

CHEM 311 (151)

**Second Major Exam**                      **2 HOURS**  
**Thursday, November 19, 2015, 8:00-10:00 PM**

STUDENT NAME: .....

STUDENT ID NUMBER: .....

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**Test Code (001)**

**(16 Questions)**

Dr. M. Morsy	Section 1
Dr. H. Badawi	Section 2
Dr. W. Foerner	Section 3
Dr. G. Oweimreen	Section 4

Physical constants, conversion factors, and useful equations

Physical Constants

$$R = 8.314 \text{ J mol}^{-1} \text{ K}^{-1}$$

$$= 0.08206 \text{ L atm K}^{-1} \text{ mol}^{-1}$$

$$= 0.08314 \text{ L bar K}^{-1} \text{ mol}^{-1}$$

$$N_A = 6.022 \times 10^{23} \text{ mol}^{-1}$$

$$k_B = 1.381 \times 10^{-23} \text{ J K}^{-1}$$

$$h = 6.626 \times 10^{-34} \text{ J s}$$

$$F = 96,500 \text{ C mol}^{-1}$$

$$c = 2.998 \times 10^8 \text{ m s}^{-1}$$

$$g = 9.81 \text{ m s}^{-2}$$

$$B = 0.51 \text{ mol}^{-1/2} \text{ dm}^{3/2}$$

(in H<sub>2</sub>O, 25°C)

Sequential reactions:



$$[B] = (k_1 / (k_2 - k_1)) f(t) [A]_0$$

$$f(t) = \exp(-k_1 t) - \exp(-k_2 t)$$

Other Units

$$1 \text{ dm}^3 = 1 \text{ L}$$

$$1 \text{ dm}^3 = 1000 \text{ cm}^3$$

$$1 \text{ J} = 1 \text{ kg m}^2 \text{ s}^{-2}$$

$$1 \text{ atm} = 1.101325 \times 10^5 \text{ Pa}$$

$$1 \text{ atm} = 760 \text{ mmHg}$$

$$1 \text{ Torr} = 1 \text{ mmHg}$$

$$1 \text{ Torr} = 133.322 \text{ Pa}$$

$$1 \text{ bar} = 10^5 \text{ Pa}$$

$$1 \text{ nm} = 10^{-9} \text{ m}$$

$$v = \frac{V[S]}{K_m + [S]}$$

$$V = k_2 [E]_0 \text{ and } K_m = \frac{k_{-1} + k_2}{k_1}$$

Eyring equation:

$$k = k_B T / (hc^0) \times f$$

$$f = \exp(\Delta S^\ddagger / R) \times \exp(-\Delta H^\ddagger / RT)$$

Important Equations

$$k = A e^{-E_a / RT}$$

$$k = \frac{k_B T}{h} e^{-\Delta^\ddagger G^\ddagger / RT}$$

$$\Delta G = \Delta H - T \Delta S$$

$$E_a = \Delta^\ddagger H^\circ - P \Delta^\ddagger V^\circ + RT \text{ (sol)}$$

$$= \Delta^\ddagger H^\circ - \Sigma \nu RT + RT \text{ (gas)}$$

$$\log k = \log k_0 - \frac{\Delta^\ddagger V}{RT} P$$

$$\Delta G^\circ = -RT \ln K_c$$

$$dP/dt = k\theta$$

$$\theta = KP / (1 + KP), \text{ at } T = \text{const}$$

$$\ln(1 - \theta) = -\theta$$

if  $\theta \ll 1$

Parallel reactions:

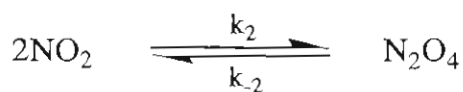
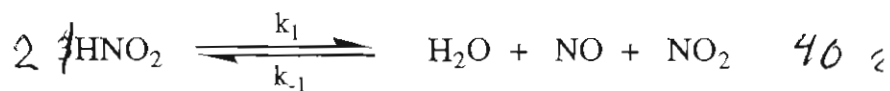
$$\Phi_i = k_i / S$$

where S is the sum of all rate constants of the parallel reactions

1. Find the rate law of the reaction:



If the first two of the following steps rapidly attain equilibrium and the third step is slow:



