Chapter 10 Sinusoidal Steady- State Power Calculations

In Chapter 9 , we calculated the **steady state voltages** and currents in electric circuits driven by **sinusoidal sources**

We used **phasor method** to find the steady state **voltages** and currents

In this chapter, we consider power in such circuits

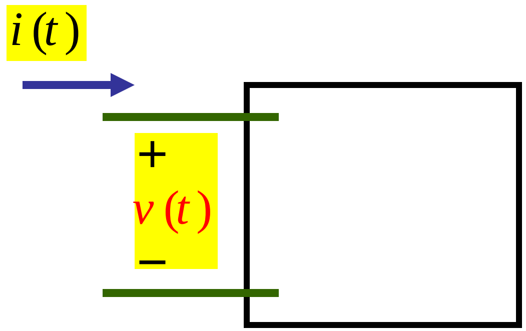
The techniques we develop are useful for analyzing many of the electric devices we encounter daily, because **sinusoidal sources** are predominate means of providing electric power in our homes, school and businesses

Examples

Electric Heater which transform electric energy to thermal energy
Electric Stove and oven
Toasters
Iron
Electric water heater
And many others

10.1 Instantaneous Power

Consider the following circuit represented by a black box



$$i(t) = I_m \cos(\omega t + \theta_i)$$

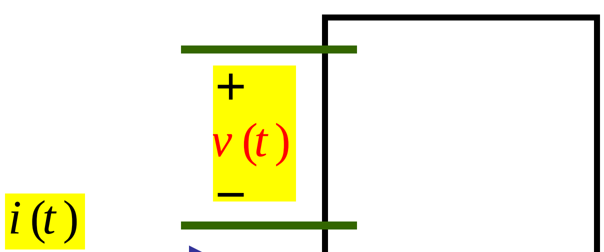
$$v(t) = V_m \cos(\omega t + \theta_v)$$

The instantaneous power assuming **passive sign convention**

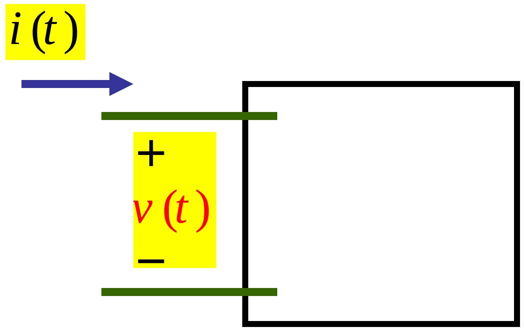
(Current in the direction of **voltage drop** + □ −)

$$p(t) = v(t)\,i(t) \qquad \text{(Watts)}$$

If the current is in the direction of **voltage rise (− □ +)** the instantaneous power is



$$p(t) = -\,v(t)\,i(t)$$



$$i(t) = I_m \cos(\omega t + \theta_i)$$

$$v(t) = V_m \cos(\omega t + \theta_v)$$

$$\Rightarrow \quad i(t) = I_m \cos(\omega t)$$

$$v(t) = V_m \cos(\omega t + \theta_v - \theta_i)$$

$$p(t) = v(t)i(t) = \{V_m \cos(\omega t + \theta_v - \theta_i)\}\{I_m \cos(\omega t)\}$$

$$= V_m I_m \cos(\omega t + \theta_v - \theta_i)\cos(\omega t)$$

Since

$$\cos\alpha\cos\beta = \frac{1}{2}\cos(\alpha-\beta) + \frac{1}{2}\cos(\alpha+\beta)$$

Therefore

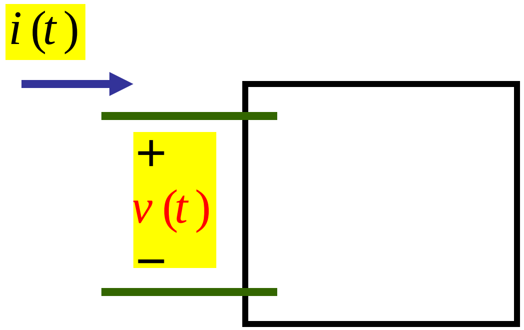
$$p(t) = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) + \frac{V_m I_m}{2}\cos(2\omega t + \theta_v - \theta_i)$$

Since

$$\cos(\alpha+\beta) = \cos\alpha\cos\beta - \sin\alpha\sin\beta$$

$$\Rightarrow \quad \cos(2\omega t + \theta_v - \theta_i) = \cos(\theta_v - \theta_i)\cos(2\omega t) - \sin(\theta_v - \theta_i)\sin(2\omega t)$$

$$\Rightarrow \quad p(t) = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) + \frac{V_m I_m}{2}\cos(\theta_v - \theta_i)\cos(2\omega t) - \frac{V_m I_m}{2}\sin(\theta_v - \theta_i)\sin(2\omega t)$$

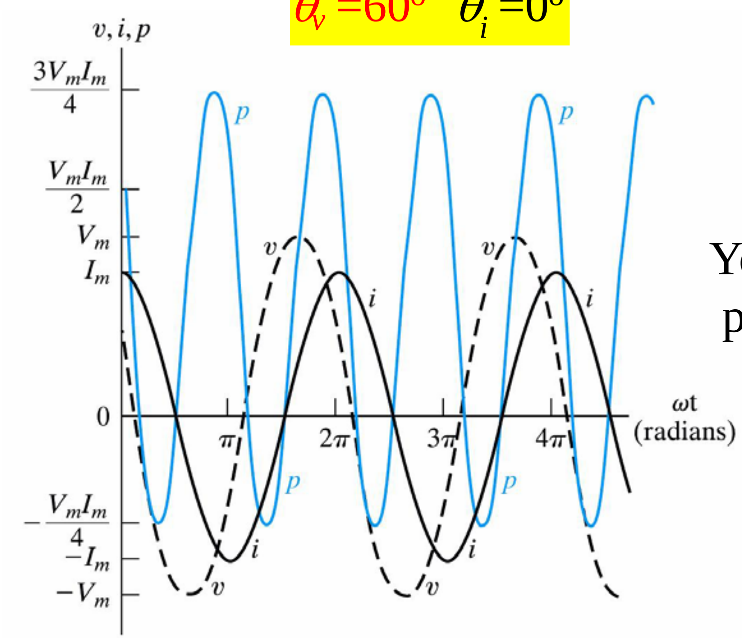


$i(t) = I_m \cos(\omega t)$

$v(t) = V_m \cos(\omega t + \theta_v - \theta_i)$

$$p(t) = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) + \frac{V_m I_m}{2}\cos(\theta_v - \theta_i)\cos(2\omega t) - \frac{V_m I_m}{2}\sin(\theta_v - \theta_i)\sin(2\omega t)$$

$\theta_v = 60^o \quad \theta_i = 0^o$



You can see that that the frequency of the Instantaneous power is twice the frequency of the voltage or current

