

# EE 380

## SOLUTION HW 3

**E3.5** From the block diagram we determine that the state equations are

$$\begin{aligned}\dot{x}_2 &= -(fk + d)x_1 + ax_1 + fu \\ \dot{x}_1 &= -kx_2 + u\end{aligned}$$

and the output equation is

$$y = bx_2 .$$

Therefore,

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}u \\ y &= \mathbf{C}\mathbf{x} + \mathbf{D}u ,\end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & -k \\ a & -(fk + d) \end{bmatrix} , \quad \mathbf{B} = \begin{bmatrix} 1 \\ f \end{bmatrix} , \quad \mathbf{C} = [ 0 \quad b ] \text{ and } \mathbf{D} = [0] .$$

**E3.7** The state equations are

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= -100x_1 - 20x_2 + u\end{aligned}$$

or, in matrix form

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ -100 & -20 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u .$$

So, the characteristic equation is determined to be

$$\det(\lambda\mathbf{I} - \mathbf{A}) = \det \begin{bmatrix} \lambda & -1 \\ 100 & \lambda + 20 \end{bmatrix} = \lambda^2 + 20\lambda + 100 = (\lambda + 10)^2 = 0 .$$

Thus, the roots of the characteristic equation are

$$\lambda_1 = \lambda_2 = -10 .$$

**E3.8** The characteristic equation is

$$\det(\lambda \mathbf{I} - \mathbf{A}) = \det \begin{bmatrix} \lambda & -1 & 0 \\ 0 & \lambda & -1 \\ 0 & 5 & \lambda + 2 \end{bmatrix} = \lambda(\lambda^2 + 2\lambda + 5) = 0 .$$

Thus, the roots of the characteristic equation are

$$\lambda_1 = 0 , \quad \lambda_2 = -1 + j2 \text{ and } \lambda_3 = -1 - j2 .$$

**E3.11** A state variable representation is

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}r \\ y &= \mathbf{C}\mathbf{x} \end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -12 & -8 \end{bmatrix} , \quad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} , \quad \mathbf{C} = [ 12 \quad 4 ] .$$

**E3.15** The equations of motion are

$$\begin{aligned} m\ddot{x} + kx + k_1(x - q) + b\dot{x} &= 0 \\ m\ddot{q} + kq + b\dot{q} + k_1(q - x) &= 0 . \end{aligned}$$

In state variable form we have

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{(k+k_1)}{m} & -\frac{b}{m} & \frac{k_1}{m} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{k_1}{m} & 0 & -\frac{(k+k_1)}{m} & -\frac{b}{m} \end{bmatrix} \mathbf{x}$$

where  $x_1 = x$ ,  $x_2 = \dot{x}$ ,  $x_3 = q$  and  $x_4 = \dot{q}$ .

**E3.19** First, compute the matrix

$$sI - \mathbf{A} = \begin{bmatrix} s & -1 \\ 3 & s+4 \end{bmatrix}.$$

Then,  $\Phi(s)$  is

$$\Phi(s) = (s\mathbf{I} - \mathbf{A})^{-1} = \frac{1}{\Delta(s)} \begin{bmatrix} s+4 & 1 \\ -3 & s \end{bmatrix}$$

where  $\Delta(s) = s^2 + 4s + 3$ , and

$$G(s) = \begin{bmatrix} 10 & 0 \end{bmatrix} \begin{bmatrix} \frac{s+4}{\Delta(s)} & \frac{1}{\Delta(s)} \\ -\frac{3}{\Delta(s)} & \frac{s}{\Delta(s)} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \frac{10}{s^2 + 4s + 3}.$$

**P3.5** (a) The closed-loop transfer function is

$$T(s) = \frac{s+1}{s^3 + 5s^2 - 5s + 1}.$$

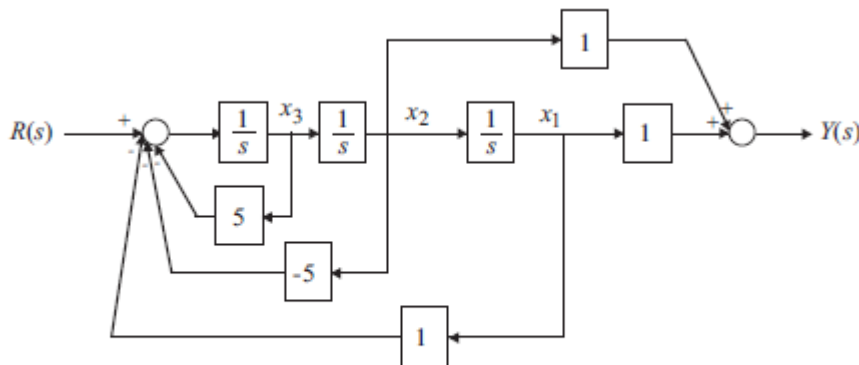
(b) A matrix differential equation is

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}u \\ y &= \mathbf{C}\mathbf{x} \end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & 5 & -5 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, \quad \mathbf{C} = \begin{bmatrix} 1 & 1 & 0 \end{bmatrix}.$$

The block diagram is shown in Figure P3.5.



