

KING FAHD UNIVERSITY OF PETROLEUM AND MINERALS

ELECTRICAL ENGINEERING DEPARTMENT

SECOND SEMESTER 2008/2009

EE 340 (03) FINAL EXAM

LOCATION: 59-1001

TIME: 7:300 -10:00 A.M.

DATE: THURSDAY 4-FEBRUARY-2010

Student's Name:.....

Student's I.D. Number: .....

Section Number: .....

	Maximum Score	Score
<b>Problem 1</b>	<b>20</b>	
<b>Problem 2</b>	<b>20</b>	
<b>Problem 3</b>	<b>20</b>	
<b>Problem 4</b>	<b>20</b>	
<b>Problem 5</b>	<b>20</b>	
<b>Total</b>	<b>100</b>	

Problem 1 [20 points]

Answer the following multiple choice problems:

a) Consider a uniform plane electromagnetic wave which propagates in a lossy medium. The electric field amplitude of the wave is found to drop from 3V/m to 0.5V/m within a distance of 15m along the wave direction of propagation. Using the given information, it can be concluded that the depth of penetration equals:

- 1) 15.00m      2) 0.119m      3) 4.10m      4) 8.37m      5) 2.18m      6) 2.50m

b) Consider two semi-infinite media, which are separated by the  $xz$  plane. Medium 1 ( $y > 0$ ) has a relative permeability of 3 and medium 2 ( $y < 0$ ) has a relative permeability of 15. The magnetic field intensity vector in medium 1, at the boundary, is given by  $\vec{H}_1 = -2\vec{a}_x + 5\vec{a}_y + 11\vec{a}_z$  A/m. Now consider a square area of dimension  $2m \times 2m$  which lies entirely at the boundary between the two media (i.e. the  $xz$  plane). The boundary has no surface current. From the given information, it can be concluded that the magnetic flux (in  $Wb$ ) through the given area equals:

- 1)  $88\mu_o$       2)  $20\mu_o$       3)  $8\mu_o$       4)  $60\mu_o$       5)  $15\mu_o$       6)  $30\mu_o$

c) A conductor occupies the cylindrical volume ( $\rho < a$ ) while the outside volume ( $\rho > a$ ) is occupied by air. The electrostatic field  $\vec{E} = \frac{A}{\rho}\vec{a}_\rho$  V/m exists in the volume occupied by air, where A is some constant. Using the given information, it can be concluded that the surface charge density (in  $C/m^2$ ) on the conductor/air boundary is given by:

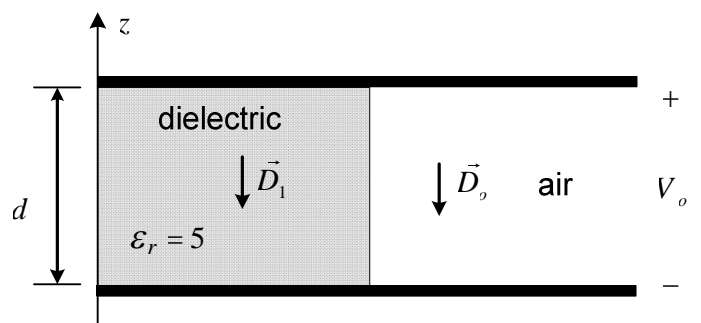
- 1)  $\frac{A}{a}\epsilon_o$       2)  $\frac{A}{\rho}$       3)  $-\frac{A}{a}\epsilon_o$       4)  $\frac{A}{\rho}\epsilon_o$       5)  $-\frac{A}{\rho}\epsilon_o$       6)  $\frac{A}{a}\epsilon_o\vec{a}_\rho$

d) Which one of the following expressions represents the 3D wave equation for the electric field in a source free region?

- 1)  $\nabla^2 \vec{E} = \mu\epsilon \vec{E}$       2)  $\nabla^2 \vec{E} = \mu\epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$       3)  $\nabla^2 \vec{E} = \frac{1}{\mu\epsilon} \frac{\partial^2 \vec{E}}{\partial t^2}$   
 4)  $\frac{\partial^2 \vec{E}}{\partial z^2} = \mu\epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$       5)  $\nabla^2 \vec{E} = \frac{\mu}{\epsilon} \frac{\partial^2 \vec{E}}{\partial t^2}$       6)  $\nabla^2 \vec{E} = \frac{\partial^2 \vec{E}}{\partial t^2}$

e) The figure shows a partially-filled parallel-plate capacitor with a plate separation  $d = 0.5cm$ . The relative permittivity of the dielectric filling is  $\epsilon_r = 5$ . The electric flux density vector in the dielectric region is given by:

$$\vec{D}_1 = -\vec{a}_z 0.707 \mu C / m^2$$



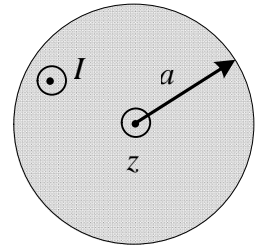
The resulting potential difference  $V_o$  across the capacitor equals:

- 1) 16V      2) 2000V      3) 60V      4) 30V      5) 80V      6) 400V

Problem 2 [20 Points]

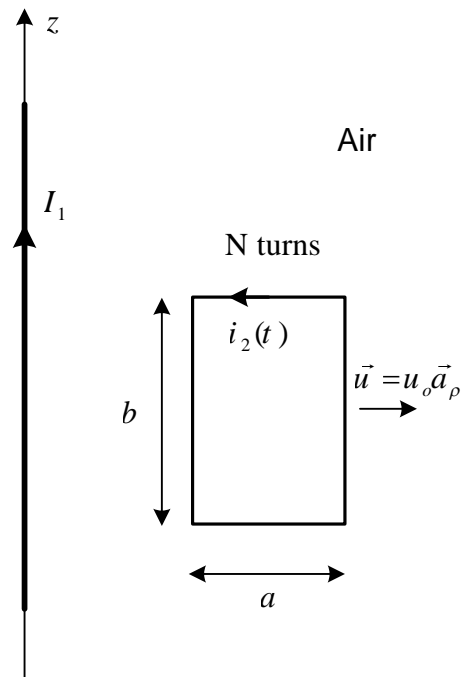
a) Consider the infinitely long cylindrical conductor shown in the figure. The conductor has radius  $a$  and it carries D.C. current  $I$  in the  $+z$  direction. The axis of the conductor coincides with the  $z$  axis. The conductor is made of a nonmagnetic material.

Derive an expression for the magnetostatic energy stored in 1m length of the conductor.



b) Consider the infinitely long straight filamentary conductor which is placed along the entire  $z$  - axis. The conductor carries DC current  $I_1$ . As shown in the figure, the coplanar N-turn closed rectangular circuit recedes from the straight conductor with the constant velocity  $\vec{u} = u_o \vec{a}_\rho$ . At  $t = 0$  the left hand side of the rectangular loop coincides with the straight conductor.

Assuming that the rectangular circuit has total resistance  $R$ , derive an expression (valid for  $t > 0$ ) for the induced current  $i_2(t)$ .



Problem 3 [20 Points]

a) A uniform plane EM propagates in a lossless nonmagnetic medium. The wavelength of the wave equals  $0.75\text{cm}$ . The magnetic flux density vector associated with the wave is given by:

$$\vec{B} = \vec{a}_z 20 \times 10^{-6} \cos(10^{11}t - \beta y) \text{ Wb/m}^2$$

Find an expression for the  $\vec{D}$  field associated with the wave. The required expression must not contain any unknown quantities.

b) The electric field of a 50MHz uniform plane EM wave propagating in a lossless medium is given by:

$$\vec{E}_s = \vec{a}_y (1 + j)e^{j2x} + \vec{a}_z \sqrt{2}e^{j2x - j\pi/4}$$

- 1) What is the direction of wave propagation?
- 2) Calculate the phase velocity.
- 3) What is the wave polarization?

Problem 4 [20 Points]

a) A uniform plane TEM wave propagates in a lossy nonmagnetic medium. The intrinsic impedance of the wave equals  $110e^{j37^\circ} \Omega$ . Calculate the phase velocity of the wave.

b) Consider a uniform EM wave propagating in free space. The wave has the following instantaneous Poynting's vector:

$$\vec{a}_y 20 \cos^2(1.5 \times 10^8 t - 0.5y) \text{ W / m}^2$$

Assuming the electric is linearly polarized in the  $x$  direction, find an expression for the magnetic field intensity vector of the wave.

Problem 5 [20 Points]

Consider two semi-infinite media. Medium 1 ( $x < 0$ ) is a *lossless nonmagnetic* dielectric and medium 2 ( $x > 0$ ) is air. A 5GHz uniform plane EM wave is normally incident from medium 1 onto medium 2. The incident and reflected electric fields are respectively given by:

$$\vec{E}_{is} = 30e^{-j\beta_1 x} \vec{a}_z \quad \text{V/m}$$

$$\vec{E}_{rs} = 10e^{j\beta_1 x} \vec{a}_z \quad \text{V/m}$$

Where the subscript  $s$  indicates the phasor form of the field. Find:

- a)  $\beta_1$
- b)  $\vec{E}_{ts}$
- c) An expression for the reflected instantaneous magnetic field  $\vec{H}_r$ .
- d) The numerical value of the reflected electric field  $\vec{E}_r$ ,  $5\text{cm}$  from the boundary at  $t = 1\mu\text{s}$ .

