec{a}_z\right)$

For $V = x^2 + 2y^2 + 4z^2 \Rightarrow \vec{E} = -(2x\vec{a}_x + 4y\vec{a}_y + 8z\vec{a}_z)$ V/m

d) In spherical coordinates $\vec{E} = -\left(\frac{\partial V}{\partial r}\vec{a}_r + \frac{1}{r}\frac{\partial V}{\partial \theta}\vec{a}_\theta + \frac{1}{r\sin\theta}\frac{\partial V}{\partial \phi}\vec{a}_\phi\right)$

For $V = e^{-r}\sin\theta\cos 2\phi \Rightarrow \vec{E} = -\left(-e^{-r}\sin\theta\cos 2\phi\vec{a}_r + \frac{e^{-r}\cos\theta\cos 2\phi}{r}\vec{a}_\theta + \frac{-2e^{-r}\sin\theta\sin 2\phi}{r\sin\theta}\vec{a}_\phi\right)$

$$\vec{E} = e^{-r}\sin\theta\cos 2\phi\vec{a}_r - \frac{e^{-r}}{r}\cos\theta\cos 2\phi\vec{a}_\theta + \frac{2e^{-r}}{r}\sin 2\phi\vec{a}_\phi$$