

EE 205 Dr. A. Zidouri

Electric Circuits II

Two-Port Circuits
Hybrid and Transmission Parameters

Lecture #43

EE 205 Dr. A. Zidouri

The material to be covered in this lecture is as follows:

- The Two-Port Hybrid parameters
- The Two-Port Transmission parameters
- Relationships Among the Two-Port Parameters
- Reciprocal Two-Port Circuits

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After finishing this lecture you should be able to:

- Determine the Two-Port Hybrid Parameters
- Determine the Two-Port Transmission Parameters
- Derive all the Other Sets from a Known Set of Parameters
- Recognize Reciprocal and Symmetric Two-Port Circuits

Hybrid parameters

- ✚ The z and y parameters of a two-port network do not always exist.
- ✚ There is a need for developing another set of parameters.

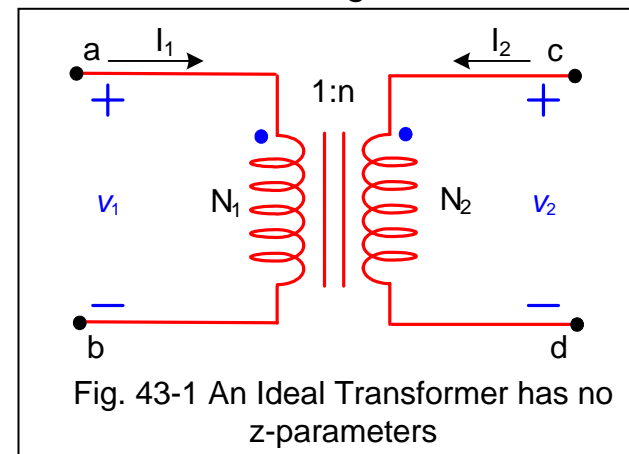
Hybrid Parameters (**h-parameters**):

$$\begin{aligned} V_1 &= h_{11}I_1 + h_{12}V_2 \\ I_2 &= h_{21}I_1 + h_{22}V_2 \end{aligned} \quad (43-1)$$

or in matrix form:

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix} = [h] \begin{bmatrix} I_1 \\ V_2 \end{bmatrix} \quad (43-2)$$

The h-parameters are very useful for describing electronic devices such as transistors. It is much easier to measure experimentally the h-parameters of such devices than to measure their **z** or **y** parameters. In fact an ideal transformer for example does not have **z**-parameters as it is impossible to express the voltages in terms of the currents or vice versa. See Fig. 43-1



$$\begin{aligned} V_1 &= \frac{1}{n}V_2 \\ I_1 &= -nI_2 \end{aligned}$$

The values of the parameters can be evaluated by setting $I_1=0$ (input port open-circuited) or $V_2=0$ (output port short-circuited). Thus,

$$h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0}, h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0}$$

$$h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0}, h_{22} = \left. \frac{I_2}{V_2} \right|_{I_1=0}$$

(43-3)

The parameters h_{11} , h_{12} , h_{21} , h_{22} represent an impedance, a voltage gain, a current gain, and an admittance respectively. This is why the h -parameters are called the hybrid parameters:

- h_{11} = short-circuit input impedance
- h_{12} = Open-circuit reverse voltage gain
- h_{21} = short-circuit forward current gain
- h_{22} = Open-circuit output admittance

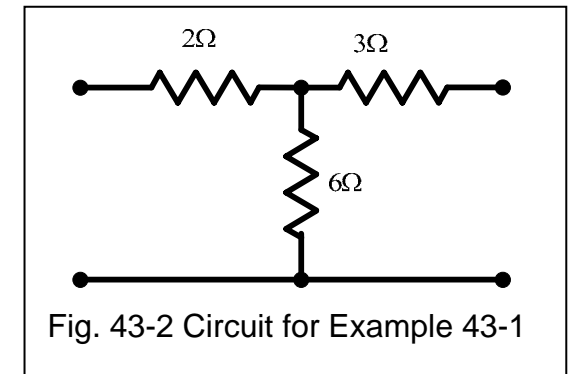
The following example illustrates the determination of the h -parameters for a resistive circuit.