10.2 Average and Reactive Power

Recall the Instantaneous power $p(t)$

$$p(t) = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) + \frac{V_m I_m}{2}\cos(\theta_v - \theta_i)\cos(2\omega t) - \frac{V_m I_m}{2}\sin(\theta_v - \theta_i)\sin(2\omega t)$$

$$p(t) = P + P\cos(2\omega t) - Q\sin(2\omega t)$$

where

$$P = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i)$$ Average Power (**Real Power**)

$$Q = \frac{V_m I_m}{2}\sin(\theta_v - \theta_i)$$ Reactive Power

Average Power P is sometimes called **Real power** because it describes the power in a circuit that is transformed from **electric** to **non electric** (**Example Heat**)

It is easy to see why P is called Average Power because

$$\frac{1}{T}\int_{t_0}^{t_0+T} p(t)dt = \frac{1}{T}\int_{t_0}^{t_0+T} \{ P + P\cos(2\omega t) - Q\sin(2\omega t)\}dt = P$$

Power for purely resistive Circuits

$$p(t) = P + P\cos(2\omega t) - Q\sin(2\omega t)$$

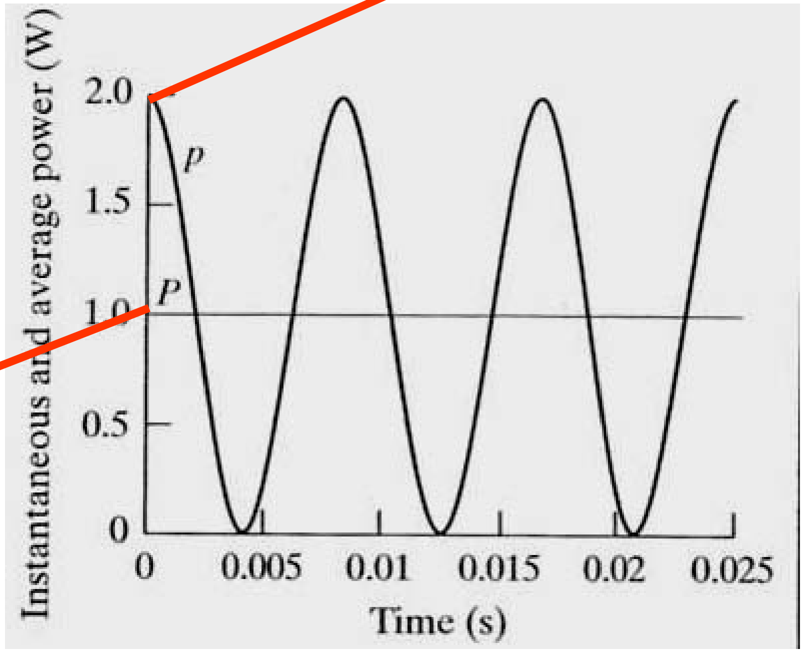
$\theta_v = \theta_i$ ⇨ $P = \dfrac{V_m I_m}{2}\cos(\theta_v - \theta_i) = \dfrac{V_m I_m}{2}\cos(0) = \dfrac{V_m I_m}{2}$

$$Q = \frac{V_m I_m}{2}\sin(\theta_v - \theta_i) = \frac{V_m I_m}{2}\sin(0) = 0$$

$V_m I_m$

⇨ $p(t) = \dfrac{V_m I_m}{2} + \dfrac{V_m I_m}{2}\cos(2\omega t)$

$\dfrac{V_m I_m}{2}$



The Instantaneous power can never be negative

⇨ power can not be extracted from a purely resistive network

Power for purely Inductive Circuits $p(t) = P + P\cos(2\omega t) - Q\sin(2\omega t)$

$\theta_v = \theta_i + 90^o$ ⇒ $\theta_v - \theta_i = 90^o$ ⇒ $P = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) = \frac{V_m I_m}{2}\cos(90^o) = 0$

⇒ $p(t) = -\frac{V_m I_m}{2}\sin(2\omega t)$

$Q = \frac{V_m I_m}{2}\sin(\theta_v - \theta_i) = \frac{V_m I_m}{2}\sin(90^o) = \frac{V_m I_m}{2}$

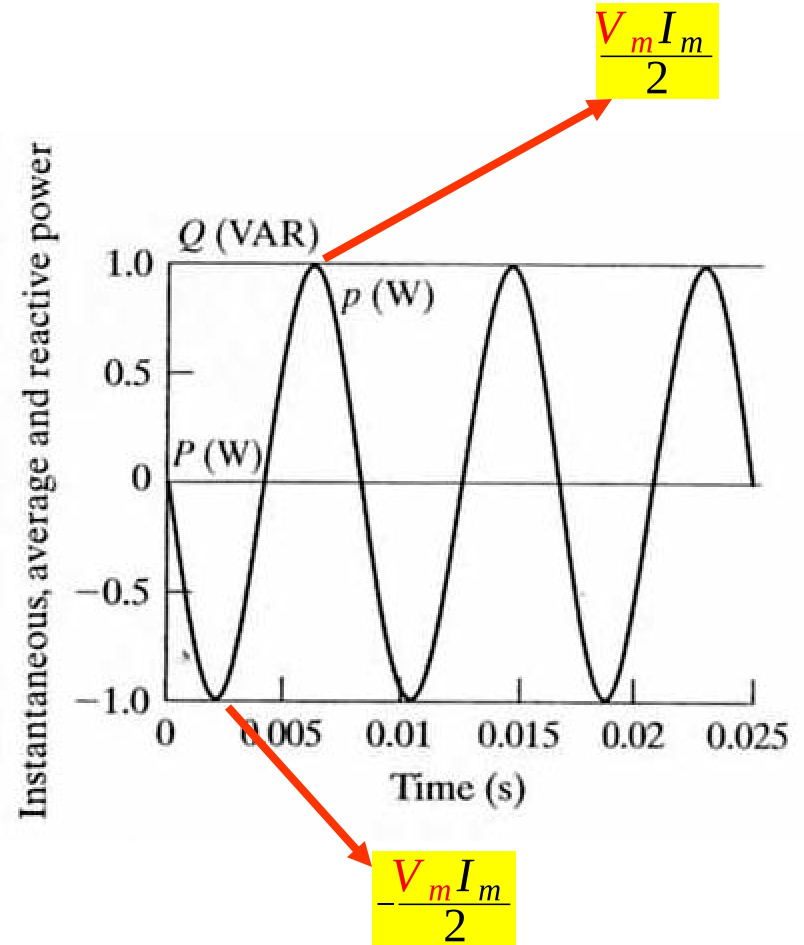
The Instantaneous power p(t) is continuously **exchanged** between the circuit and the source driving the circuit. **The average power is zero**

When p(t) is **positive**, energy is being **stored** in the **magnetic field** associated with the **inductive** element

When p(t) is **negative**, energy is being **extracted** from the **magnetic field**

The power associated with **purely inductive** circuits is the reactive power Q

The dimension of **reactive power** Q is the same as the average power P. To distinguish them we use the unit **VAR** (**V**olt **A**mpere **R**eactive) for **reactive power**



Power for purely Capacitive Circuits $p(t) = P + P\cos(2\omega t) - Q\sin(2\omega t)$

