

**King Fahd University of Petroleum & Minerals, Electrical Engineering Department**

**EE 415: Analog Integrated Circuits Analysis And Design**

**Second Semester 2004-2005 (042), Midterm Exam Part (I)**

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Name	Key
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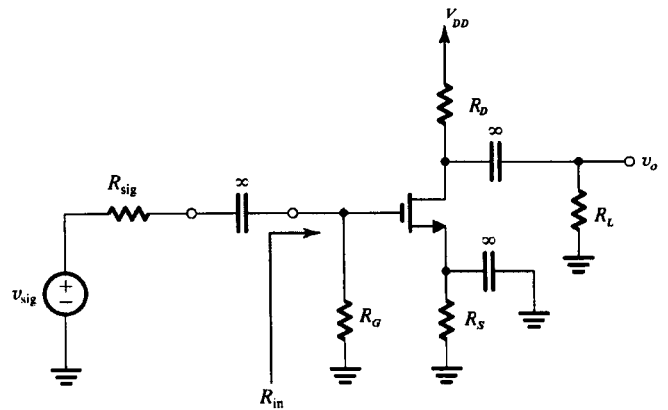
**Question # 1(7):**

For the MOSFET amplifier shown below,  $R_{sig}=100\text{ K}\Omega$ ,  $R_G=100\text{ K}\Omega$ ,  $C_{gs}=1\text{pF}$ ,  $C_{gd}=.20\text{pF}$ ,  $g_m=3\text{mA/V}$ ,  $r_{ds}=50\text{K}\Omega$ ,  $R_D=8\text{ K}\Omega$ , and  $R_L=10\text{ K}\Omega$ .

- Determine the midband gain ( $A_v=v_o/v_{sig}$ ) and the expected 3-dB cutoff frequency  $f_H$ . 4
- To double  $f_H$  a designer considers changing either  $R_{out}$  or  $R_{in}$ , evaluate the two options in terms of the change in the midband gain. 3

a) 
$$A_v = -\frac{R_G}{R_{sig} + R_G} g_m (R_D || R_L || r_{ds})$$

$$= -6.0 \text{ V/V}$$



$f_H =$

$\tau_1 = [C_{gs} + (1-A)C_{gd}] (R_G || R_{sig}) \rightarrow \tau_1 = 1.83 \times 10^{-7} \text{ sec}$

$A = -g_m (R_D || R_L || r_{ds}) = -12.3 \text{ V/V}$

$\tau_2 = \left[ \frac{C_{gd}}{(1-A)} \right] (R_D || R_L || r_{ds}) = 7.348 \times 10^{-11} \text{ sec}$

$\omega_H \approx \frac{1}{\tau_1} = 5.464 \times 10^6 \text{ rad/s} \Rightarrow f_H = 870 \text{ KHz}$

b)  $\omega_H \approx \frac{1}{[C_{gs} + (1-A)C_{gd}] (R_G || R_{sig})}$  to double  $f_H$   $\left\{ \begin{array}{l} \frac{A_{v2}}{2} \text{ using } R_{out} \\ \frac{R_G}{2} \text{ which is } R_{in} \end{array} \right.$

### Approach 1

Reducing  $C_1$  by making  $A_{new} = \frac{A}{2}$  (through  $R_{out}$ )

$R_{out} = R_D // R_{ds}$  if  $R_D$  is reduced to  $\approx 1.5 \text{ k}\Omega$

$$A_{new} = -3.8 \text{ V/V} \Rightarrow \omega_H = 10.2 \times 10^6 \text{ rad/s}$$

$$f_H = \underline{\underline{1.624 \text{ MHz}}}$$

$$A_V = \frac{R_G}{R_G + R_{sig}} A_{new} = \underline{\underline{-1.9 \text{ V/V}}}$$

### Approach 2

Reducing  $R_{G_{new}} = 33 \text{ k}\Omega$

$$\omega_H \approx \frac{1}{[C_{gs} + (1-A)C_{gd}](R_{G_{new}} // R_{sig})} = 11.01 \times 10^6 \text{ rad/s}$$

$$f_H = \underline{\underline{1.75 \text{ MHz}}}$$

$$A_V = \frac{R_{G_{new}}}{R_{G_{new}} + R_{sig}} A = \underline{\underline{-3.05 \text{ V/V}}}$$

Approach 2 is better than (1). It provides higher gain.

