

# EE 380 HW #3

E3.2 We know that the velocity is the derivative of the position, therefore we have

$$\frac{dy}{dt} = v,$$

and from the problem statement

$$\frac{dv}{dt} = -k_1 v(t) - k_2 y(t) + k_3 i(t).$$

This can be written in matrix form as

$$\frac{d}{dt} \begin{pmatrix} y \\ v \end{pmatrix} = \begin{bmatrix} 0 & 1 \\ -k_2 & -k_1 \end{bmatrix} \begin{pmatrix} y \\ v \end{pmatrix} + \begin{bmatrix} 0 \\ k_3 \end{bmatrix} i.$$

Define  $u = i$ , and let  $k_1 = k_2 = 1$ . Then,

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ k_3 \end{bmatrix}, \quad \text{and} \quad \mathbf{x} = \begin{pmatrix} y \\ v \end{pmatrix}.$$

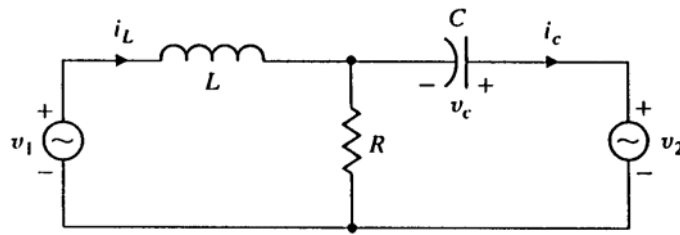


FIGURE P3.3 RLC circuit.

P3.3 The signal flow graph is shown in Figure P3.3. Using Kirchoff's voltage law

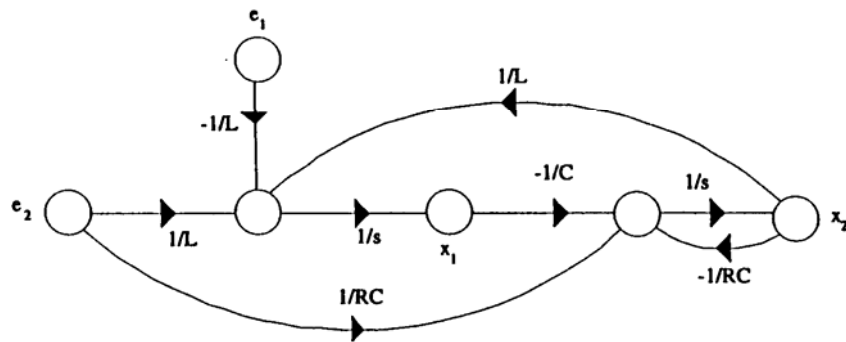


FIGURE P3.3  
Signal flow graph.

around the outer loop, we have

$$L \frac{di_L}{dt} - v_c + e_2 - e_1 = 0.$$

Then, using Kirchoff's current law at the node, we determine that

$$C \frac{dv_c}{dt} = -i_L + i_R,$$

where  $i_R$  is the current through the resistor  $R$ . Considering the right loop we have

$$i_R R - e_2 + v_c = 0 \quad \text{or} \quad i_R = -\frac{v_c}{R} + \frac{e_2}{R}.$$

Thus,

$$\frac{dv_c}{dt} = -\frac{v_c}{RC} - \frac{i_L}{C} + \frac{e_2}{RC} \quad \text{and} \quad \frac{di_L}{dt} = \frac{v_c}{L} + \frac{e_1}{L} - \frac{e_2}{L}.$$

In matrix form, the state equations are

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{bmatrix} 0 & 1/L \\ -1/C & -1/RC \end{bmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{bmatrix} 1/L & -1/L \\ 0 & 1/RC \end{bmatrix} \begin{bmatrix} e_1 \\ e_2 \end{bmatrix},$$

where  $x_1 = i_L$  and  $x_2 = v_c$ .

P3.5 (a) The closed-loop transfer function is

$$T(s) = \frac{s+1}{s^3 + 5s^2 - 5s + 1}$$

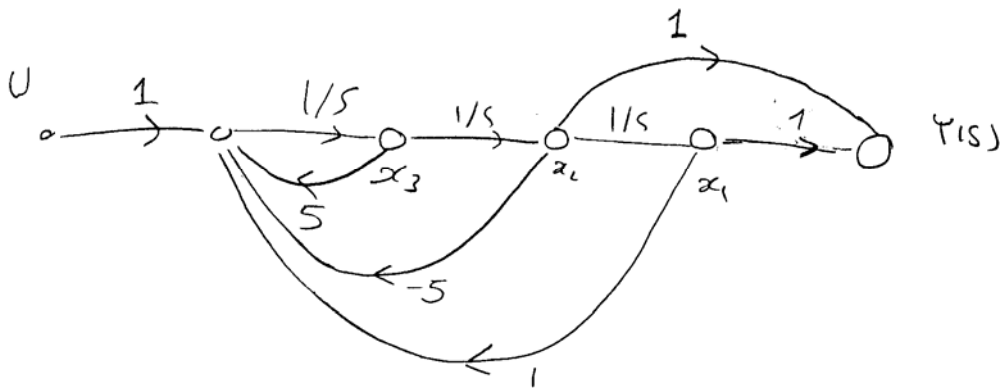
(b) The matrix differential equation in phase variable form is

