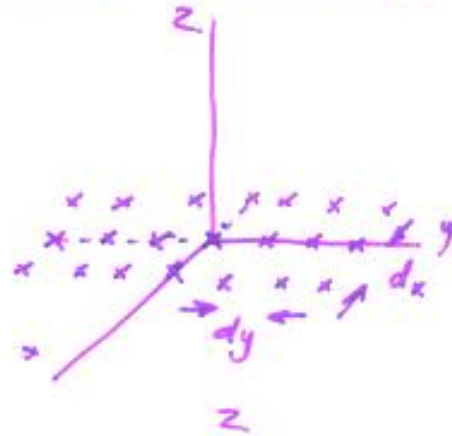
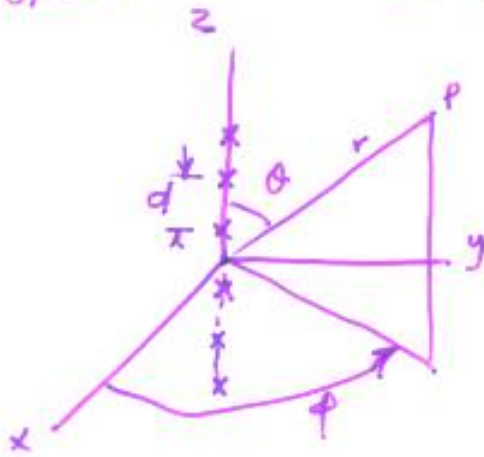
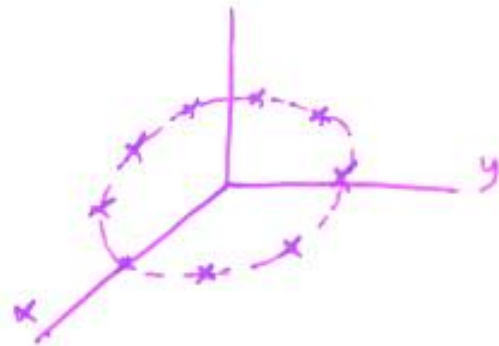


ANTENNA ARRAYS

Types! Linear, Planar, Circular



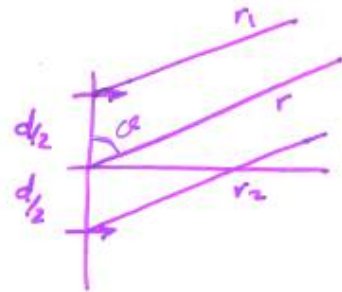
The control variables in an array of identical elements!



1. Geometrical configuration
2. Relative displacement between elements
3. Excitation amplitude
4. Excitation phase
5. Relative pattern of the individual elements.

Two-element Array

2 infinitesimal dipoles



$$E_t = E_1 + E_2$$

$$= \hat{a}_\theta j\eta \frac{kI_0 l}{4\pi} \left\{ \frac{e^{-j[kr_1 - \beta/2]}}{r_1} |\cos\theta| + \frac{e^{-j[kr_2 + \beta/2]}}{r_2} |\cos\theta| \right\}$$

$\beta \rightarrow$ the phase difference between the elements.

Using the far field approximation

$$\begin{aligned} \theta_1 &\approx \theta_2 \approx \theta \\ r_1 &\approx r - \frac{d}{2} \cos\theta \\ r_2 &\approx r + \frac{d}{2} \cos\theta \end{aligned} \left. \begin{array}{l} \text{phase} \\ \text{amplitude} \end{array} \right\}$$

$$\therefore E_t = \hat{a}_\theta j\eta \frac{kI_0 l e^{-jkr}}{4\pi r} |\cos\theta| \left[e^{j\frac{kd\cos\theta + \beta}{2}} + e^{-j\frac{kd\cos\theta + \beta}{2}} \right]$$

$$= \hat{a}_\theta j\eta \frac{kI_0 l e^{-jkr}}{4\pi r} |\cos\theta| 2 \cos \left[\frac{1}{2}(kd\cos\theta + \beta) \right]$$

= element factor \times array factor

$$AF = 2 \cos \left[\frac{1}{2}(kd\cos\theta + \beta) \right]$$

$$\text{or } AF_n = \cos \left[\frac{1}{2}(kd\cos\theta + \beta) \right]$$

Example: for the 2 element array, find the nulls of the total field when $d = \lambda/4$ and $\beta = 0, +\frac{\pi}{2}, -\frac{\pi}{2}$

$$a) \quad \beta = 0 \rightarrow E_{tn} = |\cos \theta| \cos\left(\frac{\pi}{4} \cos \theta\right)$$

$$\text{Nulls} \rightarrow E_{tn} = 0 = |\cos \theta| \cos\left(\frac{\pi}{4} \cos \theta\right)$$

$$\therefore \cos \theta_n = 0 \rightarrow \theta_n = 90^\circ$$

$$\text{also } \cos\left(\frac{\pi}{4} \cos \theta_n\right) = 0 \rightarrow \frac{\pi}{4} \cos \theta_n = \frac{\pi}{2}, -\frac{\pi}{2}$$

does not exist.