**Question # 2: (7)**

a) Design the current sources in the MOS amplifier shown in Fig. 1.

Use the current steering circuit shown in Fig. 2 which is fabricated in a technology with

$k'_n=90\mu\text{A}/\text{V}^2$ ,  $k'_p=30\mu\text{A}/\text{V}^2$ ,  $V_{tn}=0.8\text{V}$ ,  $V_{tp}=-0.9\text{V}$ ,  $V_A=50\text{V}$ .

If all devices have  $L=2\mu\text{m}$  and  $W_{Q1}=W_{Q3}=W_{Q4}=2\mu\text{m}$ .  $I_{REF}=20\mu\text{A}$ .

Find:  $R$ ,  $W_{Q2}$ ,  $W_{Q5}$  3

$$\left(\frac{W}{L}\right)_6 = \left(\frac{W}{L}\right)_7 = \frac{2\mu}{2\mu}$$

b) Determine the upper limit of  $v_o$ . 1

c) Find an expression for the voltage gain  $A_v=v_o/v_i$  in terms of  $g_{m6}$ ,  $g_{m7}$ ,  $r_{o6}$ ,  $r_{o7}$ ,  $r_{o2}$ ,  $r_{o5}$ . 2

d) Calculate the voltage gain  $A_v=v_o/v_i$  1

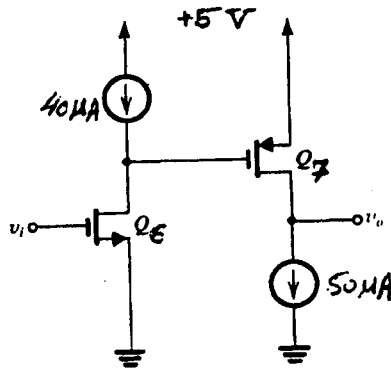


Fig. 1

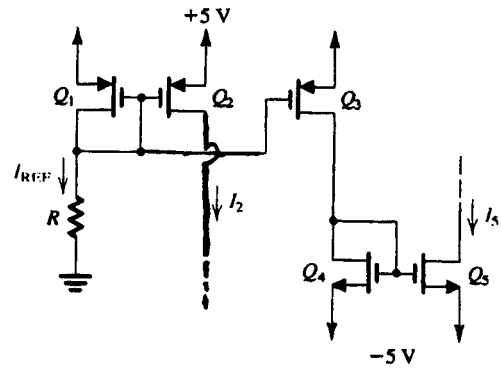


Fig. 2

Q2

$$a) I_{REF} = \frac{1}{2} K_n' \left(\frac{W}{L}\right)_1 (V_{GS1} - V_t)^2$$

$$20\mu = \frac{1}{2} (30\mu) \left(\frac{2}{2}\right) (V_{GS1} - 0.9)^2 \Rightarrow V_{GS1} = -2.05 \text{ V}$$

$$R = \frac{V_{DD} - V_{GS1}}{I_{REF}} = \frac{2.95}{20\mu} = \underline{\underline{147.26 \text{ k}\Omega}}$$

$$I_2 = 40\mu\text{A} \Rightarrow \frac{(W/L)_2}{(W/L)_1} = \frac{I_2}{I_1} = 2 \Rightarrow W_{Q2} = \underline{\underline{4\mu\text{m}}}$$

$$I_5 = 50\mu\text{A} \Rightarrow \frac{(W/L)_5}{(W/L)_4} = \frac{I_5}{I_4} = \frac{50\mu}{20\mu} = 2.5$$

$$W_{Q5} = \underline{\underline{5\mu\text{m}}}$$

$$b) V_{omax} = V_{DD} - V_{eff7} \quad ; \quad V_{eff7} = V_{GS7} - V_t$$

$$V_{eff7} = \sqrt{\frac{2 I_7}{K_p' \left(\frac{W}{L}\right)_7}} = \sqrt{\frac{2 \times 50\mu}{30\mu \times \left(\frac{2}{2}\right)}} = \sqrt{\frac{100\mu}{30\mu}} = 1.83 \text{ V}$$