{ Note:  $k_1/k_{-1} = K_1$  and  $k_2/k_{-2} = K_2$  }

- A)  $k_1 k_2 [\text{HNO}_2]^2 / [\text{NO}]^2 [\text{H}_2\text{O}]$
- B)  $K_1 k_3 [\text{NO}]^2 [\text{H}_2\text{O}]$
- C)  $K_1 K_2 k_3 [\text{HNO}_2]^4 / [\text{NO}]^2 [\text{H}_2\text{O}]$
- D)  $K_1 K_2 k_3 [\text{HNO}_2] / [\text{NO}] [\text{H}_2\text{O}]$
- E)  $K_2 k_3 [\text{HNO}_2] / [\text{NO}]^2$

$$\textcircled{1} \quad R = - \frac{d[\text{H}_2\text{O}]}{dt} \quad \text{---}$$

$$= k_3 [\text{H}_2\text{O}][\text{N}_2\text{O}_4]$$

$$K_2 = \frac{[\text{N}_2\text{O}_4]}{[\text{NO}_2]^2}$$

$$[\text{N}_2\text{O}_4] = K_2 [\text{NO}_2]^2$$

$$K_1 = \frac{[\text{H}_2\text{O}][\text{NO}][\text{NO}_2]}{[\text{HNO}_2]^2}$$

$$[\text{NO}_2] = K_1 \frac{[\text{HNO}_2]^2}{[\text{H}_2\text{O}][\text{NO}]}$$

$$[\text{N}_2\text{O}_4] = K_2 [\text{NO}_2]^2$$

$$= K_1^2 K_2 \frac{[\text{HNO}_2]^4}{[\text{H}_2\text{O}]^2 [\text{NO}]^2}$$

$$R = k_3 [\text{H}_2\text{O}][\text{N}_2\text{O}_4]$$

$$= K_1^2 K_2 k_3 \overset{\checkmark}{[\text{H}_2\text{O}]} \frac{[\text{HNO}_2]^4}{\underset{\checkmark}{([\text{H}_2\text{O}]^2 [\text{NO}]^2)}}$$

$$= K_1^2 K_2 k_3 \frac{[\text{HNO}_2]^4}{[\text{H}_2\text{O}][\text{NO}]^2} \quad \textcircled{C}$$

2. In a trimolecular gas-phase reaction  $[A(g) + B(g) + C(g) \rightarrow TS(g)$  (TS = transition state)] the rate constant,  $k$ , is  $3.44 \times 10^5 \text{ M}^{-2} \text{ s}^{-1}$  at  $55.0 \text{ }^\circ\text{C}$  and the entropy of activation,  $\Delta S^\ddagger$ , is  $-152 \text{ J K}^{-1} \text{ mol}^{-1}$ . What is the activation energy,  $E_a$ , according to transition state or activated complex theory?
- A)  $0.152 \text{ J mol}^{-1}$
  - B)  $1.16 \text{ J mol}^{-1}$
  - C)  $4.16 \text{ kJ mol}^{-1}$
  - D)  $0.695 \text{ kJ mol}^{-1}$
  - E)  $0.695 \text{ J mol}^{-1}$
3. Transition state theory assumes an equilibrium between
- A) all reaction components except radicals
  - B) stable intermediates
  - C) activated complex and reactants
  - D) reactants and products
  - E) all reaction components even radicals

② tri molecular gas reactions

$$E_a = \Delta H^\ddagger + 3RT \quad \Delta n_{\text{gas}} = \frac{1-3}{3-1-2} = -2$$

$$\Delta U^\ddagger = \Delta H^\ddagger - \Delta n_{\text{gas}} RT \\ = \Delta H^\ddagger + 2RT$$

$$E_a = RT + \Delta U^\ddagger = \Delta H^\ddagger + 3RT$$

$$A = \frac{e^3 k_B T \Delta S^\ddagger / R}{h(c^\circ)^2} e$$

$$\Delta S^\ddagger / R = -152 \frac{\text{J}}{\text{K mol}} / 8.314 \frac{\text{J}}{\text{K mol}} = -18.282$$

$$e^{\Delta S^\ddagger / R} = e^{-18.282} = 1.149 \cdot 10^{-8}$$

$$A_F = \frac{e^3 \cdot 1.381 \cdot 10^{-23} \text{ J/K} \cdot 328.15 \text{ K}}{6.626 \cdot 10^{-34} \text{ Js} \cdot 1 \text{ M}^2 \cdot 1.149 \cdot 10^{-8}}$$

$$= 1.5784 \cdot 10^6 \frac{1}{\text{M}^2 \text{ s}}$$

$$k = A e^{-E_a / RT}$$

$$E_a = -RT \ln \frac{k}{A}$$

$$E_a = -8.314 \frac{\text{J}}{\text{K mol}} \cdot 328.15 \text{ K} \cdot \ln \frac{3.44 \cdot 10^5 \frac{1}{\text{M}^2 \text{ s}}}{1.5784 \cdot 10^6 \frac{1}{\text{M}^2 \text{ s}}}$$

$$= -2.728 \frac{\text{kJ}}{\text{mol}} \cdot \ln(0.2179)$$

$$= -2.728 \frac{\text{kJ}}{\text{mol}} \cdot (-1.5237)$$

$$= 4.15(7) \frac{\text{kJ}}{\text{mol}} = 4.16 \frac{\text{kJ}}{\text{mol}}$$

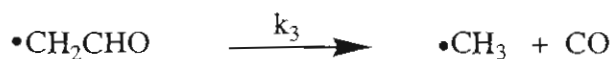
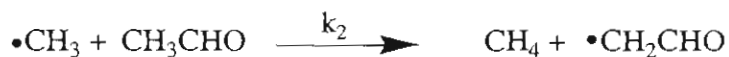
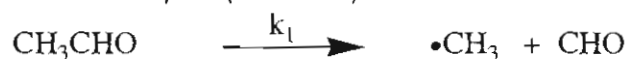
③