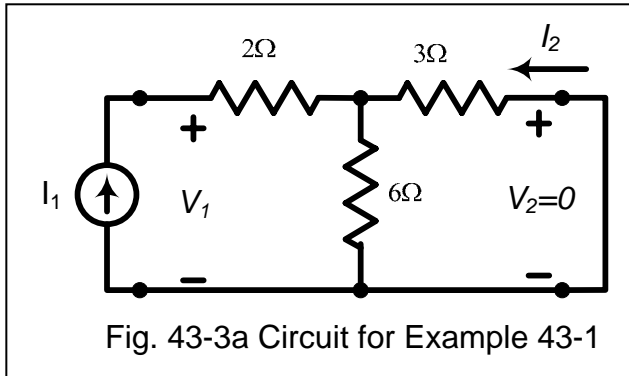
Example 43-1

Find the hybrid parameters for the two-port network of Fig. 43-2

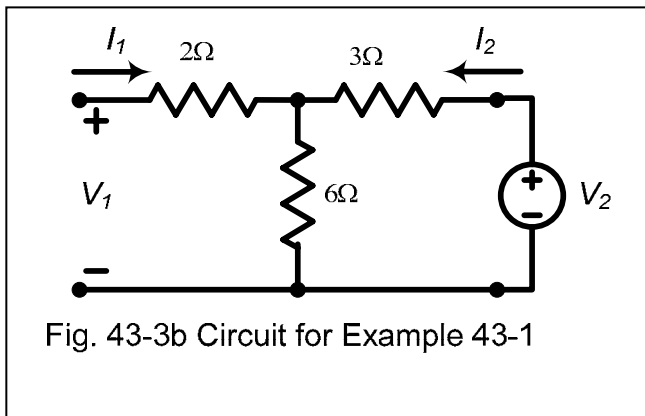
Solution:

To find h_{11} and h_{21} , we short circuit the output port and connect a current source I_1 to the input port as shown in Fig. 43-3a





$V_1 = I_1(2 + 3 \parallel 6) = 4I_1$ hence $h_{11} = \frac{V_1}{I_1} = 4\Omega$ and by
 current division, $-I_2 = \frac{6}{6+3}I_1 = \frac{2}{3}I_1$ hence $h_{21} = \frac{I_2}{I_1} = -\frac{2}{3}$



To find h_{12} and h_{22} , we open circuit the input port and connect a voltage source I_2 to the input port as shown in Fig. 43-3b. By voltage division

$V_1 = \frac{6}{6+3}V_2 = \frac{2}{3}V_2$ hence $h_{12} = \frac{V_1}{V_2} = \frac{2}{3}$ and,
 $V_2 = I_2(6+3) = 9I_2$ hence $h_{22} = \frac{I_2}{V_2} = \frac{1}{9}S$

Hybrid Parameters (**g-parameters**):

$$\begin{aligned} I_1 &= g_{11}V_1 + g_{12}I_2 \\ V_2 &= g_{21}V_1 + g_{22}I_2 \end{aligned} \quad (43-4)$$

or in matrix form:

$$\begin{bmatrix} I_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = [g] \begin{bmatrix} V_1 \\ I_2 \end{bmatrix} \quad (43-5)$$

The values of the **g-parameters** can be evaluated by setting $V_1=0$ (input port short-circuited) or $I_2=0$ (output port open-circuited). Thus,

$$\begin{aligned} g_{11} &= \left. \frac{I_1}{V_1} \right|_{I_2=0}, & g_{12} &= \left. \frac{I_1}{I_2} \right|_{V_1=0} \\ g_{21} &= \left. \frac{V_2}{V_1} \right|_{I_2=0}, & g_{22} &= \left. \frac{V_2}{I_2} \right|_{V_1=0} \end{aligned} \quad (43-6)$$

The g-parameters or inverse hybrid parameters are:

