1. Do Problems 3.9, 3.10 and 3.13 of textbook.


Reynolds number
Re $=\frac{\rho u_{m} D}{\mu}$
$=\frac{51 \times u_{m} \times \frac{2.067}{12}}{4.38 / 3600}$
$\mathrm{Re}=7,220 \mathrm{um}$
Case 2 -type problem


$$
u_{m}=\sqrt{\frac{D}{2 f_{f} \rho_{L}}\left[\left(p_{1}-p_{2}\right)-\rho_{c} \Delta z\right]}
$$

$$
\begin{aligned}
& =\sqrt{\frac{2.067 / 12}{2 f_{6} \times 51 \times 150}[\underbrace{15 \times 144 \times 32.2-51 \times 32.2 \times 20}_{36,708}]} \\
& =\frac{0.643}{\sqrt{f_{F}}}
\end{aligned}
$$

Now toughness ratio is $\frac{\varepsilon}{D}=\frac{0.00015 \times 12}{2.067}=8.71 \times 10^{-4}$ $\mathrm{ft} / \mathrm{s}$

| $u_{m}$ | $\operatorname{Re}$ | $f_{F}$ |
| :---: | :---: | :---: |
| - | - | 0.005 |
| 9.09 | 65,654 | 0.0057 |
| 8.52 | 61,491 | 0.0058 |
| 8.44 | 60,958 | 0.0058 |

$$
\begin{aligned}
Q & =\frac{\pi D^{2} u m}{4} u m \\
& =\frac{\pi}{4}\left(\frac{2.067}{12}\right)^{2} \times 8.44 \\
& =0.197 \times 60 \times 7.48 \\
Q & =88.3 \mathrm{gmm}
\end{aligned}
$$

3.10

Lodge Watet Supply


Pressute ©Drop $-\Delta p=z f_{f} \rho u_{m}^{2} \frac{L}{\partial}+\rho_{\rho} \Delta z$

$C^{B}=0.220 x^{3} b^{3}$

$$
8=0.000 \%-48
$$

 $4=3 \cdot 40$ 40

3.13

Pumping and Piping

Energy (2) $\rightarrow$ (3) $\frac{p_{3}-p_{2}}{p}+q\left(z_{3}-z_{2}\right)+2 f_{F} u_{m}^{2} \frac{\hbar}{D}=0$
How tare $Q=\frac{\pi^{2}}{4} u_{m}$ ot $u_{m}^{2}=\frac{16 Q^{2}}{\pi \pi^{2} D^{4}}$
Hence $p_{2}-p_{3}=\rho g\left(z_{3}-x_{2}\right)+\frac{32 f_{F} \rho Q^{2} L}{\pi^{2} D^{5}}$

$$
\begin{gathered}
=\frac{62.4 \times 32.2 \times 25}{32.2 \times 144}+\frac{32 f_{F} \times 62.4 \times Q^{2} \times 1000}{\pi^{2} \times\left(\frac{4.026}{12}\right)^{5} \times 32.2 \times 144} \\
p_{2}-p_{3}=10.83+10,265 f_{F} Q^{2}=\Delta p_{\text {pipe }}
\end{gathered}
$$

Ctost-section $A=\frac{\pi}{4}\left(\frac{4.026}{12}\right)^{2}=0.08844^{2}$
Roughness (comm. Steel) $k=\varepsilon=0.0018 \mathrm{~m} \quad \frac{\varepsilon}{D D}=\frac{0.0018}{4.026}=0.00045$
for large $\mathrm{Re}, \mathrm{F}_{\mathrm{F}}=0.0045$
Pump Equation $\Delta p_{\text {pump }}=19.2-133.4 \Phi^{4.5}$
Check on $f_{f} \quad u_{m}=\frac{0.38}{0.0884}=4.30$

| $\frac{Q}{\text { P. } 3 / \mathrm{sec}}$ | $\frac{\Delta p_{\text {pipe }}}{p_{\text {sic }}}$ |  |
| :---: | :---: | :---: |
| 0.3 | $\frac{\Delta p_{\text {pump }}}{p s i}$ |  |
| 0.3 .99 | 18.61 |  |
| 0.38 | 17.50 | 17.49 |
| 0.4 | 18.22 | 17.04 |

$$
\begin{aligned}
\mathrm{Re}_{\mathrm{Re}} & =\frac{62.4 \times 4.30 \times \frac{4.026}{12}}{1 \times 0.00672} \\
& =1.34 \times 10^{5} \\
f_{f} & =0.0045-\text { no change. }
\end{aligned}
$$