$\theta_v = \theta_i - 90^o$ ⟹ $\theta_v - \theta_i = -90^o$ ⟹ $P = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) = \frac{V_m I_m}{2}\cos(-90^o) = 0$

⟹ $p(t) = \frac{V_m I_m}{2}\sin(2\omega t)$ $Q = \frac{V_m I_m}{2}\sin(\theta_v - \theta_i) = \frac{V_m I_m}{2}\sin(-90^o) = -\frac{V_m I_m}{2}$

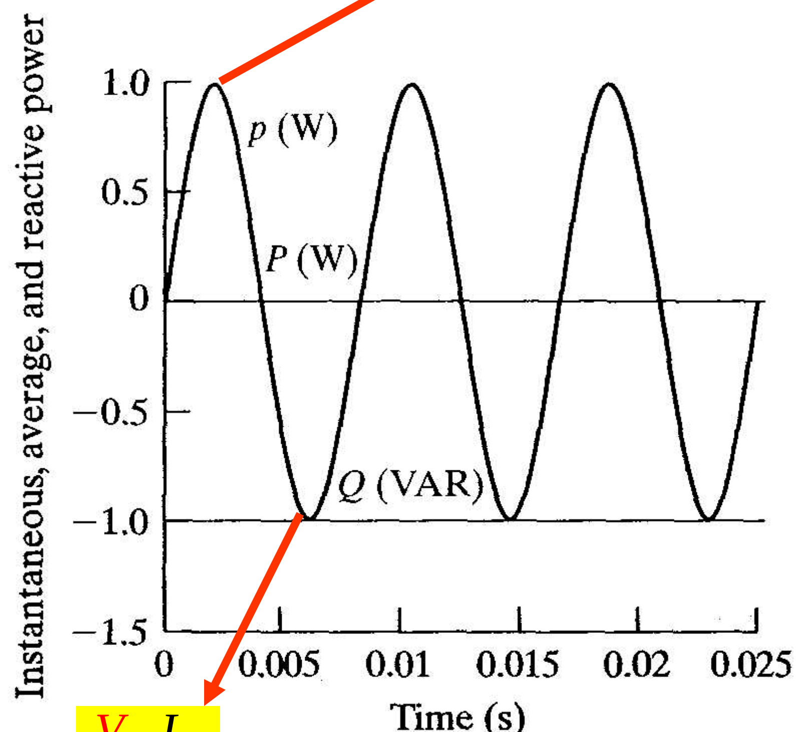
The Instantaneous power p(t) is continuously **exchanged** between the circuit and the source driving the circuit. **The average power is zero**

$\frac{V_m I_m}{2}$

When p(t) is **positive**, energy is being **stored** in the **electric field** associated with the **capacitive** element

When p(t) is **negative**, energy is being **extracted** from the **electric field**

The power associated with **purely capacitive** circuits is the reactive power Q (**VAR**)



$-\frac{V_m I_m}{2}$

The power factor

Recall the Instantaneous power p(t)

$$p(t) = \underbrace{\frac{V_m I_m}{2}\cos(\theta_v - \theta_i)}_{P \text{ average power}} + \underbrace{\frac{V_m I_m}{2}\cos(\theta_v - \theta_i)}_{P \text{ average power}}\cos(2\omega t) - \underbrace{\frac{V_m I_m}{2}\sin(\theta_v - \theta_i)}_{Q \text{ reactive power}}\sin(2\omega t)$$

$$= P + P\cos(2\omega t) - Q\sin(2\omega t)$$

The angle $\theta_v - \theta_i$ plays a role in the computation of both **average** and **reactive** power

The angle $\theta_v - \theta_i$ is referred to as the **power factor angle**

We now define the following :

The **power factor** $\quad \mathbf{pf} = \cos(\theta_v - \theta_i)$

The **reactive factor** $\quad \mathbf{rf} = \sin(\theta_v - \theta_i)$

The **power factor** $\mathbf{pf} = \cos(\theta_v - \theta_i)$

Knowing the power factor **pf** does not tell you the power factor angle , because

$$\cos(\theta_v - \theta_i) = \cos(\theta_i - \theta_v)$$

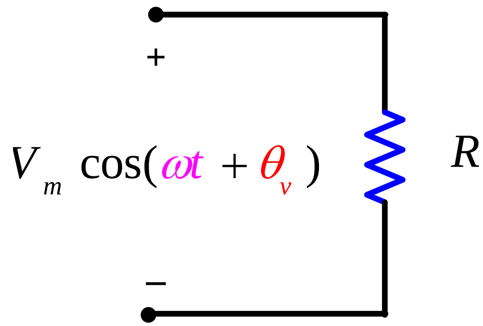
To completely describe this angle, we use the descriptive phrases **lagging power factor** and **leading power factor**

Lagging power factor implies that current **lags** voltage hence an inductive load

Leading power factor implies that current **leads** voltage hence a capacitive load

10.3 The rms Value and Power Calculations

Assume that a sinusoidal voltage is applied to the terminals of a resistor as shown



Suppose we want to determine the average power delivered to the resistor

$$P = \frac{1}{T}\int_{t_0}^{t_0+T} p(t)\,dt = \frac{1}{T}\int_{t_0}^{t_0+T} \frac{\left\{V_m \cos(\omega t + \theta_v)\right\}^2}{R}dt = \frac{1}{R}\left[\frac{1}{T}\int_{t_0}^{t_0+T} V_m^2 \cos^2(\omega t + \theta_v)\,dt\right]$$

However since $\quad V_{\text{rms}} = \sqrt{\frac{1}{T}\int_{t_0}^{t_0+T} V_m^2 \cos^2(\omega t + \theta_v)\,dt}$

$\Rightarrow \quad \boxed{P = \frac{V_{rms}^2}{R}}$ If the resistor carry sinusoidal current $\boxed{P = RI_{rms}^2}$

Recall the Average and Reactive power

$$P = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) \qquad Q = \frac{V_m I_m}{2}\sin(\theta_v - \theta_i)$$

Which can be written as

$$P = \frac{V_m I_m}{\sqrt{2}\sqrt{2}}\cos(\theta_v - \theta_i) \qquad Q = \frac{V_m I_m}{\sqrt{2}\sqrt{2}}\sin(\theta_v - \theta_i)$$

Therefore the Average and Reactive power can be written in terms of the **rms** value as

$$P = V_{\mathrm{rms}} I_{\mathrm{rms}}\cos(\theta_v - \theta_i) \qquad Q = V_{rms} I_{rms}\sin(\theta_v - \theta_i)$$

The **rms** value is also referred to as the **effective value eff**

Therefore the Average and Reactive power can be written in terms of the **eff** value as

$$P = V_{\mathrm{eff}} I_{\mathrm{eff}}\cos(\theta_v - \theta_i) \qquad Q = V_{\mathrm{eff}} I_{\mathrm{eff}}\sin(\theta_v - \theta_i)$$

Example 10.3

10.4 Complex Power

Previously, we found it convenient to introduce sinusoidal voltage and current in terms of the complex number the **phasor**