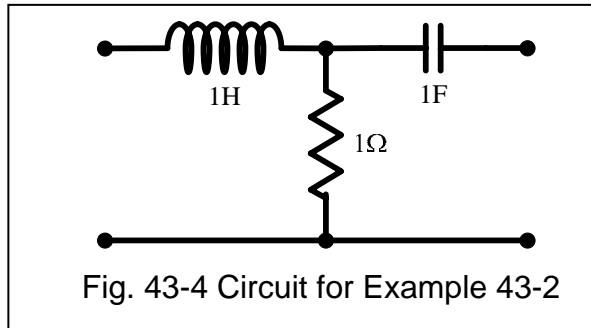
- g_{11} = Open-circuit input admittance
- g_{12} = Short-circuit reverse current gain
- g_{21} = Open-circuit forward voltage gain
- g_{22} = Short-circuit output impedance

The following example illustrates the determination of the g-parameters.

Example 43-2

Find the g parameters as a function of s for the circuit of Fig. 43-4

Solution:



In the s domain, we have $1H \Rightarrow sL = s$, $1F \Rightarrow \frac{1}{sC} = \frac{1}{s}$

To get g_{11} and g_{21} , we open circuit the output port and connect a voltage source V_1 to the input port as shown in Fig. 43-4a

$$I_1 = \frac{V_1}{s+1} \text{ or } g_{11} = \frac{I_1}{V_1} = \frac{1}{s+1}$$

By voltage division, $V_2 = \frac{1}{s+1}V_1$ or $g_{21} = \frac{V_2}{V_1} = \frac{1}{s+1}$

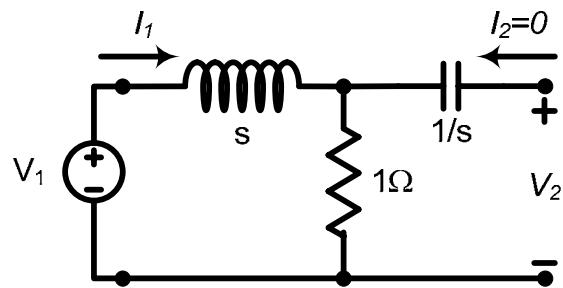


Fig. 43-4a Circuit for Example 43-2

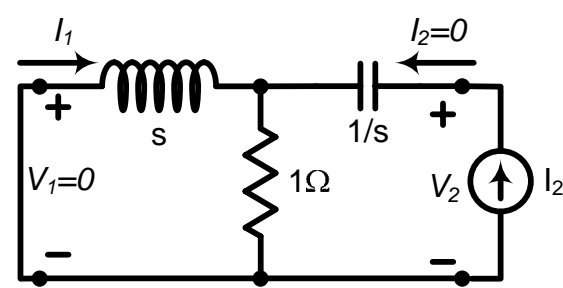


Fig. 43-4b Circuit for Example 43-2

To get g_{12} and g_{22} , we short circuit the input port and connect a current source I_2 to the output port as shown in Fig. 43-4b.

$$\text{By current division, } I_1 = -\frac{1}{s+1}I_2 \text{ or } g_{12} = \frac{I_1}{I_2} = -\frac{1}{s+1}$$

$$\text{Also, } V_2 = I_2 \left(\frac{1}{s} + s \parallel 1 \right) \text{ or } g_{22} = \frac{V_2}{I_2} = \frac{1}{s} + \frac{s}{s+1} = \frac{s^2 + s + 1}{s(s+1)}$$

$$\text{Thus, } [g] = \begin{bmatrix} \frac{1}{s+1} & -\frac{1}{s+1} \\ \frac{1}{s+1} & \frac{s^2 + s + 1}{s(s+1)} \end{bmatrix}$$

Transmission parameters

As we have seen in Eqs. (42-5) and (42-6) that we reproduce here for convenience:

$$\text{Transmission Parameters (a-parameters):} \quad \begin{aligned} V_1 &= a_{11}V_2 - a_{12}I_2 \\ I_1 &= a_{21}V_2 - a_{22}I_2 \end{aligned} \quad (43-7)$$

$$\text{Inverse Transmission Parameters (b-parameters):} \quad \begin{aligned} V_2 &= b_{11}V_1 - b_{12}I_1 \\ I_2 &= b_{21}V_1 - b_{22}I_1 \end{aligned} \quad (43-8)$$

where we express the input variables in terms of the output variables or the output variables in terms of the input variables.