Further refinement not needed.
2. A $35^{\circ}$ API distillate is being transferred from a storage tank at 1 atm absolute pressure to a pressure vessel at 50 psig by means of the piping arrangements shown in figure. The liquid flows at the rate of $23100 \mathrm{lb} / \mathrm{hr}$ through 3 -inch Schedule 40 steel pipe; the length of the straight pipe is 450 feet. Calculate the minimum horsepower input to the pump having an efficiency of 60 percent. The properties of the distillate are: viscosity $=3.4 \mathrm{cP}$, density $=52 \mathrm{lb} / \mathrm{ft} 3$. The following are the data for the pipe and fittings:
a. For 3 inch Schedule 40 Nominal pipe, $O D=3.5$ inch; Thickness $=0.216$ inch
b. Flow coefficients for the fittings ( K ) are:
i. Gate valve $=0.25 ; 90$ o elbow $=0.9$; Check valve $=10$
c. Friction factor can be calculated from Blasius equation. Account for entry and exit losses also.


| Conversion Factors |  |  |  |
| ---: | :--- | ---: | :--- |
| 1 feet |  | 0.3048 | m |
| 1 lb |  | 0.454 | kg |
| 1 inch |  | 0.0254 | m |
| 1 centipoise |  | 0.001 | $\mathrm{~kg} / \mathrm{m} . \mathrm{sec}$ |
| 1 atm |  | 14.7 | psi |
| 1 atm |  | $1.01 \mathrm{E}+05$ | $\mathrm{~N} / \mathrm{m}^{2}$ |
| g |  | 9.812 | $\mathrm{~m} / \mathrm{sec}^{2}$ |


| Data given: |  |  |  | Converted data: |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mass flow rate |  | 23100 | $\mathrm{lb} / \mathrm{hr}$ | $=$ | 2.913167 | $\mathrm{kg} / \mathrm{sec}$ |
| Density | $\rho$ | 52 | $\mathrm{lb} / \mathrm{ft}^{3}$ | = | 833.7087 | kg/m ${ }^{3}$ |
| Viscosity | $\mu$ | 3.4 | cP | = | 0.0034 | kgm.sec |
| Pipe OD |  | 3.5 | inch |  |  |  |
| Pipe thickness |  | 0.216 | inch |  |  |  |
| Pipe length | L | 450 | feet | = | 137.16 | m |
| Vertical height | $\begin{gathered} \mathrm{z}_{1}- \\ \mathrm{z}_{2} \\ \hline \end{gathered}$ | 70 | feet | = | 21.336 | m |
| Pump efficiency (in fraction) |  | 0.6 |  |  |  |  |
|  |  |  |  |  |  |  |
| Loss coefficient of Gate Valve |  | 0.25 |  |  |  |  |
| Loss coefficient of elbow |  | 0.9 |  |  |  |  |
| Loss coefficient of check valve Valve |  | 10 |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Pipe ID | D | 3.068 | inch | = | 0.077927 | m |


| Pressure at 2 | $\mathrm{P}_{2}$ | 50 | psig | $=1$ | 344642.9 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{~N} / \mathrm{m}^{2}$ |  |  |  |  |  |

Calculations:

| Volumetric flow rate Velocity | Q v | $\begin{array}{r} \hline 0.00349 \\ 0.7326 \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{m}^{3} / \mathrm{sec} \\ & \mathrm{~m} / \mathrm{sec} \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Reynolds Number | NRe | 13999 |  |
| Friction factor | f | 0.00726 |  |
|  |  |  |  |
| $\mathrm{hf}_{\mathrm{f}}$ of pipe |  | 1.3985 | m |
|  |  |  |  |
| $\mathrm{v}^{2} / 2 \mathrm{~g}$ |  | 0.02735 | m |
| $\mathrm{h}_{\mathrm{f}}$ of Gate valve |  | 0.00684 | m |
| $\mathrm{h}_{\mathrm{f}}$ of 2 number of elbows |  | 0.04923 | m |
| $h_{\text {f }}$ of Check valve |  | 0.27351 | m |
|  |  |  |  |
| $h_{f}$ of sudden contraction at inlet |  | 0.01094 | m |
| $\mathrm{h}_{\mathrm{f}}$ of sudden expansion at outlet |  | 0.02735 | m |
| Total frictional head |  | 1.76642 | m |
|  |  |  |  |
| Pump head |  | 22.561 | m |
|  |  |  |  |
| Minimum power for the pump |  | 1074.81 | Watt |
|  |  |  |  |