Definition

Let the **complex power** be the complex sum of real power and reactive power

$$\boldsymbol{S} = P + jQ$$

were

$\boldsymbol{S}$ is the complex power

P is the average power

Q is the reactive power

Advantages of using complex power $\boldsymbol{S} = P + jQ$

– We can compute the average and reactive power from the complex power $\boldsymbol{S}$

$$P = \Re\{\boldsymbol{S}\} \qquad Q = \Im\{\boldsymbol{S}\}$$

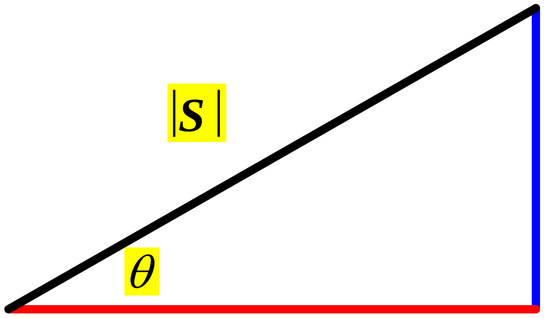
– complex power $\boldsymbol{S}$ provide a geometric interpretation

$$\boldsymbol{S} = P + jQ = |\boldsymbol{S}|\, e^{j\theta}$$

were

$$|\boldsymbol{S}| = \sqrt{P^2 + Q^2}$$

Is called **apparent power**



$$\theta = \tan^{-1}\left(\frac{Q}{P}\right) = \tan^{-1}\left(\frac{V_m I_m \cos(\theta_v - \theta_i)}{V_m I_m \sin(\theta_v - \theta_i)}\right) = \tan^{-1}\left(\frac{\cos(\theta_v - \theta_i)}{\sin(\theta_v - \theta_i)}\right) = \tan^{-1}\left(\tan(\theta_v - \theta_i)\right) = \underbrace{\theta_v - \theta_i}_{\text{power factor angle}}$$

The geometric relations for a right triangle mean the four power triangle dimensions ($|\boldsymbol{S}|$, P, Q, θ) can be determined if **any two** of the four are known

Example 10.4

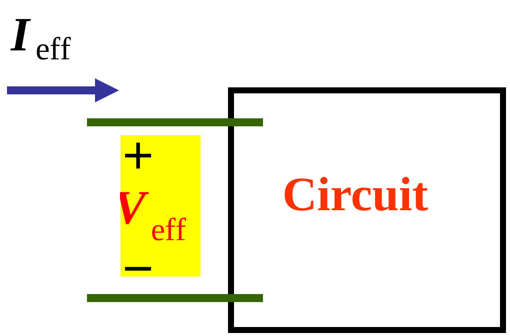
10.5 Power Calculations

$$\boldsymbol{S} = P + jQ = \frac{V_m I_m}{2}\cos(\theta_v - \theta_i) + j\,\frac{V_m I_m}{2}\sin(\theta_v - \theta_i)$$

$$= \frac{V_m I_m}{2}\left[\cos(\theta_v - \theta_i) + j\ \sin(\theta_v - \theta_i)\right] = \frac{V_m I_m}{2}\mathrm{e}^{j(\theta_v - \theta_i)} = V_{\text{eff}} I_{\text{eff}}\mathrm{e}^{j(\theta_v - \theta_i)}$$

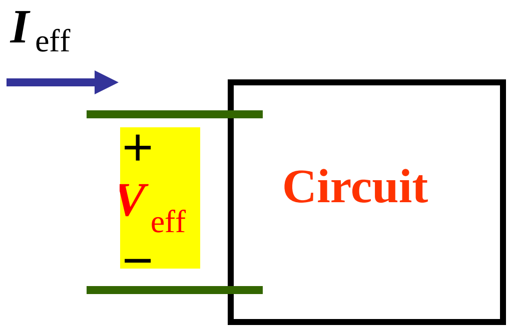
$$= V_{\text{eff}}\mathrm{e}^{j\theta_v} I_{\text{eff}}\mathrm{e}^{j\ \theta_i} \qquad \boxed{= \boldsymbol{V}_{\text{eff}}\boldsymbol{I}^{*}_{\text{eff}}}$$

were $\boldsymbol{I}^{*}_{\text{eff}}$ Is the conjugate of the current phasor $\boldsymbol{I}_{\text{eff}}$



Also $\boldsymbol{S} = \frac{1}{2}\,\boldsymbol{V}\boldsymbol{I}^{*}$

Alternate Forms for Complex Power



The complex power was **defined** as

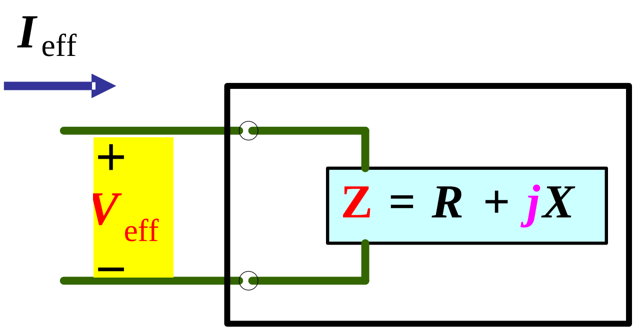
$$S = P + jQ$$

Then complex power was **calculated** to be

$$S = V_{\text{eff}} I^*_{\text{eff}} \quad \textbf{OR} \quad S = \frac{1}{2} V I^*$$

However there several useful variations as follows:

First variation

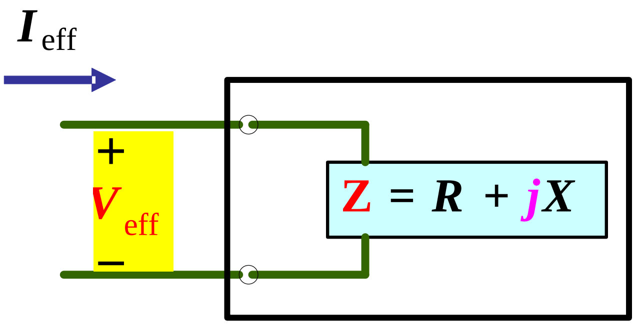


$$S = V_{\text{eff}} I^*_{\text{eff}} = (Z I_{\text{eff}}) I^*_{\text{eff}} = Z I_{\text{eff}} I^*_{\text{eff}} = Z |I_{\text{eff}}|^2$$

$$= (R + jX)|I_{\text{eff}}|^2 = \underbrace{R|I_{\text{eff}}|^2}_{P} + \underbrace{jX|I_{\text{eff}}|^2}_{Q}$$

$$P = R|I_{\text{eff}}|^2 = R I^2_{\text{eff}} = \frac{1}{2} R I^2_m \qquad Q = X|I_{\text{eff}}|^2 = X I^2_{\text{eff}} = \frac{1}{2} X I^2_m$$