③ condition for TS theory:

equilibrium between TS and reactants

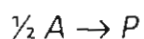
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4. The following free radical mechanism has been proposed for the thermal decomposition of acetaldehyde (ethanal):



Find an expression for the rate of formation of ethane ( $\text{CH}_3\text{CH}_3$ )

- A)  $(k_1/k_4)^{1/2} [\text{CH}_3\text{CHO}]^{1/2}$
- B)  $k_1k_2/k_3 [\text{CH}_3\text{CHO}]^2$
- C)  $k_1/k_4 [\text{CH}_3\text{CHO}]^{1/2}$
- D)  $k_1[\text{CH}_3\text{CHO}]$
- E)  $k_1[\text{CH}_3\text{CHO}]/[\text{CH}_3\text{CH}_3]$
5. What is the half-life of A in the following elementary reaction,



when  $[\text{A}]_0 = 4.00 \text{ M}$ ,  $[\text{P}]_0 = 0$  and the rate constant being  $k = 1.21 \times 10^4 \text{ M}^{1/2} \text{ s}^{-1}$  ?

- A)  $\tau_{1/2} = 34.2 \mu\text{s}$
- B)  $\tau_{1/2} = 70.5 \mu\text{s}$
- C)  $\tau_{1/2} = 10.3 \mu\text{s}$
- D)  $\tau_{1/2} = 96.8 \mu\text{s}$
- E)  $\tau_{1/2} = 48.4 \mu\text{s}$



$$(4) \quad R = \frac{d[C_2H_6]}{dt} = k_4 [CH_3^\cdot]^2$$

$$\frac{d[CH_3^\cdot]}{dt} \text{ SSA} = 0 = k_1 [CH_3CHO] - k_2 [CH_3^\cdot] [CH_3CHO] + k_3 [CH_2CHO^\cdot] - 2k_4 [CH_3^\cdot]^2 \quad (1)$$

$$\frac{d[CH_2CHO^\cdot]}{dt} \text{ SSA} = 0 = k_2 [CH_3^\cdot] [CH_3CHO] - k_3 [CH_2CHO^\cdot] \quad (2)$$

$$(1) + (2) \quad 0 = k_1 [CH_3CHO] - 2k_4 [CH_3^\cdot]^2$$

$$k_4 [CH_3^\cdot]^2 = \frac{k_1}{2k_4} k_1 [CH_3CHO]$$

$$R = k_1 [CH_3CHO]$$

(D)

### Half-Life concept, Sections 5.2 and 5.4

5 What is the half-life of A in the following elementary reaction  
 $\frac{1}{2} A \rightarrow P$   $k$  is the effective rate constant of the process  
 when  $[A]_0 = 4.00 \text{ M}$ ,  $[P]_0 = 0$  and the rate constant being  $k = 1.21 \times 10^4 \text{ M}^{1/2} \text{ s}^{-1}$ ?

- A)  $\tau_{1/2} = 96.8 \mu\text{s}$
- B)  $\tau_{1/2} = 48.4 \mu\text{s}$
- C)  $\tau_{1/2} = 34.2 \mu\text{s}$
- D)  $\tau_{1/2} = 70.5 \mu\text{s}$
- E)  $\tau_{1/2} = 10.3 \mu\text{s}$

rate:  $\frac{1}{\nu_i} \frac{d[i]}{dt}$   
 but rate of consumption  $\nu_i = \frac{1}{2}$   
 $v = -\frac{d[A]}{dt} = k[A]^{1/2}$

$$\frac{d[A]}{dt} = -k[A]^{1/2} \quad \int x^{-1/2} dx = 2x^{1/2} + C$$

$$\int_{[A]_0}^{[A]_0/2} \frac{d[A]}{[A]^{1/2}} = 2[A]^{1/2} \Big|_{[A]_0}^{[A]_0/2} = -k\tau_{1/2}$$

$$\left(\frac{[A]_0}{2}\right)^{1/2} - [A]_0^{1/2} = -\frac{1}{2}k\tau_{1/2} \quad \left(\frac{1}{\sqrt{2}} - 1\right)[A]_0^{1/2} = -\frac{1}{2}k\tau_{1/2}$$

$$\frac{1-\sqrt{2}}{\sqrt{2}} [A]_0^{1/2} = -\frac{1}{2}k\tau_{1/2} \quad \tau_{1/2} = -2 \frac{1-\sqrt{2}}{\sqrt{2}} \left(\frac{1}{k}\right) [A]_0^{1/2}$$