**FIGURE P3.5**  
Block diagram model.

**P3.10** (a) From the signal flow diagram, we determine that a state-space model is given by

$$\dot{\mathbf{x}} = \begin{bmatrix} -K_1 & K_2 \\ -K_1 & -K_2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} K_1 & -K_2 \\ K_1 & K_2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix}$$

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \mathbf{x}.$$

(b) The characteristic equation is

$$\det[s\mathbf{I} - \mathbf{A}] = s^2 + (K_2 + K_1)s + 2K_1K_2 = 0.$$

(c) When  $K_1 = K_2 = 1$ , then

$$\mathbf{A} = \begin{bmatrix} -1 & 1 \\ -1 & -1 \end{bmatrix}.$$

The state transition matrix associated with  $\mathbf{A}$  is

$$\Phi = \mathcal{L}^{-1}\{[s\mathbf{I} - \mathbf{A}]^{-1}\} = e^{-t} \begin{bmatrix} \cos t & \sin t \\ -\sin t & \cos t \end{bmatrix}.$$

**P3.12** (a) The phase variable representation is

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -48 & -44 & -12 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r$$

$$y = [40 \ 8 \ 0]\mathbf{x}.$$

(b) The canonical representation is

$$\dot{\mathbf{z}} = \begin{bmatrix} -2 & 0 & 0 \\ 0 & -4 & 0 \\ 0 & 0 & -6 \end{bmatrix} \mathbf{z} + \begin{bmatrix} -0.5728 \\ 4.1307 \\ 4.5638 \end{bmatrix} r$$

$$y = [-5.2372 \ -0.4842 \ -0.2191]\mathbf{z}$$

(c) The state transition matrix is

$$\Phi(t) = \begin{bmatrix} \Phi_1(t) & \Phi_2(t) & \Phi_3(t) \end{bmatrix},$$

where

$$\Phi_1(t) = \begin{bmatrix} e^{-6t} - 3e^{-4t} + 3e^{-2t} \\ -6e^{-6t} + 12e^{-4t} - 6e^{-2t} \\ 36e^{-6t} - 48e^{-4t} + 12e^{-2t} \end{bmatrix} \quad \Phi_2(t) = \begin{bmatrix} \frac{3}{4}e^{-6t} - 2e^{-4t} + \frac{5}{4}e^{-2t} \\ -\frac{9}{2}e^{-6t} + 8e^{-4t} - \frac{5}{2}e^{-2t} \\ 27e^{-6t} - 32e^{-4t} + 5e^{-2t} \end{bmatrix}$$

$$\Phi_3(t) = \begin{bmatrix} \frac{1}{8}e^{-6t} - \frac{1}{4}e^{-4t} + \frac{1}{8}e^{-2t} \\ -\frac{3}{4}e^{-6t} + e^{-4t} - \frac{1}{4}e^{-2t} \\ \frac{9}{2}e^{-6t} - 4e^{-4t} + \frac{1}{2}e^{-2t} \end{bmatrix}.$$

**P3.19** Define the state variables as

$$\begin{aligned}x_1 &= \phi_1 - \phi_2 \\x_2 &= \frac{\omega_1}{\omega_o} \\x_3 &= \frac{\omega_2}{\omega_o} .\end{aligned}$$

Then, the state equations of the robot are

$$\begin{aligned}\dot{x}_1 &= \omega_o x_2 - \omega_o x_3 \\ \dot{x}_2 &= \frac{-J_2 \omega_o}{J_1 + J_2} x_1 - \frac{b}{J_1} x_2 + \frac{b}{J_1} x_3 + \frac{K_m}{J_1 \omega_o} i \\ \dot{x}_3 &= \frac{J_1 \omega_o}{J_1 + J_2} x_2 + \frac{b}{J_2} x_2 - \frac{b}{J_2} x_3\end{aligned}$$

or, in matrix form

$$\dot{\mathbf{x}} = \omega_o \begin{bmatrix} 0 & 1 & -1 \\ a - 1 & -b_1 & b_1 \\ a & b_2 & -b_2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ d \\ 0 \end{bmatrix} i$$

where

$$a = \frac{J_1}{(J_1 + J_2)} , \quad b_1 = \frac{b}{J_1 \omega_o} , \quad b_2 = \frac{b}{J_2 \omega_o} \text{ and } d = \frac{K_m}{J_1 \omega_o} .$$