Second variation



$$S = V_{\text{eff}} I_{\text{eff}}^* = V_{\text{eff}} \left(\frac{V_{\text{eff}}}{Z} \right)^* = \frac{V_{\text{eff}} V_{\text{eff}}^*}{Z^*} = \boxed{\frac{|V_{\text{eff}}|^2}{Z^*}}$$

$$= \frac{|V_{\text{eff}}|^2}{R - jX} = \frac{|V_{\text{eff}}|^2}{R - jX} \frac{R + jX}{R + jX} = \frac{R + jX}{R^2 + X^2} |V_{\text{eff}}|^2$$

$$= \underbrace{\frac{R}{R^2 + X^2} |V_{\text{eff}}|^2}_{P} + j \underbrace{\frac{X}{R^2 + X^2} |V_{\text{eff}}|^2}_{Q}$$

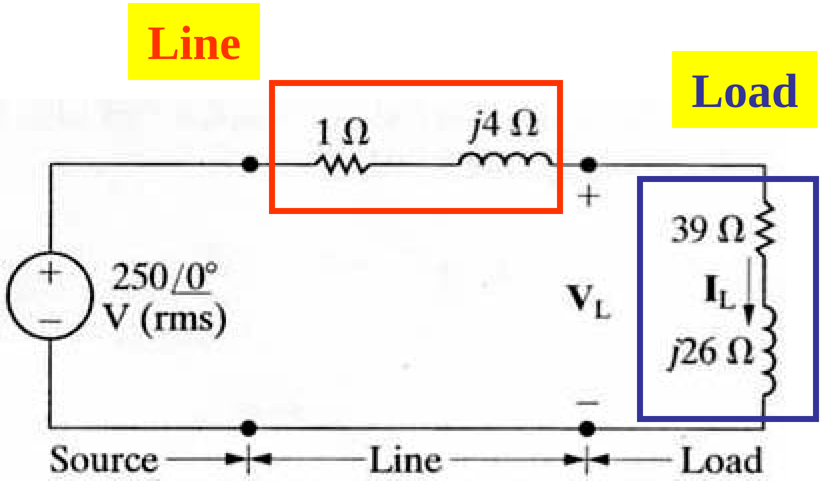
$$\Rightarrow \quad P = \frac{R}{R^2 + X^2} |V_{\text{eff}}|^2 = \frac{R}{R^2 + X^2} V_{\text{eff}}^2 = \frac{1}{2} \frac{R}{R^2 + X^2} V_m^2$$

$$Q = \frac{X}{R^2 + X^2} |V_{\text{eff}}|^2 = \frac{X}{R^2 + X^2} V_{\text{eff}}^2 = \frac{1}{2} \frac{X}{R^2 + X^2} V_m^2$$

If $Z = R$ (pure resistive) $X = 0$ $\Rightarrow$ $P = \dfrac{R}{R^2 + X^2} |V_{\text{eff}}|^2 = \dfrac{|V_{\text{eff}}|^2}{R}$ $\quad Q = 0$

If $Z = X$ (pure reactive) $R = 0$ $\Rightarrow$ $P = 0 \quad Q = \dfrac{X}{R^2 + X^2} |V_{\text{eff}}|^2 = \dfrac{|V_{\text{eff}}|^2}{X}$

Example 10.5



In the circuit shown a load having an impedance of $39 + j26\ \Omega$ is fed from a voltage source through a line having an impedance of $1 + j4\ \Omega$. The effective, or rms, value of the source voltage is 250 V.

a) Calculate the load current $\mathbf{I}_L$ and voltage $\mathbf{V}_L$.

SOLUTION

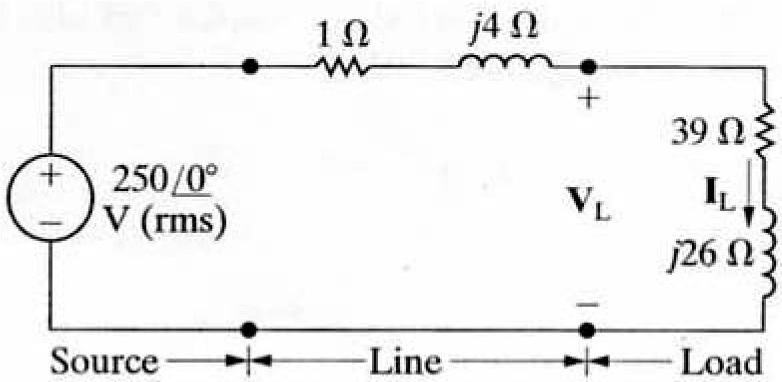
a) The line and load impedances are in series across the voltage source, so the load current equals the voltage divided by the total impedance, or

$$\mathbf{I}_L = \frac{250\angle 0^\circ}{40 + j30} = 4 - j3$$

$$= 5\angle -36.87^\circ \text{ A (rms)}$$

rms because the voltage is given in terms **of rms**

$$\mathbf{V}_L = (39 + j26)\mathbf{I}_L = 234 - j13 = 234.36\angle -3.18^\circ \text{ V (rms)}$$



$$\mathbf{I}_L = 4 - j3 = 5\angle{-36.87^\circ} \text{ A (rms)}$$

$$\mathbf{V}_L = 234 - j13 = 234.36\angle{-3.18^\circ} \text{ V (rms)}$$

b) Calculate the average and reactive power delivered to the load.

$$S = \mathbf{V}_L \mathbf{I}_L^* = (234 - j13)(4 + j3) = 975 + j650 \text{ VA}$$

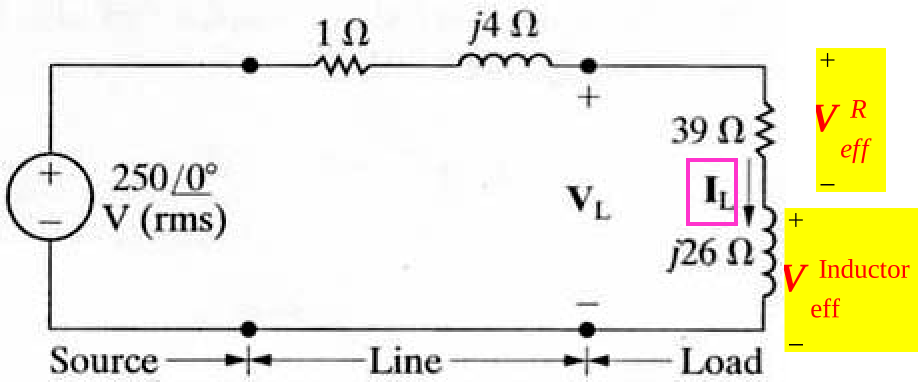
$P = 975$ W $\qquad Q = 650$ var

Another solution The load average power is the power absorb by the load resistor 39 Ω

Recall the average Power for purely resistive Circuits $P = \dfrac{V_m^R I_m^R}{2} = V_{eff}^R I_{eff}^R$

were V_{eff}^R and I_{eff}^R Are the **rms** voltage across the resistor and the **rms** current through the resistor

$$P = V_{eff}^R I_{eff}^R = R I_{eff}^2$$



$I_L = 4 - j3 = 5\angle{-36.87°}$ A (rms)

$V_L = 234 - j13 = 234.36\angle{-3.18°}$ V (rms)