\therefore only one null at $\theta_n = 90^\circ$.

$$b) \quad \beta = \frac{\pi}{2} \rightarrow E_{tn} = |\cos \theta| \cos\left[\frac{\pi}{4}(\cos \theta + 1)\right]$$

$$\therefore \cos \theta_n = 0 \rightarrow \theta_n = 90^\circ$$

$$\text{also } \frac{\pi}{4}(\cos \theta_n + 1) = \frac{\pi}{2} \rightarrow \cos \theta_n = 1 \rightarrow \theta_n = 0^\circ$$

$$c) \quad \beta = -\frac{\pi}{2} \rightarrow E_{tn} = |\cos \theta| \cos\left[\frac{\pi}{4}(\cos \theta - 1)\right]$$

$$\therefore \cos \theta_n = 0 \rightarrow \theta_n = 90^\circ$$

$$\text{also } \frac{\pi}{4}(\cos \theta_n - 1) = -\frac{\pi}{2} \rightarrow \theta_n = 180^\circ$$

General 2-element array nulls:

$$E_{tn} = |\cos \theta| \cos\left[\frac{1}{2}(kd \cos \theta + \beta)\right]$$

$$\therefore E_{tn} = 0 \rightarrow \cos \theta_n = 0 \rightarrow \theta_n = 90^\circ$$

$$\text{Also when } \cos\left[\frac{1}{2}(kd \cos \theta + \beta)\right] = 0 \rightarrow \frac{1}{2}(kd \cos \theta + \beta) = \pm \frac{2n+1}{2}\pi$$

$$\therefore \theta_n = \cos^{-1}\left[\frac{1}{kd}\{-\beta \pm (2n+1)\pi\}\right] \quad n = 0, 1, 2, \dots$$

N-element Linear Array (uniform)

$$AF = 1 + e^{j(kd\cos\theta + \beta)} + e^{j2(kd\cos\theta + \beta)} + \dots + e^{j(N-1)(kd\cos\theta + \beta)}$$

$$= \sum_{n=1}^N e^{j(n-1)(kd\cos\theta + \beta)}$$

$$\therefore AF = \sum_{n=1}^N e^{j(n-1)\psi}, \quad \psi = kd\cos\theta + \beta.$$

$$= 1 + e^{j\psi} + e^{j2\psi} + \dots + e^{j(N-1)\psi}$$

$$AF e^{j\psi} = e^{j\psi} + e^{j2\psi} + e^{j3\psi} + \dots + e^{jN\psi}$$

$$\therefore AF = \frac{e^{jN\psi} - 1}{e^{j\psi} - 1} = e^{j\frac{N-1}{2}\psi} \frac{\sin \frac{N\psi}{2}}{\sin \frac{\psi}{2}}$$

Moving Reference to the Centre of Array:

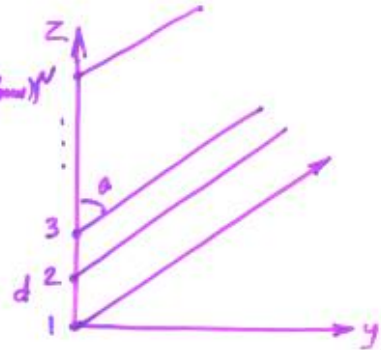
$$\therefore AF_n = \frac{1}{N} \frac{\sin \frac{N\psi}{2}}{\sin \frac{\psi}{2}}$$

for small values of $\psi \rightarrow AF_n \approx \frac{\sin \frac{N\psi}{2}}{\frac{N\psi}{2}}$