**P3.24** (a) The phase variable representation is

$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -30 & -31 & -10 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r \\ y &= [1 \ 0 \ 0] \mathbf{x} .\end{aligned}$$

(b) The input feedforward representation is

$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -10 & 1 & 0 \\ -31 & 0 & 1 \\ -30 & 0 & 0 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r \\ y &= [1 \ 0 \ 0] \mathbf{x} .\end{aligned}$$

(c) The physical variable representation is

$$\dot{\mathbf{x}} = \begin{bmatrix} -3 & 1 & 0 \\ 0 & -2 & 1 \\ 0 & 0 & -5 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r$$

$$y = [1 \ 0 \ 0] \mathbf{x} .$$

(d) The decoupled representation is

$$\dot{\mathbf{x}} = \begin{bmatrix} -3 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -5 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} r$$

$$y = \left[ \frac{1}{6} \ \frac{1}{3} \ -\frac{1}{2} \right] \mathbf{x} .$$

**DP3.2** The desired transfer function is

$$\frac{Y(s)}{U(s)} = \frac{10}{s^2 + 4s + 3} .$$

The transfer function derived from the phase variable representation is

$$\frac{Y(s)}{U(s)} = \frac{d}{s^2 + bs + a} .$$

Therefore, we select  $d = 10$ ,  $a = 3$  and  $b = 4$ .

**CP3.2** The m-file script to compute the transfer function models using the `tf` function is shown in Figure CP3.2.

Transfer function: $\frac{6s - 48}{s^3 - 11s^2 + 4s - 36}$	←	<pre>% Part (b) A=[1 1 0;-2 0 4;6 2 10];B=[-1;0;1];C=[0 1 0];D=[0]; sys_ss=ss(A,B,C,D); sys_tf = tf(sys_ss)</pre>
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CP3.7 The m-file script and system response is shown in Figure CP3.7.

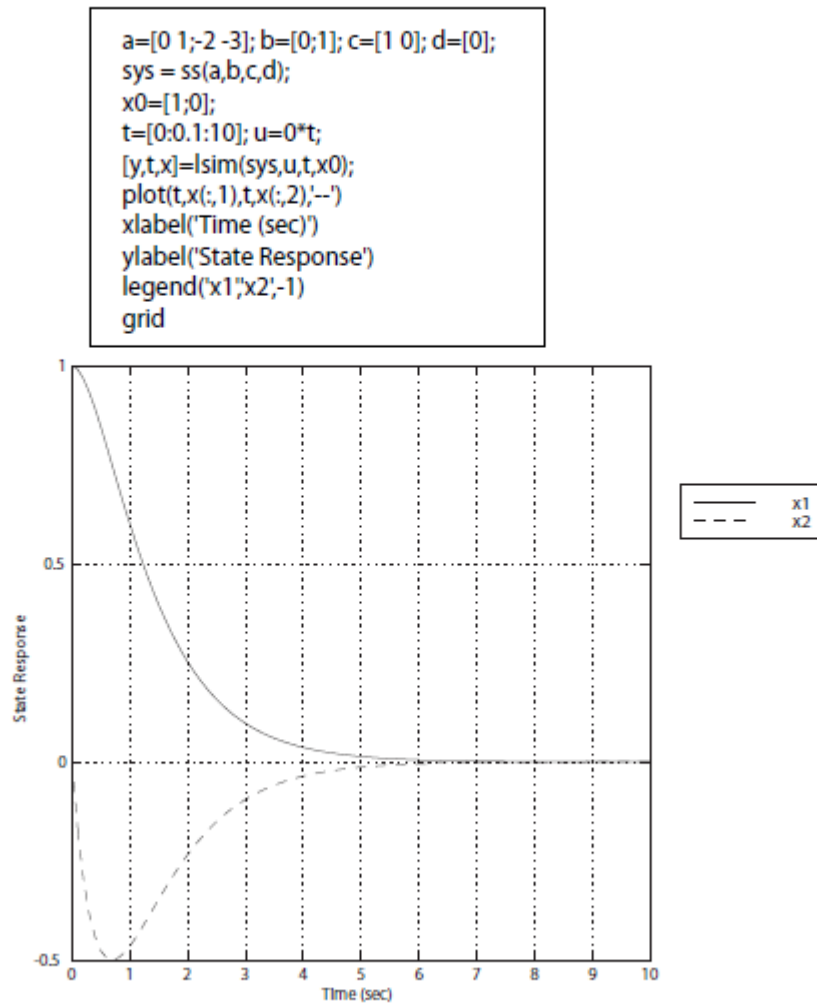


FIGURE CP3.7  
Using the lsim function to compute the zero input response.