$S = V_L I_L^* = (234 - j13)(4 + j3) = 975 + j650$ VA

$\Rightarrow$ $P = 975$ W

$Q = 650$ var

From Power for purely resistive Circuits

$$P = \frac{1}{2}V_m I_m = V_{eff} I_{eff} \Rightarrow P = |V^R_{eff}|\,|\overbrace{I^R_{eff}}^{I_L}| = V^R_{eff} I^R_{eff}$$

$$V^R_{eff} = \frac{39}{39 + j26} V_L = \frac{39}{39 + j26} 234.36e^{-j3.18°} = \underbrace{195}_{|V^R_{eff}|}e^{j36.87°} \Rightarrow V^R_{eff} = 195$$

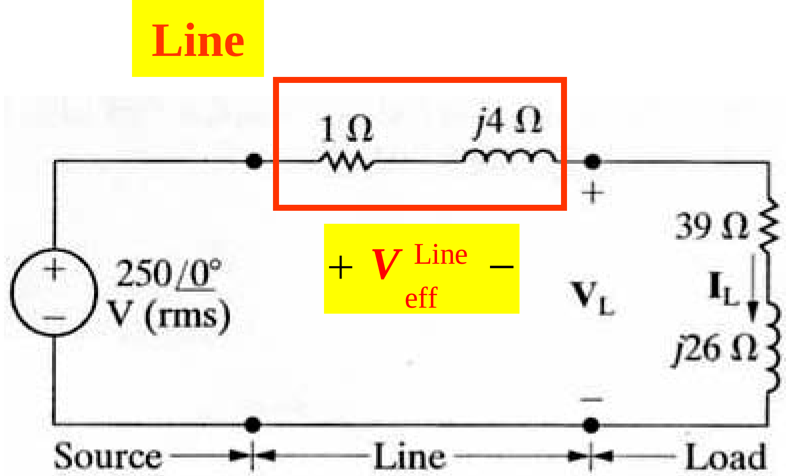
$$\Rightarrow P = V^R_{eff} I^R_{eff} = (195)(5) = 975 \text{ W}$$

OR $P = V^R_{eff} I^R_{eff} = (RI^R_{eff})I^R_{eff} = R(I^R_{eff})^2 = (39)(5^2) = (39)(25) = \mathbf{975\ \ W}$

$$Q = V_{eff} I_{eff} \Rightarrow Q = V^{Inductor}_{eff} \underbrace{I^{Inductor}_{eff}}_{I_L = 5} \qquad V^{Inductor}_{eff} = \frac{j26}{39 + j26} V_L = \frac{j26}{39 + j26} 234.36e^{-j3.18°} = 130e^{j93°}$$

$$\Rightarrow V^{Inductor}_{eff} = 130 \Rightarrow Q = (130)(5) = 650 \text{ VAR}$$

OR $Q = XI^2_{eff} = 650$ var



$\mathbf{I}_L = 4 - j3 = 5 \angle -36.87^\circ$ A (rms)

$\mathbf{V}_L = 234 - j13 = 234.36 \angle -3.18^\circ$ V (rms)

c) Calculate the average and reactive power delivered to the line.

$P = I_{\text{eff}}^2 \boldsymbol{R}$ ⇒ $P = (5)^2(1) = 25$ W,

$Q = I_{\text{eff}}^2 \boldsymbol{X}$ ⇒ $Q = (5)^2(4) = 100$ VAR

OR using complex power

$$\boldsymbol{S}_{\textbf{Line}} = \boldsymbol{V}_{\text{eff}}^{\text{Line}} \boldsymbol{I}_{\text{eff}}^{*}$$

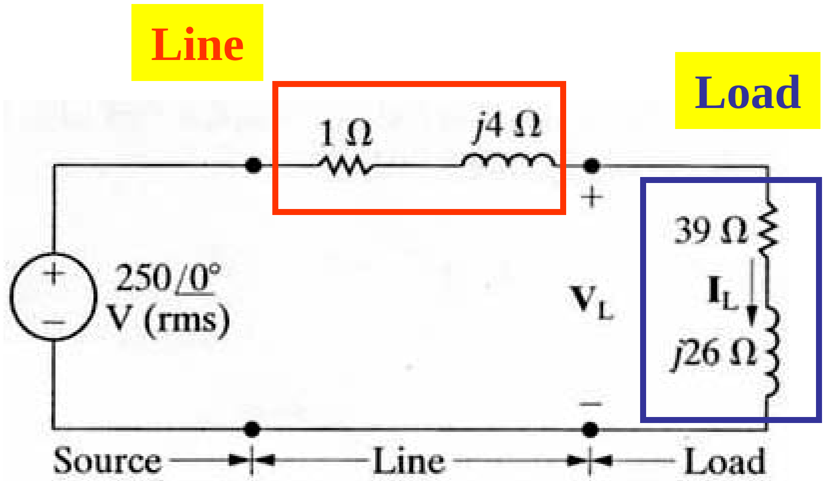
$$\boldsymbol{V}_{\text{eff}}^{\text{Line}} = \frac{1+j4}{(1+j4)+(39+j26)}(250)$$

OR

$$\boldsymbol{V}_{\text{eff}}^{\text{Line}} = 250 - \boldsymbol{V}_L$$

$$\boldsymbol{V}_{\text{eff}}^{\text{Line}} = 20.6 \angle 39.1^\circ \quad \text{V rms}$$

$$\boldsymbol{S}_{\textbf{Line}} = \boldsymbol{V}_{\text{eff}}^{\text{Line}} \boldsymbol{I}_{\text{eff}}^{*} = 20.6 \angle 39.1^\circ \quad 5 \angle 36.87^\circ = 103 \angle 75.97^\circ = 25 + j100 \quad \text{VA}$$



$$\mathbf{I}_L = 4 - j3 = 5\angle{-36.87^\circ} \text{ A (rms)}$$

$$\mathbf{V}_L = 234 - j13 = 234.36\angle{-3.18^\circ} \text{ V (rms)}$$

d) Calculate the average and reactive power supplied by the source.

$$\boldsymbol{S}_{\textbf{Absorb}} = \boldsymbol{S}_{Line} + \boldsymbol{S}_{Load} = \overbrace{(25 + j\,100)}^{\text{From part (c)}} + \overbrace{(975 + j\,650)}^{\text{From part (b)}} = (25 + 975) + j\,(100 + 650) = 1000 + j\,750 \quad \text{VA}$$

$$\boldsymbol{S}_{\textbf{Supply}} = -\boldsymbol{S}_{\textbf{Absorb}} = -(1000 + j\,750) \quad \text{VA}$$