Nulls $\sin \frac{N\psi}{2} = 0 \rightarrow \frac{N\psi}{2} = \pm n\pi$

$$\therefore \theta_n = \cos^{-1} \left[\frac{\lambda}{2\pi d} (-\beta \pm \frac{2n}{N}\pi) \right]$$

for $n = 1, 2, 3, \dots$ & $n \neq N, 2N, \dots$



Max. values occur $\rightarrow \frac{\Psi}{2} = \frac{1}{2} (kd \cos \theta + \beta) = \pm m\pi$

$$\text{or } \theta_m = \cos^{-1} \left[\frac{\lambda}{2\pi d} (-\beta \pm 2m\pi) \right]$$

$$m = 0, 1, 2, \dots$$

for small Ψ $Af = \frac{\sin \frac{N\Psi}{2}}{\frac{N\Psi}{2}} \rightarrow$ only one max.

$$\text{at } \rightarrow \theta_m = \cos^{-1} \left(\frac{\lambda \beta}{2\pi d} \right) \quad (\text{when } m=0)$$

3dB points $\frac{N\Psi}{2} = \frac{N}{2} (kd \cos \theta + \beta) = \pm 1.391$
 $\theta = \theta_h$

$$\therefore \theta_h = \cos^{-1} \left[\frac{\lambda}{2\pi d} \left(-\beta \pm \frac{2.782}{N} \right) \right]$$

also can be written as $\theta_h = \frac{\pi}{2} - \sin^{-1} \left[\frac{\lambda}{2\pi d} \left(-\beta \pm \frac{2.782}{N} \right) \right]$

for large d ($d \gg \lambda$) $\theta_h \approx \left[\frac{\pi}{2} - \frac{\lambda}{2\pi d} \left(-\beta \pm \frac{2.782}{N} \right) \right]$

$$\therefore \text{HPBW} = 2 | \theta_m - \theta_h |$$

Maximum of 1st minor lobe $\rightarrow \frac{N\Psi}{2} \approx \pm \frac{3\pi}{2}$

$$\therefore \frac{N}{2} (kd \cos \theta + \beta) \approx \pm \frac{3\pi}{2}$$

$$\text{or } \theta_s = \cos^{-1} \left\{ \frac{\lambda}{2\pi d} \left[-\beta \pm \frac{3\pi}{N} \right] \right\}$$

$$A.F. \text{ at this point} = \frac{\sin \frac{N\Psi}{2}}{\frac{N\Psi}{2}} = \frac{2}{3\pi} = 0.212 \quad (= -13.46 \text{ dB})$$

Broadside Arrays

AF max occurs when $\psi = 0 = kd \cos \theta + \beta$

for $\theta = 90^\circ \rightarrow \beta = 0^\circ$ for broadside condition

end fire arrays

AF maximum in the direction $\theta = 0^\circ$ or 180° .

$$\therefore \psi = kd \cos \theta + \beta \Big|_{\theta=0^\circ} = kd + \beta \rightarrow \beta = -kd$$

$$\text{or } \psi = kd \cos \theta + \beta \Big|_{\theta=180^\circ} = -kd + \beta \rightarrow \beta = +kd$$

phased (scanned) Arrays

$$\psi = kd \cos \theta + \beta \Big|_{\theta=\theta_0} = 0 \rightarrow \beta = -kd \cos \theta_0$$

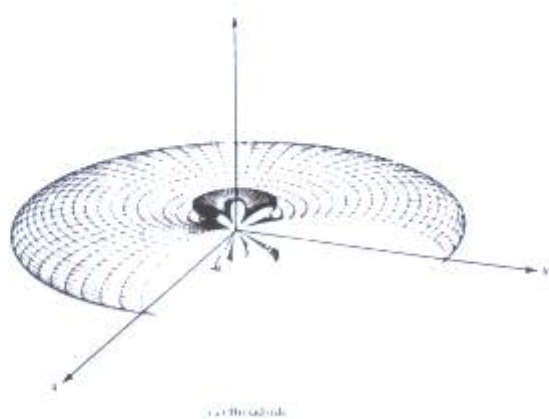


Figure 6.6 Three-dimensional amplitude patterns for broadside, and broadside/end-fire arrays.