In matrix form:

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix} = [T] \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix} \quad (43-9)$$

$$\begin{bmatrix} V_2 \\ I_2 \end{bmatrix} = \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ -I_1 \end{bmatrix} = [t] \begin{bmatrix} V_1 \\ -I_1 \end{bmatrix} \quad (43-10)$$

Where

$$a_{11} = \left. \frac{V_1}{V_2} \right|_{I_2=0}, a_{12} = - \left. \frac{V_1}{I_2} \right|_{V_2=0} \quad (43-11)$$

$$a_{21} = \left. \frac{I_1}{V_2} \right|_{I_2=0}, a_{22} = - \left. \frac{I_1}{I_2} \right|_{V_2=0}$$

$$b_{11} = \left. \frac{V_2}{V_1} \right|_{I_1=0}, b_{12} = - \left. \frac{V_2}{I_1} \right|_{V_1=0} \quad (43-12)$$

$$b_{21} = \left. \frac{I_2}{V_1} \right|_{I_1=0}, b_{22} = - \left. \frac{I_2}{I_1} \right|_{V_1=0}$$

The **a**-parameters represent:

- a_{11} = Open-circuit reverse voltage ratio
- a_{12} = Negative short-circuit transfer impedance
- a_{21} = Open circuit transfer admittance
- a_{22} = Negative short-circuit reverse current ratio

The **b**-parameters or inverse hybrid parameters are:

- b_{11} = Open-circuit voltage gain
- b_{12} = Negative short-circuit transfer impedance
- b_{21} = Open circuit transfer admittance
- b_{22} = Negative short-circuit current gain

- ✚ These parameters are useful in the analysis of transmission lines (such as cable and fiber) because they express sending-end variables in terms of receiving-end variables.
- ✚ They are also called **ABCD** parameters (for **a**) and **abcd** parameters (for **b**).
- ✚ They are used in the design of telephone systems, microwave networks, and radars.

Relationships among the Two-Port Parameters

- ✚ If we know one set of parameters we can derive all the other sets from the known set
- ✚ Table 43-1 shows the Parameter Conversion Table
- ✚ Let's derive the relationship between **z** and **y** and between **z** and **a** as an example.

To derive the relationship between **z** and **y** we first solve Eqs. (42-2)
$$\begin{aligned} I_1 &= y_{11}V_1 + y_{12}V_2 \\ I_2 &= y_{21}V_1 + y_{22}V_2 \end{aligned}$$
 for V_1 and V_2 .

Then compare the coefficients of I_1 and I_2 in the resulting expressions to the coefficients of I_1 and I_2 in

Eqs. (42-1)
$$\begin{aligned} V_1 &= z_{11}I_1 + z_{12}I_2 \\ V_2 &= z_{21}I_1 + z_{22}I_2 \end{aligned}$$
 . From Eqs. (42-2) we have:

$$V_1 = \frac{\begin{vmatrix} I_1 & y_{12} \\ I_2 & y_{22} \end{vmatrix}}{\begin{vmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{vmatrix}} = \frac{y_{22}}{\Delta y} I_1 - \frac{y_{12}}{\Delta y} I_2 \quad (43-13)$$

$$V_2 = \frac{\begin{vmatrix} y_{11} & I_1 \\ y_{21} & I_2 \end{vmatrix}}{\begin{vmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{vmatrix}} = \frac{y_{21}}{\Delta y} I_1 - \frac{y_{11}}{\Delta y} I_2 \quad (43-14)$$

comparing (43-13) and (43-14) with (42-1) shows:

$$z_{11} = \frac{y_{22}}{\Delta y} \quad (43-15)$$

$$z_{12} = -\frac{y_{12}}{\Delta y} \quad (43-16)$$

$$z_{21} = -\frac{y_{21}}{\Delta y} \quad (43-17)$$

$$z_{22} = \frac{y_{11}}{\Delta y} \quad (43-18)$$

To find \mathbf{z} -parameters as a function of the \mathbf{a} -parameters, we rearrange Eqs. (43-7) in the form of Eqs. (42-1) and then compare the coefficients. From the second equation in (42-5):

$$V_2 = \frac{1}{a_{21}} I_1 + \frac{a_{22}}{a_{21}} I_2 \quad (43-19)$$

therefore, substituting Eq. (43-19) into the first equation of Eqs. (42-5) yields

$$V_1 = \frac{a_{11}}{a_{21}} I_1 + \left(\frac{a_{11}a_{22}}{a_{21}} - a_{12} \right) I_2 \quad (43-20)$$