$$\tau_{1/2} = -\sqrt{2}(1-\sqrt{2}) 2 \frac{1}{k} \sqrt{M} \quad [A]_0 = 4 \text{ M}$$

$$\tau_{1/2} = -2\sqrt{2}(1-\sqrt{2}) \frac{1}{k} \sqrt{M}$$

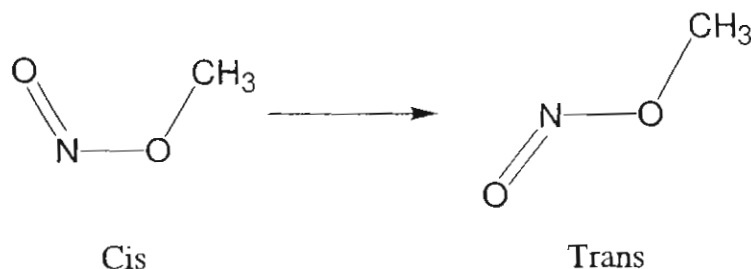
$$= 1.17157 \cdot \frac{1}{1.21 \cdot 10^4} \text{ s} = 9.682 \cdot 10^{-5} \text{ s}$$

$$= 96.8 \cdot 10^{-6} \text{ s} = 96.8 \mu\text{s} \quad \textcircled{A} \quad \textcircled{D} \text{ in Version 1}$$

$k$ : effective rate constant of



6. The compound  $\text{CH}_3\text{-O-N=O}$  has an internal rotation about the O-N bond as follows:



The half-life of the first order disappearance of the cis form can be measured by NMR techniques. It is  $1.00 \times 10^{-6}$  sec at  $25^\circ\text{C}$ . Assuming  $\Delta S^\ddagger = 0$  for this reaction, calculate the height of the barrier to rotation.

- A) 11.2 kJ/mol  
 B) -21.1 kJ/mol  
 C) 42.2 kJ/mol  
 D) 21.1 kJ/mol  
 E) -11.2 kJ/mol
7. For a reaction of a rate constant  $k$ . If all reactants have initial concentration  $a$  and concentration  $x$  at any time of an order of  $n$ , and its integrated rate equation is

$$\frac{1}{(n-1)x^{n-1}} = \frac{1}{(n-1)a^{n-1}} + kt$$

which of the following mathematical expression is the half-life,  $t_{1/2}$ ,

- A)  $\frac{1}{(n-1)a^{n-1}}$   
 $\frac{2^{n-1}}{2^{n-1}}$   
 B)  $k a^{n-1}$   
 C)  $\frac{1}{(n-1)k a^{n-1}}$   
 $\frac{2^{n-1} - 1}{2^{n-1} - 1}$   
 D)  $\frac{(n-1)k}{2^{n-1} - 1}$   
 E)  $\frac{(n-1)k a^{n-1}}{2^{n-1} - 1}$

⑥ barrier height =  $E_a$

1. order  $k = \frac{\ln 2}{\tau} = \frac{\ln 2}{1.00 \cdot 10^{-6} \text{ s}} = 6,9315 \cdot 10^5 \text{ s}^{-1}$

$$k = A e^{-E_a/RT}$$

$$A = \frac{e k_B T}{h}$$

$$\Delta S^\ddagger = 0$$

$$\Rightarrow e^{\Delta S^\ddagger/R} = 1$$

$$A = \frac{e \cdot 1,381 \cdot 10^{-23} \text{ J/K} \cdot 298,15 \text{ K}}{6,626 \cdot 10^{-34} \text{ Js}} = 1,6892 \cdot 10^{13} \frac{1}{\text{s}}$$

$$E_a = -RT \ln \frac{k}{A} = -8,314 \frac{\text{J}}{\text{K mol}} \cdot 298,15 \text{ K} \ln \frac{6,9315 \cdot 10^5}{1,6892 \cdot 10^{13}}$$

$$= -2,4788 \frac{\text{kJ}}{\text{mol}} (-17,0115)$$

$$= 42,1(7) \frac{\text{kJ}}{\text{mol}} = 42,2 \frac{\text{kJ}}{\text{mol}}$$

©

(7)

$$kt = \frac{1}{(n-1)x^{n-1}} - \frac{1}{(n-1)a^{n-1}}$$

$$t = t_{1/2} = \tau \Rightarrow x = \frac{a}{2}$$

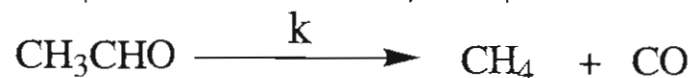
$$k\tau = \frac{1}{(n-1)\left(\frac{a}{2}\right)^{n-1}} - \frac{1}{(n-1)a^{n-1}}$$

$$= \frac{2^{n-1}}{(n-1)a^{n-1}} - \frac{1}{(n-1)a^{n-1}}$$

$$= \frac{2^{n-1} - 1}{(n-1)a^{n-1}}$$

$$\tau = \frac{2^{n-1} - 1}{(n-1)ka^{n-1}} \quad \text{(E)}$$

8. The thermal Decomposition of acetaldehyde vapor:



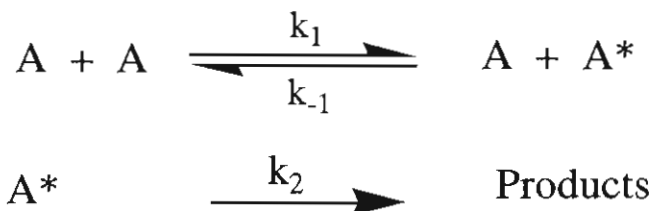
Is an irreversible process whose rate at 518 °C is given by the following two sets of data for pressure changes at constant temperature and volume