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

$$y = \mathbf{C}\mathbf{x}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & 5 & -5 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, \quad \mathbf{C} = [1 \ 1 \ 0]$$



P3.25 The matrix representation of the state equations is

$$\dot{\mathbf{x}} = \begin{bmatrix} 3 & 0 \\ 0 & 2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} d$$

When  $u_1 = 0$  and  $u_2 = d = 1$ , we have

$$\dot{x}_1 = 3x_1 + u_2$$

$$\dot{x}_2 = 2x_2 + 2u_2$$

So we see that we have two independent equations for  $x_1$  and  $x_2$ . With  $U_2(s) = 1/s$  and zero initial conditions, the solution for  $x_1$  is found to be

$$\begin{aligned} x_1(t) &= \mathcal{L}^{-1}\{X_1(s)\} = \mathcal{L}^{-1}\left\{\frac{1}{s(s-3)}\right\} \\ &= \mathcal{L}^{-1}\left\{-\frac{1}{3s} + \frac{1}{3}\frac{1}{s-3}\right\} = -\frac{1}{3}(1 - e^{3t}) \end{aligned}$$

and the solution for  $x_2$  is

$$x_2(t) = \mathcal{L}^{-1}\{X_2(s)\} = \mathcal{L}^{-1}\left\{\frac{2}{s(s-2)}\right\} = \mathcal{L}^{-1}\left\{-\frac{1}{s} + \frac{1}{s-2}\right\} = -1 + e^{2t}$$

DP3.2 The desired transfer function is

$$\frac{Y(s)}{U(s)} = \frac{10}{s^2 + 4s + 3}$$

The transfer function derived from the phase variable representation is

$$\frac{Y(s)}{U(s)} = \frac{d}{s^2 + bs + a}$$

Therefore, we select  $d = 10$ ,  $a = 3$  and  $b = 4$ .

MP3.1 The MATLAB script to compute the state-space models using the `tf2ss` function is shown in Figure MP3.1.

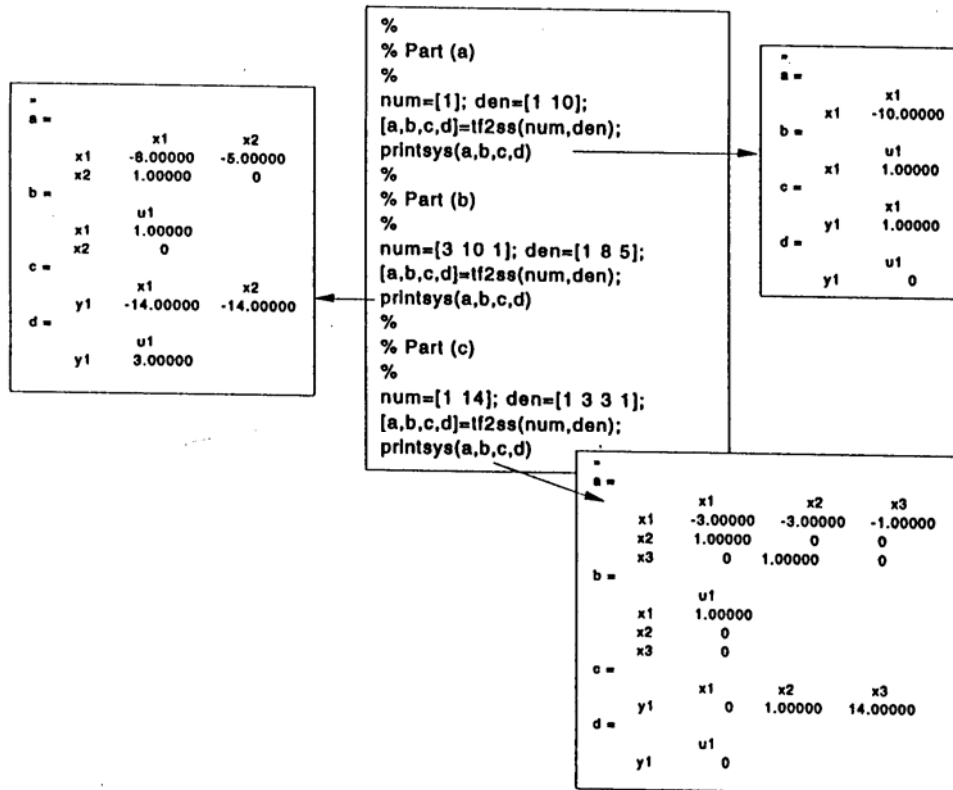


FIGURE MP3.1 Script to compute state-space models from transfer functions.