From Eq. (43-20) $z_{11} = \frac{a_{11}}{a_{21}} \quad (43-21)$ $z_{12} = \frac{\Delta a}{a_{21}} \quad (43-22)$

From Eq. (43-19) $z_{21} = \frac{1}{a_{21}} \quad (43-23)$ $z_{22} = \frac{a_{22}}{a_{21}} \quad (43-24)$

Example 43-3

Two sets of measurements are made on a two-port resistive circuit. The first set is made with port 2 open, and the second set is made with port 2 short-circuited. The results are as follows:

Port 2 Open

$$V_1 = 10mV$$

$$I_1 = 10\mu A$$

$$V_2 = -40V$$

Port 2 Short Circuited

$$V_1 = 24mV$$

$$I_1 = 20\mu A$$

$$I_2 = 1mA$$

Find the **h** parameters of the circuit.

Solution:

From the short circuit test: $h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0} = \frac{24 \times 10^{-3}}{20 \times 10^{-6}} = 1.2k\Omega$ and $h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0} = \frac{10^{-3}}{20 \times 10^{-6}} = 50$

h_{12} and h_{22} cannot be obtained directly from the open circuit test. However we can obtain them from **a**-parameters either from a conversion table or through a similar procedure as seen in previous slides in

this lecture. We get $h_{12} = \frac{\Delta a}{a_{22}}$, $h_{22} = \frac{a_{21}}{a_{22}}$ The a-parameters are

$$a_{11} = \left. \frac{V_1}{V_2} \right|_{I_2=0} = \frac{10 \times 10^{-3}}{-40} = -0.25 \times 10^{-3}$$

$$a_{21} = \left. \frac{I_1}{V_2} \right|_{I_2=0} = \frac{10 \times 10^{-6}}{-40} = -0.25 \times 10^{-6} \text{ S}$$

$$a_{12} = - \left. \frac{V_1}{I_2} \right|_{V_2=0} = - \frac{24 \times 10^{-3}}{10^{-3}} = -24 \Omega$$

$$a_{22} = - \left. \frac{I_1}{I_2} \right|_{V_2=0} = - \frac{20 \times 10^{-6}}{10^{-3}} = -20 \times 10^{-3} \text{ which give } \Delta a = a_{11} a_{22} - a_{12} a_{21} = 5 \times 10^{-6} - 6 \times 10^{-6} = -10^{-6}$$

$$\text{Therefore } h_{12} = \frac{\Delta a}{a_{22}} = \frac{-10^{-6}}{-20 \times 10^{-3}} = 5 \times 10^{-5} \text{ and } h_{22} = \frac{a_{21}}{a_{22}} = \frac{-0.25 \times 10^{-6}}{-20 \times 10^{-3}} = 12.5 \mu\text{S}$$

Reciprocal Two-Port Circuits

If a two-port circuit is **reciprocal** the following relationships exist among the port parameters:

$$z_{12} = z_{21} \quad (43-23)$$

$$y_{12} = y_{21} \quad (43-24)$$

$$a_{11} a_{22} - a_{12} a_{21} = \Delta a = 1 \quad (43-25)$$

$$b_{11} b_{22} - b_{12} b_{21} = \Delta b = 1 \quad (43-26)$$

$$h_{12} = -h_{21} \quad (43-27)$$

$$g_{12} = -g_{21} \quad (43-28)$$

A two-port circuit is **reciprocal** if the interchange of an ideal voltage source at one port with an ideal ammeter at the other port produces the same ammeter reading.