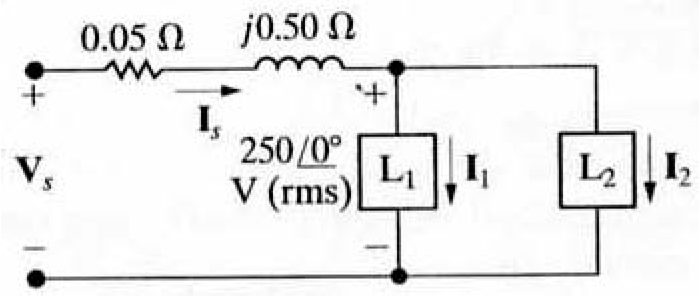
OR

$$\boldsymbol{S}_{\textbf{Supply}} = -250\angle 0^{\circ}\,(\boldsymbol{I}_L^*) = -250\angle 0^{\circ}\; 5\angle 36.87^\circ = \mathbf{-1250}\angle 36.87^{\circ} \quad \text{VA}$$

$$= -1000 - j\,750 \quad \text{VA}$$

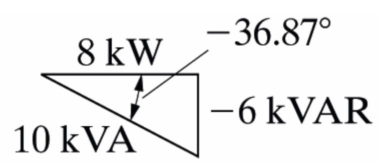
Example 10.6 Calculating Power in Parallel Loads

The two loads in the circuit shown can be described as follows: Load 1 absorbs an average power of 8 kW at a leading power factor of 0.8. Load 2 absorbs 20 kVA at a lagging power factor of 0.6.

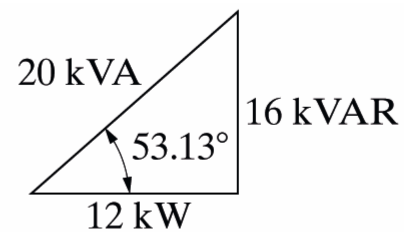


a) Determine the power factor of the two loads in parallel.

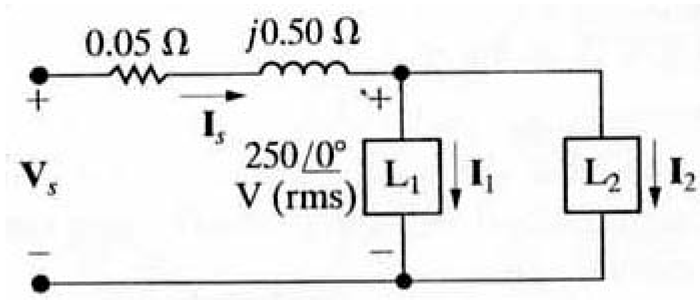
$\mathbf{I}_s = \mathbf{I}_1 + \mathbf{I}_2$ $\quad S = (250)\mathbf{I}_s^* \quad = (250)(\mathbf{I}_1 + \mathbf{I}_2)^* \quad = (250)\mathbf{I}_1^* + (250)\mathbf{I}_2^* \quad = S_1 + S_2$



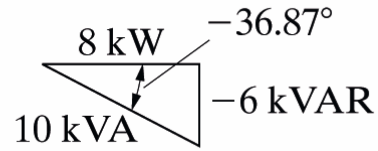
$$S_1 = 8000 - j\frac{8000(.6)}{(.8)} = 8000 - j6000 \text{ VA}$$



$$S_2 = 20{,}000(.6) + j20{,}000(.8) = 12{,}000 + j16{,}000 \text{ VA}$$

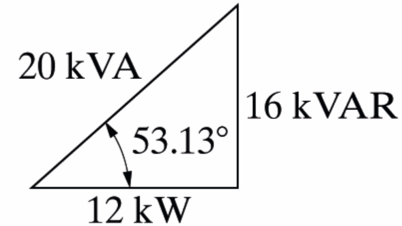


$$I_s = I_1 + I_2$$



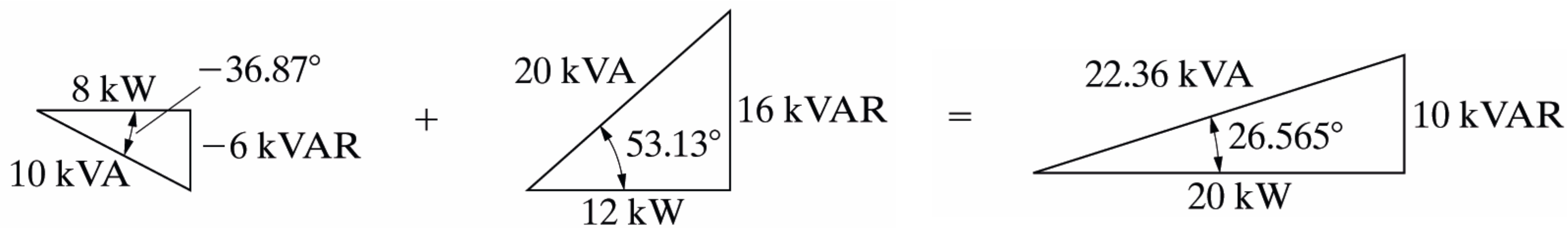
$$S_1 = 8000 - j\frac{8000(.6)}{(.8)}$$

$$= 8000 - j6000 \text{ VA}$$



$$S_2 = 20{,}000(.6) + j20{,}000(.8)$$

$$= 12{,}000 + j16{,}000 \text{ VA}$$



$$S = 20{,}000 + j10{,}000 \text{ VA}$$

$$I_s^* = \frac{20{,}000 + j10{,}000}{250} = 80 + j40 \text{ A}$$

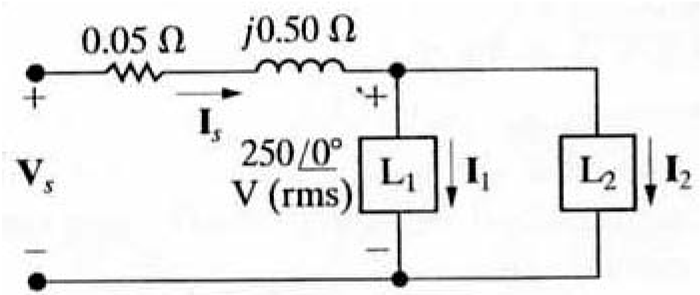
$$I_s = 80 - j40 = 89.44 \angle -26.57^\circ \text{ A}$$

$$\mathbf{pf} = \cos(\theta_v - \theta_i)$$

$$\text{pf} = \cos(0 + 26.57^\circ)$$

$$= 0.8944 \text{ lagging}$$

The power factor of the two loads in parallel is lagging because the net reactive power is positive.



b) Determine the apparent power required to supply the loads, the magnitude of the current, $\mathbf{I}_s$, and the average power loss in the transmission line.