Initial Pressure of Acetaldehyde (mm Hg)	Total Pressure of the system after 100 sec (mm Hg)
400.0	500.0
300.0	360.0

Find the order of the decomposition process with respect to acetaldehyde.

- A) 0
- B) 2
- C) 2.5
- D) 1
- E) 1.5

11. The isomerization of cyclopropane to propylene follows Lindemann kinetics:



so that the reaction process follow the rate law:

$$\frac{dP_A}{dt} = \frac{k_1 k_2 P_A^2}{(k_2 + k_{-1} P_A)}$$

where  $P_A$  is the reactant pressure. Calculate the ratio of the time for 1% of the propylene to isomerize at a given temperature if the initial pressure is 1 atm to the time for 1% to isomerize if the initial pressure is  $1 \times 10^{-2}$  atm. The values of  $k_1$ ,  $k_{-1}$ , and  $k_2$  are  $1 \times 10^{14} \text{ min}^{-1} \text{ atm}^{-1}$ ,  $1 \times 10^{11} \text{ min}^{-1} \text{ atm}^{-1}$ , and  $1 \times 10^4 \text{ min}^{-1}$ , respectively.

- A) 10
- B) 50
- C) 100
- D) 1
- E) 20

$$\frac{\Delta P}{\Delta t} = \frac{k_1 k_2 P_A}{k_{-1}}$$

$$\frac{t_2}{t_1} = \frac{P_{A1}}{P_{A2}} = 100$$

$$\textcircled{11} \quad \frac{dP_A}{dt} = \frac{\Delta P_A}{\Delta t} = \frac{k_1 k_2 P_A^2}{k_{-1} P_A} = \frac{k_1 k_2}{k_{-1}} P_A$$

$$k_2 = 10^4 \text{ min}^{-1} \ll k_{-1} = 10^{10} \frac{1}{\text{min atm}}$$

$\Delta P_A$  is in both cases 1%

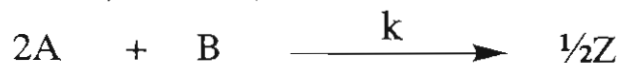
$$\Rightarrow R_1 = \frac{1\%}{\Delta t_1} \quad R_2 = \frac{1\%}{\Delta t_2}$$

$$\frac{R_2}{R_1} = \frac{\Delta t_2}{\Delta t_1} = \frac{P_A(1)}{P_A(2)} = \frac{1 \text{ atm}}{0.01 \text{ atm}} = 100$$

$\textcircled{E}$



12. Consider the elementary reaction,



what is the rate of consumption of A, if  $[A]_0 = 2a_0$ ,  $[B]_0 = a_0$ ,  $[Z]_0 = 0$ , and after time  $t$ ,  $[Z] = \frac{1}{2}x$ ?

A)  $-\frac{d[A]}{dt} = -8k(a_0 - x)^3$

B)  $-\frac{d[A]}{dt} = 4k(a_0 - x)^2$

C)  $-\frac{d[A]}{dt} = 8k(a_0 - x)^2$

D)  $-\frac{d[A]}{dt} = 8k(a_0 - x)^3$

E)  $-\frac{d[A]}{dt} = 4k(a_0 - x)^3$

13. Apply the steady state approximation to the intermediates B and C in the consecutive reaction sequence



to obtain an expression for the concentration  $[D]$  as function of time, when initially  $[A] = [A]_0$ , and  $[B]_0 = [C]_0 = [D]_0 = 0$ .

{ Note:  $\int e^{ax} dx = \frac{1}{a} e^{ax} + C$ , where  $C$  is the integration constant }