Example 43-4

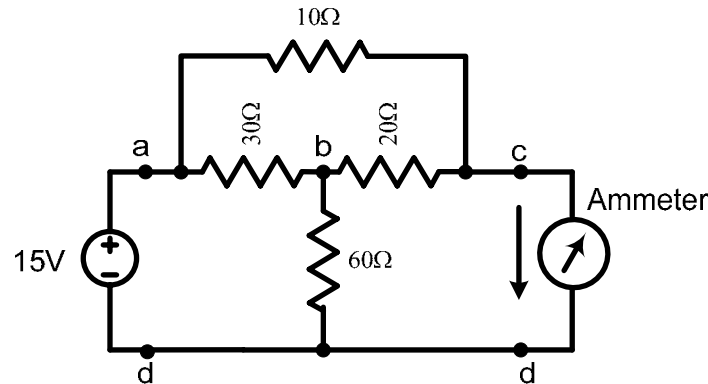


Fig. 42-4 A Reciprocal two-port Circuit

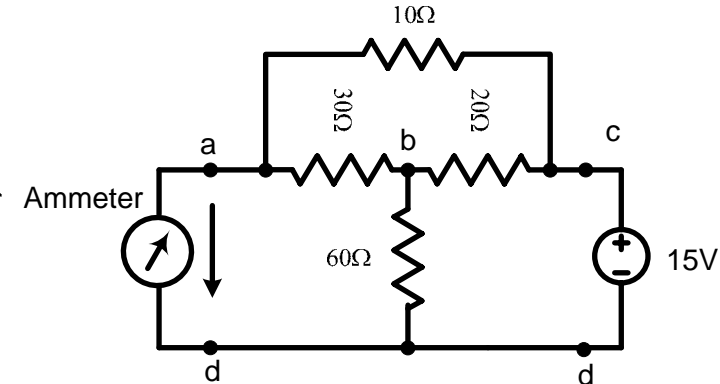


Fig. 42-5 The Circuit in Fig. 42-4 with the Voltage and Ammeter Interchanged

Consider the circuit of Fig. 43-5. When a voltage source of 15 V is applied to port ad, it produces a current of 1.75 A in the ammeter at port cd.

The ammeter current can be determined easily from V_{bd}

$$\frac{V_{bd}}{60} + \frac{V_{bd} - 15}{30} + \frac{V_{bd}}{20} = 0 \quad (43-29) \text{ and } V_{bd} = 5V \text{ therefore } I = \frac{5}{20} + \frac{15}{10} = 1.75A \quad (43-30)$$

If the voltage source and ammeter are interchanged the ammeter will still read 1.75 A. We verify this by solving the circuit of Fig. 43-6:

$$\frac{V_{bd}}{60} + \frac{V_{bd}}{30} + \frac{V_{bd} - 15}{20} = 0 \quad (43-31) \text{ therefore } V_{bd} = 7.5V \text{ the current } I_{ad} \text{ is}$$

$$I_{ad} = \frac{7.5}{30} + \frac{15}{10} = 1.75A \quad (43-32)$$

A reciprocal circuit is also symmetric, if its port can be interchanged without disturbing the values of the terminal currents and voltages. The following additional relationships will hold:

$$z_{11} = z_{22} \quad (43-33)$$

$$y_{11} = y_{22} \quad (43-34)$$

$$h_{11}h_{22} - h_{12}h_{21} = \Delta h = 1 \quad (43-35)$$

$$g_{11}g_{22} - g_{12}g_{21} = \Delta g = 1 \quad (43-36)$$

For a symmetric reciprocal circuit only two calculations or measurements are necessary to determine all the two-port parameters.

Self Test 43:

Two sets of measurements are made on a two-port network that is symmetric and reciprocal. The first set is made with port 2 open, and the second set is made with port 2 short-circuited as follows:

Port 2 Open

$$V_1 = 95V$$

$$I_1 = 5A$$

Port 2 Short Circuited

$$V_1 = 11.52V$$

$$I_2 = -2.72A$$

Calculate the z parameters of the two-port network.

Answer:

$$z_{11} = z_{22} = 19\Omega \quad z_{12} = z_{21} = 17\Omega$$