$$AF_n = \frac{\sin 5\psi}{10 \sin \frac{\psi}{2}}$$

$$\psi = kd \cos \theta + \beta$$

$$\beta = 0$$

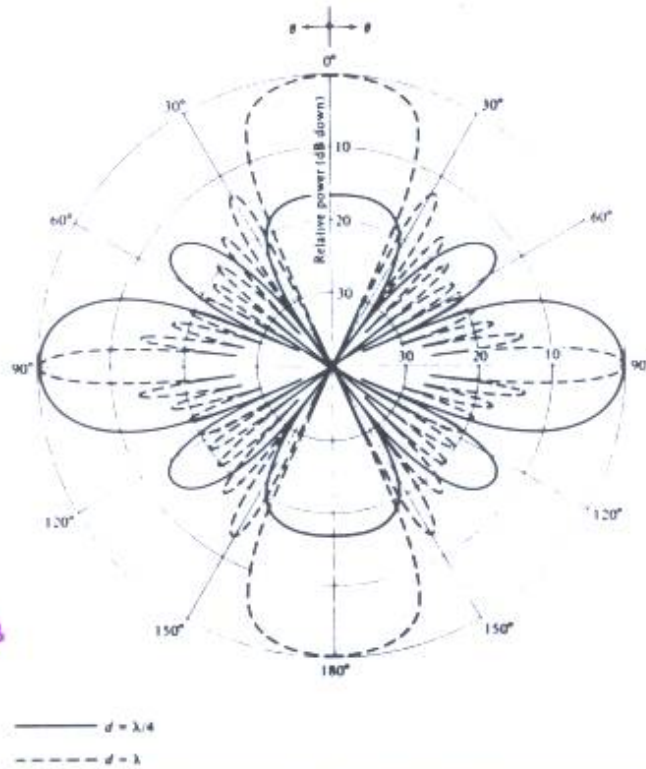


Figure 6.7 Array factor patterns of a 10-element uniform amplitude broadside array ($N = 10, \beta = 0$).

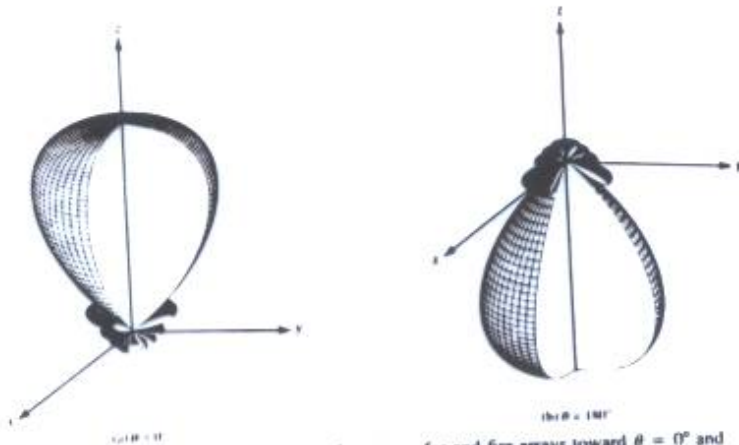


Figure 6.8 Three-dimensional amplitude patterns for end-fire arrays toward $\theta = 0^\circ$ and 180° .

$$AF_n = \frac{\sin 5\psi}{10 \sin \frac{\psi}{2}}$$

$$\psi = kd \cos \theta + \beta$$

$$= kd \cos \theta - kd \cos \theta_0$$

$$d = \frac{\lambda}{4}$$

$$\psi = \frac{\pi}{2} \left(\cos \theta - \frac{1}{2} \right)$$

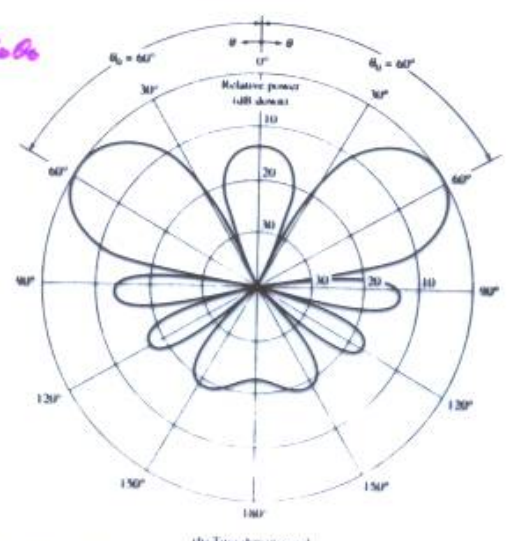


Figure 6.10 Three- and two-dimensional array factor patterns of a 10-element uniform amplitude scanning array ($N = 10$, $\beta = -kd \cos \theta_0$, $\theta_0 = 60^\circ$, $d = \lambda/4$.)