A)  $[D] = \frac{k_A}{k_B} [A]_0 (e^{-k_A t} - 1)$

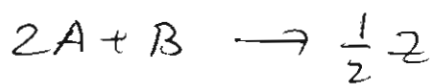
B)  $[D] = [A]_0 (e^{-k_A t} - 1)$

C)  $[D] = \frac{k_A}{k_B} [A]_0 (e^{-k_B t} - e^{-k_A t})$

D)  $[D] = \frac{k_A}{k_B} [A]_0 (1 - e^{-k_A t})$

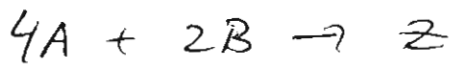
E)  $[D] = [A]_0 (1 - e^{-k_A t})$

12



$$-\frac{1}{2} \frac{d[A]}{dt} = k[A]^2[B]$$

$$-\frac{d(A)}{dt} = 2k[A]^2[B]$$



$$2a_0 - 2x \quad a_0 - x \quad x/2$$

$$\text{with } [A]_0 = 2a_0, [B]_0 = a_0$$

$$-\frac{d(A)}{dt} = 2k[2(a_0 - x)]^2(a_0 - x)$$

$$= 8k(a_0 - x)^3$$

D

(13)

$$\frac{d[D]}{dt} = k_c [C]$$

$$\frac{d[C]}{dt} = 0 = k_B [B] - k_c [C] \rightarrow k_c [C] = k_B [B]$$

$$\frac{d[B]}{dt} = 0 = k_A [A] - k_B [B] \rightarrow k_B [B] = k_A [A]$$

$$\frac{d[D]}{dt} = k_A [A]$$

$$\frac{d[A]}{dt} = -k_A [A] \quad \int_{[A]_0}^{[A]} \frac{d[A]}{[A]} = -k_A \int_0^t dt$$

$$\ln \frac{[A]}{[A]_0} = -k_A t \Rightarrow [A] = [A]_0 e^{-k_A t}$$

$$\frac{d[D]}{dt} = k_A [A]_0 e^{-k_A t}$$

$$[D] - [D]_0 = k_A [A]_0 \int_0^t e^{-k_A t} dt$$

$$= k_A [A]_0 \left(-\frac{1}{k_A}\right) \left(e^{-k_A t} - 1\right)$$

$$[D] = -[A]_0 \left(e^{-k_A t} - 1\right)$$

$$= [A]_0 (1 - e^{-k_A t})$$

(E)

14. The Steady State Approximation can be applied to a reaction intermediate if it reaches rapidly a concentration being constant in most of the reaction time, is much smaller than the reactant concentration, and
- A) is formed slowly.
  - B) its concentration is constant but large compared to reactant concentrations.
  - C) is not reacting during the course of the reaction.
  - D) is consumed rapidly.
  - E) is present in a concentration much smaller than reactant concentrations but is not constant.

15. In an experiment (at 15 °C) on the reaction



the obtained data ( $v_0$  denotes the initial rate of consumption of NO) are

Run	[NO] <sub>0</sub> (mM)	[H <sub>2</sub> ] <sub>0</sub> (mM)	$v_0$ ( $\mu\text{M L}^{-1} \text{s}^{-1}$ )
1	12.8	4.4	52
2	25.6	4.4	200
3	12.8	9.0	102

What is the overall order of the reaction?

- A) 2
- B) 0
- C) 4
- D) 1
- E) 3

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SSA good if intermediate decays fast <sup>(D) ✓</sup>  
~~and formed slowly (A)~~

ERROR both (A) and (D) are correct  
~~B, C, E nonsense!~~

(15)  $v_0 = k [NO]^n [H_2]^m$

in 1 & 2  $[H_2]_0$  is the same

$$\rightarrow \frac{\text{Rate 1}}{\text{Rate 2}} = \frac{52}{200} = \left(\frac{12.8}{25.6}\right)^n \left(\frac{4.4}{4.4}\right)^m$$

$$0.26 = (0.5)^n$$

$$n = \frac{\ln 0.26}{\ln 0.5} = 1.94 = 2$$

$$\frac{\text{Rate 2}}{\text{Rate 3}} = \frac{200}{102} = \left(\frac{25.6}{12.8}\right)^2 \left(\frac{4.4}{9.6}\right)^m$$

$$1.96078 = 4 \cdot (0.4889)^m$$

$$\ln 1.96078 = \ln 4 + m \ln 0.4889$$

$$m = \frac{\ln \frac{1.96078}{4}}{\ln \frac{0.4889}{0.4889}} = 0.996 = 1$$

overall,  $1+2=3$  (E)

16. The Pt-Catalyzed decomposition of HI obeys the following rate laws depending on the HI pressure:

$dP_{HI}/dt = k_1$ , at high pressure, with  $k_1 = 500 \text{ mm Hg sec}^{-1}$  at  $100^\circ\text{C}$ ,

$dP_{HI}/dt = k_2 P_{HI}$ , at low pressure, with  $k_2 = 50 \text{ sec}^{-1}$  at  $100^\circ\text{C}$ .

Calculate the HI pressure at which the value of  $dP_{HI}/dt = 250 \text{ mm Hg sec}^{-1}$ , at the same temperature.