For example, in part (c) the state-space model is

$$\begin{aligned} \dot{\mathbf{x}} &= \mathbf{Ax} + \mathbf{Bu} \\ y &= \mathbf{Cx} + \mathbf{Du} \end{aligned}$$

where  $\mathbf{D} = [0]$  and

$$\mathbf{A} = \begin{bmatrix} -3 & -3 & -1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \quad \mathbf{C} = [0 \ 1 \ 14].$$

MP3.4 The MATLAB script and state history is shown in Figure MP3.4.

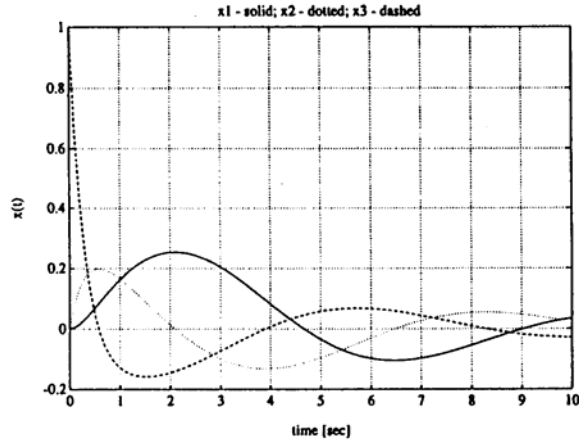


FIGURE MP3.4  
(a) The system step response.

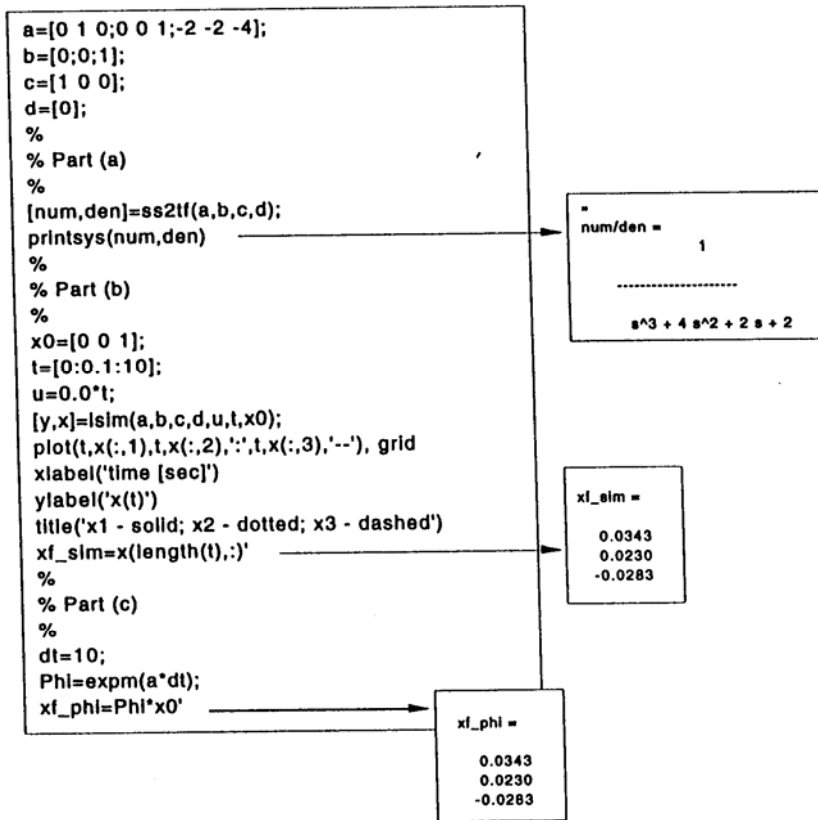


FIGURE MP3.4  
CONTINUED: (b) The MATLAB script using the `lsim` function.

The transfer function equivalent is

$$G(s) = \frac{1}{s^3 + 4s^2 + 2s + 2}$$

The computed state vector at  $t = 10$  is the same using the simulation and the state transition matrix.