Directivity of B.S. & E.F. Linear Arrays

1. B.S. uniform array:

$$(AF)_n = \frac{\sin \left[\frac{N}{2} kd \cos \theta \right]}{N \sin \left[\frac{1}{2} kd \cos \theta \right]}$$

for $d \ll \lambda$ "Large array"

$$(AF)_n \approx \frac{\sin \left[\frac{N}{2} kd \cos \theta \right]}{\left[\frac{N}{2} kd \cos \theta \right]}$$

$$\text{Radiation intensity} \rightarrow U(\theta) = [(AF)_n]^2 = \left[\frac{\sin Z}{Z} \right]^2$$

$$\text{where } Z = \frac{N}{2} kd \cos \theta$$

$$\therefore U_{\max} = 1 \quad \text{for } \theta_{\max} = \frac{\pi}{2}$$

$$\begin{aligned} \therefore U_0 &= \frac{1}{4\pi} \text{Prad} = \frac{1}{2} \int_0^\pi \left[\frac{\sin Z}{Z} \right]^2 \sin \theta \, d\theta \\ &= \frac{1}{2} \int_0^\pi \left[\frac{\sin \left(\frac{N}{2} kd \cos \theta \right)}{\left(\frac{N}{2} kd \cos \theta \right)} \right]^2 \sin \theta \, d\theta \end{aligned}$$

Change variable to $Z = \frac{N}{2} kd \cos \theta$

$$\therefore dz = -\frac{N}{2} kd \sin \theta \, d\theta$$

$$\therefore U_0 = \frac{1}{Nkd} \int_{\frac{Nkd}{2}}^{-\frac{Nkd}{2}} \left[\frac{\sin Z}{Z} \right]^2 dz = \frac{1}{Nkd} \int_{-\frac{Nkd}{2}}^{\frac{Nkd}{2}} \left[\frac{\sin Z}{Z} \right]^2 dz$$

(10)

For a large array i.e. $\frac{Nkd}{2} \rightarrow \text{large}$

$$\therefore U_0 \approx \frac{1}{Nkd} \int_{-\infty}^{\infty} \left[\frac{\sin Z}{Z} \right]^2 dz$$

$$\text{Using } \int_{-\infty}^{\infty} \left[\frac{\sin Z}{Z} \right]^2 dz = \pi$$

$$\therefore U_0 \approx \frac{\pi}{Nkd} \rightarrow D_0 = \frac{U_{\max}}{U_0} = \frac{Nkd}{\pi}$$

$$\text{or } D_0 = 2N \frac{d}{\lambda}$$

For a linear array with equal element spacing

$$L = (N-1)d$$

$$\therefore D_0 = 2N \frac{d}{\lambda} = 2 \left(1 + \frac{L}{d}\right) \frac{d}{\lambda}$$

$$\text{if } L \gg d \quad \therefore D_0 \approx \underline{\underline{2 \frac{L}{\lambda}}}$$

2. End-fire uniform array:

$$\psi = \frac{1}{2} kd (\cos \theta - 1)$$

$$(AF)_n = \frac{\sin \left[\frac{N}{2} kd (\cos \theta - 1) \right]}{\left[\frac{N}{2} kd (\cos \theta - 1) \right]}$$

$$\therefore U(\theta) = [(AF)_n]^2 = \left[\frac{\sin Z}{Z} \right]^2$$

$$\text{where } Z = \frac{N}{2} kd (\cos \theta - 1)$$

(12)

$$U_0 = \frac{1}{4\pi} \int_0^{2\pi} \int_0^\pi \left[\frac{\sin Z}{Z} \right]^2 \sin \theta d\theta d\phi$$

$$= \frac{1}{2} \int_0^\pi \left[\frac{\sin \left(\frac{N}{2} kd (\cos \theta - 1) \right)}{\frac{N}{2} kd (\cos \theta - 1)} \right]^2 \sin \theta d\theta$$

$$Z = \frac{N}{2} kd (\cos \theta - 1)$$

$$dZ = -\frac{N}{2} kd \sin \theta d\theta$$

$$\therefore U_0 = -\frac{1}{Nkd} \int_0^{-Nkd} \left[\frac{\sin Z}{Z} \right]^2 dZ = \frac{1}{Nkd} \int_0^{Nkd} \left[\frac{\sin Z}{Z} \right]^2 dZ$$

Using the condition of large array:

$$\therefore U_0 \approx \frac{1}{Nkd} \int_0^\infty \left[\frac{\sin Z}{Z} \right]^2 dZ = \frac{\pi}{2Nkd}$$

$$\therefore D_0 = \frac{U_{\max}}{U_0} = \frac{2Nkd}{\pi} = 4N \frac{d}{\lambda}$$

using $L = (N-1)d$

$$\therefore D_0 = 4 \left(1 + \frac{L}{d} \right) \frac{d}{\lambda}$$

$$\text{or for } L \gg d \quad D_0 \approx 4 \frac{L}{\lambda}$$

$\therefore D_0$ for G.F. array = Twice D_0 for B.S. array.