$$V_{omax} = 5 - 1.83 = 3.17 \text{ V}$$

$$c) \frac{V_o}{V_i} = \left[ -g_{m6} (r_{ds6} \parallel r_{ds2}) \right] \left[ -g_{m7} (r_{ds7} \parallel r_{ds5}) \right]$$

$$= g_{m6} g_{m7} (r_{ds6} \parallel r_{ds2}) (r_{ds7} \parallel r_{ds5})$$

$$d) g_{m6} = \sqrt{2 K_n' \left(\frac{W}{L}\right)_6 I_{D6}} = \sqrt{2 \times 90\mu \times 40\mu} = 84.8 \mu\text{A/V}$$

$$g_{m7} = \sqrt{2 K_p' \left(\frac{W}{L}\right)_7 I_{D7}} = \sqrt{2 \times 30\mu \times 50\mu} = 54.8 \mu\text{A/V}$$

Q2

$$r_{ds6} = r_{ds2} = \frac{V_A}{I_{D2,6}} = \frac{50}{40\mu} = 1.25 M\Omega ;$$

$$r_{ds7} = r_{ds5} = \frac{V_A}{I_{D7,5}} = \frac{50}{50\mu} = 1 M\Omega$$

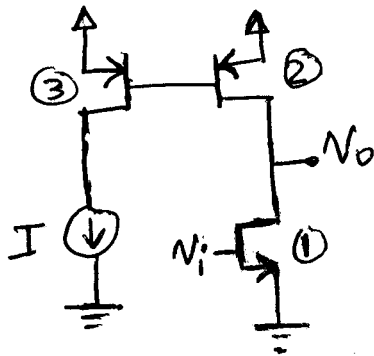
$$\frac{v_o}{v_i} = 84.8 \mu \times 54.8 \mu \times (1.25 M \parallel 1.25 M) (1 M \parallel 1 M)$$
$$= 1452.2 \quad v/v$$

**Question # 3: (6)**

Assuming that MOSFETs used in the following designs have  $g_m$  on the order of  $0.75\text{mA/V}$  and  $r_{ds}$  on the order of  $100\text{k}\Omega$ ,

- Draw an integrated circuit common source amplifier and estimate its voltage gain. 2
- Draw an integrated circuit cascode amplifier and estimate its voltage gain. 2
- Compare the two configurations in terms of gain and output voltage swing. 2

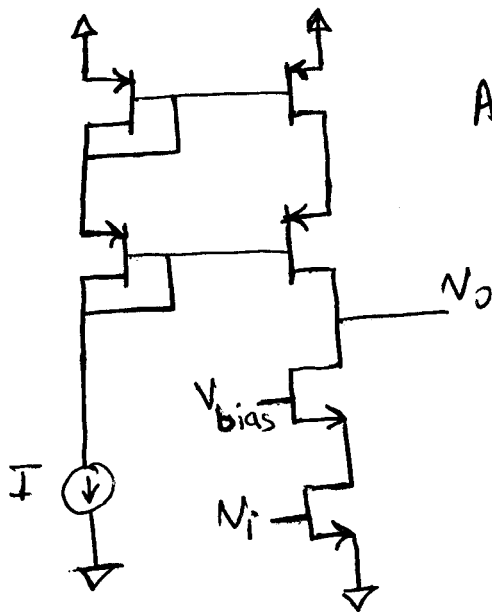
a)



$$A_v = \frac{V_o}{V_i} = -g_{m1}(r_{ds1} || r_{ds2})$$

$$= -0.75\text{m}(100\text{k} || 100\text{k}) = -37.5$$

b) Cascode



$$A_v = \frac{V_o}{V_i} = -\frac{g_m^2 r_{ds}^2}{2} = -703.1 \text{ V/V}$$

c) As indicated in parts a & b:

cascode amplifier has a higher voltage gain.

in terms of voltage swing, it is known that simple common source Amplifier has a wider voltage swing