- A) 200 mm Hg  
 B) 0.1 mm Hg  
 C) 500 mm Hg  
 D) 50 mm Hg  
 E) 10 mm Hg

$$\text{Langmuir } \theta = \frac{KP}{1 + KP}$$

$$R = \frac{dP_{HI}}{dt} = k_1 \theta \text{ at high } P$$

$$K = \left( \frac{k_1}{k_2} \right)^{-1} = \left( \frac{500 \text{ torr/s}}{50 \text{ s}^{-1}} \right)^{-1} = 10 \text{ torr} = 0.1 \text{ torr}^{-1}$$

$$R = k_1 \frac{0.1 \text{ torr}^{-1} P}{1 + 0.1 \text{ torr}^{-1} P}$$

$$R(1 + 0.1 \text{ torr}^{-1} P) = k_1 \cdot 0.1 \text{ torr}^{-1} P$$

$$(0.1 \text{ torr}^{-1} R - k_1 \cdot 0.1 \text{ torr}^{-1}) P = -R$$

$$P = \frac{-250 \text{ torr/s}}{\frac{0.1}{\text{torr}} \cdot 250 \frac{\text{torr}}{\text{s}} - 500 \frac{\text{torr}}{\text{s}} \cdot 0.1 \text{ torr}^{-1}}$$

~~25~~

$$= \frac{-250 \text{ torr/s}}{25 \text{ } 1/\text{s} - 50 \text{ } 1/\text{s}} = 10 \text{ torr (E)}$$



NAME \_\_\_\_\_

STUDENT No. \_\_\_\_\_

SECTION No. \_\_\_\_\_

TEST ANSWER FORM

TESTING SERVICES SYSTEM

MARKING INSTRUCTIONS

0	1	2	3	4	5	6	7	8	9	A	B	C	D	E
0	1	2	3	4	5	6	7	8	9	A	B	C	D	E
0	1	2	3	4	5	6	7	8	9	A	B	C	D	E
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STUDENT NUMBER

0	1	2	3	4	5	6	7	8	9	A	B	C	D	E
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SECTION NUMBER

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0	1	2	3	4	5	6	7	8	9	A	B	C	D	E
0	1	2	3	4	5	6	7	8	9	A	B	C	D	E

TEST CODE No.

DIRECTIONS:

Read each question and its numbered answers. When you have decided which answer is correct, blacken the corresponding oval on this form with a no. 2 pencil. Make no extra marks. They may be counted as incorrect answers. Erase incorrect answers fully before filling in correct answer.

DO NOT USE INK OR BALL POINT PEN

SAMPLE

1. RIYADH is:

- A - a country
- B - a mountain
- C - an island
- D - a city
- E - a river

1 (A) (B) (C) (D) (E)