$$\mathbf{I}_s = 80 - j40 = 89.44 \angle -26.57^\circ \text{ A}$$

$$\boldsymbol{S}_1 = 8000 - j6000 \quad \text{VA}$$

$$\boldsymbol{S}_2 = 12000 + j16000 \quad \text{VA}$$

$$\boldsymbol{S} = 20000 + j10000 \quad \text{VA}$$

The apparent power which must be supplied to these loads is

$$|\boldsymbol{S}| = |20000 + j10000| \quad \text{VA} = 22.36 \quad \text{kVA}$$

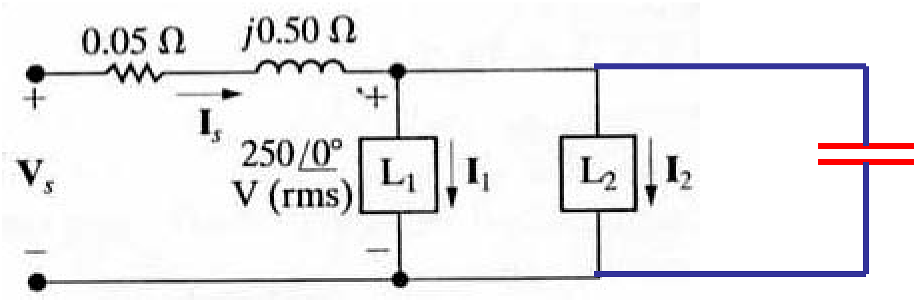
The magnitude of the current that supplies this apparent power is

$$|\mathbf{I}_s| = |80 - j40| = 89.44 \text{ A}$$

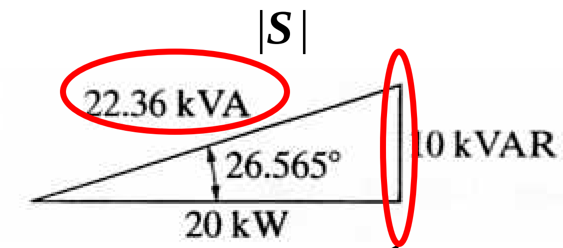
The average power lost in the line results from the current flowing through the line resistance

$$P_{\text{line}} = |\mathbf{I}_s|^2 R = (89.44)^2(0.05) = 400 \text{ W}$$

Note that the power supplied totals 20,000 + 400 = 20,400 W, even though the loads require a total of only 20,000 W.



C ?



c) Given that the frequency of the source is 60 Hz, compute the value of the capacitor that would correct the power factor to 1 if placed in parallel with the two loads. Recompute the values in (b) for the load with the corrected power factor.

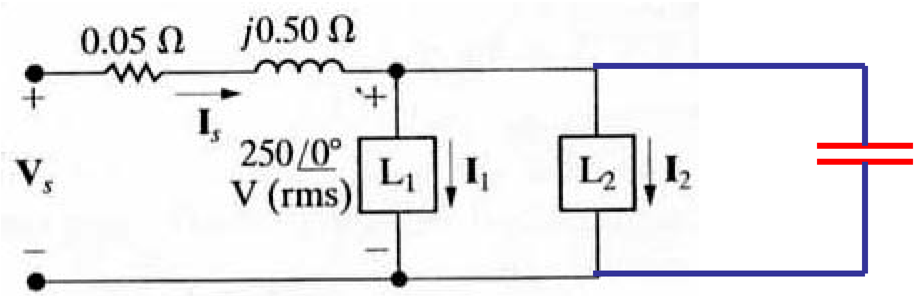
Will cancel this

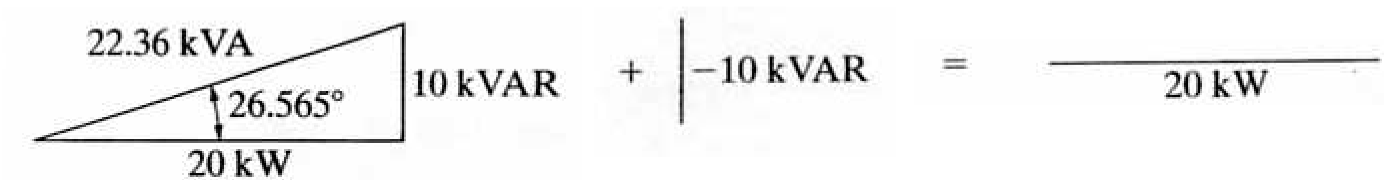
As we can see from the power triangle

We can correct the power factor to 1 if we place a capacitor in parallel with the existing load

the capacitive reactance $X = \dfrac{|V_{eff}|^2}{Q} = \dfrac{(250)^2}{-10{,}000} = -6.25\ \Omega.$

Recall that $X = -\dfrac{1}{\omega C}$ $\omega = 2\pi(60) = 376.99$ rad/s $C = \dfrac{-1}{\omega X} = \dfrac{-1}{(376.99)(-6.25)} = 424.4\ \mu F$





When the power factor is 1, the apparent power and the average power are the same

$$|S| = P = 20 \text{ kVA}$$

The magnitude of the current that supplies this apparent power is

$$|\mathbf{I}_s| = \frac{20{,}000}{250} = 80 \text{ A}$$

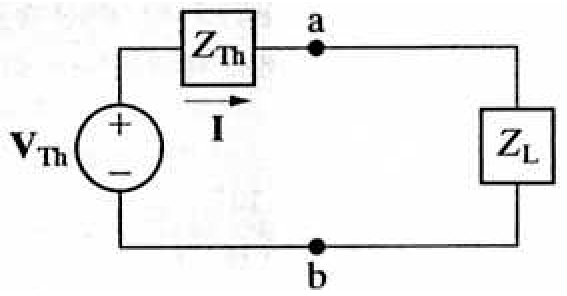
The average power lost in the line is thus reduced to

$$P_{\text{line}} = |\mathbf{I}_s|^2 R = (80)^2(0.05) = 320 \text{ W}$$

Now, the power supplied totals $20{,}000 + 320 = 20{,}320$ W

The addition of the capacitor has reduced the line loss from **400 W** to **320 W**

10.6 • Maximum Power Transfer



For maximum average power transfer, Z_L must equal the conjugate of the Thévenin impedance; that is, $\boxed{Z_L = Z_{Th}^*}$

Find Z_L that will absorb the maximum power

$$Z_{Th} = R_{Th} + jX_{Th} \qquad Z_L = R_L + jX_L$$

load current **I** is $$\mathbf{I} = \frac{\mathbf{V}_{Th}}{(R_{Th} + R_L) + j(X_{Th} + X_L)}$$

The average power delivered to the load is $P = |\mathbf{I}|^2 R_L$ $$P = \frac{|\mathbf{V}_{Th}|^2 R_L}{(R_{Th} + R_L)^2 + (X_{Th} + X_L)^2}$$

$$\frac{\partial P}{\partial X_L} = \frac{-|\mathbf{V}_{Th}|^2 2R_L(X_L + X_{Th})}{[(R_L + R_{Th})^2 + (X_L + X_{Th})^2]^2}$$

$$\frac{\partial P}{\partial R_L} = \frac{|\mathbf{V}_{Th}|^2[(R_L + R_{Th})^2 + (X_L + X_{Th})^2 - 2R_L(R_L + R_{Th})]}{[(R_L + R_{Th})^2 + (X_L + X_{Th})^2]^2}$$

$\partial P/\partial X_L$ is zero when $X_L = -X_{Th}$

$\partial P/\partial R_L$ is zero when $R_L = \sqrt{R_{Th}^2 + (X_L + X_{Th})^2} = \sqrt{R_{th}^2 + (\cancel{X_L} + \cancel{X_{th}})^2} = R_{th}$

$$Z_L = R_{th} - X_{th} = Z_{th}^*$$