1

- |                        |                        |                        |                         |                         |
|------------------------|------------------------|------------------------|-------------------------|-------------------------|
| 1 (A) (B) (C) (D) (E)  | 26 (A) (B) (C) (D) (E) | 51 (A) (B) (C) (D) (E) | 76 (A) (B) (C) (D) (E)  | 101 (A) (B) (C) (D) (E) |
| 2 (A) (B) (C) (D) (E)  | 27 (A) (B) (C) (D) (E) | 52 (A) (B) (C) (D) (E) | 77 (A) (B) (C) (D) (E)  | 102 (A) (B) (C) (D) (E) |
| 3 (A) (B) (C) (D) (E)  | 28 (A) (B) (C) (D) (E) | 53 (A) (B) (C) (D) (E) | 78 (A) (B) (C) (D) (E)  | 103 (A) (B) (C) (D) (E) |
| 4 (A) (B) (C) (D) (E)  | 29 (A) (B) (C) (D) (E) | 54 (A) (B) (C) (D) (E) | 79 (A) (B) (C) (D) (E)  | 104 (A) (B) (C) (D) (E) |
| 5 (A) (B) (C) (D) (E)  | 30 (A) (B) (C) (D) (E) | 55 (A) (B) (C) (D) (E) | 80 (A) (B) (C) (D) (E)  | 105 (A) (B) (C) (D) (E) |
| 6 (A) (B) (C) (D) (E)  | 31 (A) (B) (C) (D) (E) | 56 (A) (B) (C) (D) (E) | 81 (A) (B) (C) (D) (E)  | 106 (A) (B) (C) (D) (E) |
| 7 (A) (B) (C) (D) (E)  | 32 (A) (B) (C) (D) (E) | 57 (A) (B) (C) (D) (E) | 82 (A) (B) (C) (D) (E)  | 107 (A) (B) (C) (D) (E) |
| 8 (A) (B) (C) (D) (E)  | 33 (A) (B) (C) (D) (E) | 58 (A) (B) (C) (D) (E) | 83 (A) (B) (C) (D) (E)  | 108 (A) (B) (C) (D) (E) |
| 9 (A) (B) (C) (D) (E)  | 34 (A) (B) (C) (D) (E) | 59 (A) (B) (C) (D) (E) | 84 (A) (B) (C) (D) (E)  | 109 (A) (B) (C) (D) (E) |
| 10 (A) (B) (C) (D) (E) | 35 (A) (B) (C) (D) (E) | 60 (A) (B) (C) (D) (E) | 85 (A) (B) (C) (D) (E)  | 110 (A) (B) (C) (D) (E) |
| 11 (A) (B) (C) (D) (E) | 36 (A) (B) (C) (D) (E) | 61 (A) (B) (C) (D) (E) | 86 (A) (B) (C) (D) (E)  | 111 (A) (B) (C) (D) (E) |
| 12 (A) (B) (C) (D) (E) | 37 (A) (B) (C) (D) (E) | 62 (A) (B) (C) (D) (E) | 87 (A) (B) (C) (D) (E)  | 112 (A) (B) (C) (D) (E) |
| 13 (A) (B) (C) (D) (E) | 38 (A) (B) (C) (D) (E) | 63 (A) (B) (C) (D) (E) | 88 (A) (B) (C) (D) (E)  | 113 (A) (B) (C) (D) (E) |
| 14 (A) (B) (C) (D) (E) | 39 (A) (B) (C) (D) (E) | 64 (A) (B) (C) (D) (E) | 89 (A) (B) (C) (D) (E)  | 114 (A) (B) (C) (D) (E) |
| 15 (A) (B) (C) (D) (E) | 40 (A) (B) (C) (D) (E) | 65 (A) (B) (C) (D) (E) | 90 (A) (B) (C) (D) (E)  | 115 (A) (B) (C) (D) (E) |
| 16 (A) (B) (C) (D) (E) | 41 (A) (B) (C) (D) (E) | 66 (A) (B) (C) (D) (E) | 91 (A) (B) (C) (D) (E)  | 116 (A) (B) (C) (D) (E) |
| 17 (A) (B) (C) (D) (E) | 42 (A) (B) (C) (D) (E) | 67 (A) (B) (C) (D) (E) | 92 (A) (B) (C) (D) (E)  | 117 (A) (B) (C) (D) (E) |
| 18 (A) (B) (C) (D) (E) | 43 (A) (B) (C) (D) (E) | 68 (A) (B) (C) (D) (E) | 93 (A) (B) (C) (D) (E)  | 118 (A) (B) (C) (D) (E) |
| 19 (A) (B) (C) (D) (E) | 44 (A) (B) (C) (D) (E) | 69 (A) (B) (C) (D) (E) | 94 (A) (B) (C) (D) (E)  | 119 (A) (B) (C) (D) (E) |
| 20 (A) (B) (C) (D) (E) | 45 (A) (B) (C) (D) (E) | 70 (A) (B) (C) (D) (E) | 95 (A) (B) (C) (D) (E)  | 120 (A) (B) (C) (D) (E) |
| 21 (A) (B) (C) (D) (E) | 46 (A) (B) (C) (D) (E) | 71 (A) (B) (C) (D) (E) | 96 (A) (B) (C) (D) (E)  | 121 (A) (B) (C) (D) (E) |
| 22 (A) (B) (C) (D) (E) | 47 (A) (B) (C) (D) (E) | 72 (A) (B) (C) (D) (E) | 97 (A) (B) (C) (D) (E)  | 122 (A) (B) (C) (D) (E) |
| 23 (A) (B) (C) (D) (E) | 48 (A) (B) (C) (D) (E) | 73 (A) (B) (C) (D) (E) | 98 (A) (B) (C) (D) (E)  | 123 (A) (B) (C) (D) (E) |
| 24 (A) (B) (C) (D) (E) | 49 (A) (B) (C) (D) (E) | 74 (A) (B) (C) (D) (E) | 99 (A) (B) (C) (D) (E)  | 124 (A) (B) (C) (D) (E) |
| 25 (A) (B) (C) (D) (E) | 50 (A) (B) (C) (D) (E) | 75 (A) (B) (C) (D) (E) | 100 (A) (B) (C) (D) (E) | 125 (A) (B) (C) (D) (E) |

Question	Code	Answer
1	001	C ✓
2	001	C ✓
3	001	C ✓
4	001	D ✓
5	001	D ✓
6	001	C ✓
7	001	E ✓
8	001	B ✓
9	001	E ✓
10	001	E ✓
11	001	C ✓
12	001	D ✓
13	001	E ✓
14	001	D ✓
15	001	E ✓
16	001	E ✓
1	002	B
2	002	B
3	002	E
4	002	B
5	002	D
6	002	D
7	002	D
8	002	A
9	002	A
10	002	A
11	002	D
12	002	B
13	002	D
14	002	C
15	002	C
16	002	A

Question	Code	Answer
1	003	B
2	003	C
3	003	B
4	003	D
5	003	E
6	003	C
7	003	C
8	003	C
9	003	C
10	003	C
11	003	D
12	003	B
13	003	B
14	003	D
15	003	A
16	003	B
1	004	D
2	004	E
3	004	E
4	004	B
5	004	E
6	004	E
7	004	D
8	004	A
9	004	C
10	004	E
11	004	B
12	004	D
13	004	C
14	004	E
15	004	D
16	004	A