### Electrostatics:

$$\vec{E} = \sum_{i=1}^N \frac{Q_i \vec{R}_i}{4\pi\epsilon R_i^3} + \int_l \frac{\rho_L \vec{R}}{4\pi\epsilon R^3} + \int_s \frac{\rho_s \vec{R}}{4\pi\epsilon R^3} + \int_v \frac{\rho_v \vec{R}}{4\pi\epsilon R^3}, \quad V = \sum_{i=1}^N \frac{Q_i}{4\pi\epsilon R_i} + \int_l \frac{\rho_L}{4\pi\epsilon R} + \int_s \frac{\rho_s}{4\pi\epsilon R} + \int_v \frac{\rho_v}{4\pi\epsilon R}$$

$$\oint_s \vec{D} \cdot d\vec{s} = Q, \quad \oint_l \vec{E} \cdot d\vec{l} = 0, \quad \nabla \cdot \vec{D} = \rho_v, \quad \nabla \times \vec{E} = 0, \quad \vec{D} = \epsilon \vec{E}, \quad V_p = -\int_{\infty}^p \vec{E} \cdot d\vec{l},$$

$$V_{AB} = V_B - V_A = -\int_A^B \vec{E} \cdot d\vec{l}, \quad \vec{E} = -\nabla V, \quad w_e = \frac{1}{2} \epsilon E^2, \quad \vec{E} = \frac{\rho_L}{2\pi\epsilon\rho} \vec{a}_\rho, \quad \vec{E} = \frac{\rho_s}{2\epsilon} \vec{a}_N, \quad D_{1n} - D_{2n} = \rho_s,$$

$$E_{1t} = E_{2t}, \quad C = \frac{Q}{V_o}, \quad \nabla^2 V = -\frac{\rho_v}{\epsilon}$$

### Magnetostatics:

$$\oint_s \vec{B} \cdot d\vec{s} = 0, \quad \oint_l \vec{H} \cdot d\vec{l} = I, \quad \nabla \cdot \vec{B} = 0, \quad \nabla \times \vec{H} = \vec{J}, \quad \vec{B} = \mu \vec{H}, \quad \vec{B} = \nabla \times \vec{A}, \quad \vec{A} = \frac{I}{4\pi} \int_l \frac{d\vec{l} \times \vec{R}}{R}, \quad \nabla \cdot \vec{A} = 0,$$

$$\nabla^2 \vec{A} = -\mu \vec{J}, \quad \psi_m = \int_s \vec{B} \cdot d\vec{s} = \oint_l \vec{A} \cdot d\vec{l}, \quad M_{21} = \frac{\Lambda_{21}}{I_1} = \frac{N_2 \psi_{21}}{I_1}, \quad L = \frac{\Lambda}{I}, \quad d\vec{H} = \frac{I}{4\pi} \frac{d\vec{l} \times \vec{R}}{R^3},$$

$$w_m = \frac{1}{2} \mu H^2, \quad \vec{H} = \vec{a}_\phi \frac{I}{4\pi\rho} [\cos\alpha_2 - \cos\alpha_1], \quad \vec{H} = \vec{a}_\phi \frac{I}{2\pi\rho}, \quad \vec{F}_m = I \int_l d\vec{l} \times \vec{B}, \quad B_{1n} = B_{2n},$$

$$(\vec{H}_1 - \vec{H}_2) \times \vec{a}_{n12} = \vec{K}$$

$$\text{EMF: } emf = -\int_s \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} + \oint_l (\vec{u} \times \vec{B}) \cdot d\vec{l} = -\frac{d\psi_m}{dt}$$

### Maxwell's Equations (General Form):

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}, \quad \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}, \quad \nabla \cdot \vec{D} = \rho_v, \quad \nabla \cdot \vec{B} = 0$$

### Plane TEM Waves:

$$u_p = \frac{\omega}{\beta}, \quad u_s = \frac{d\omega}{d\beta}, \quad u_p = \frac{c}{\sqrt{\mu_r \epsilon_r}}, \quad \eta = \sqrt{\frac{\mu}{\epsilon}}, \quad \lambda = \frac{2\pi}{\beta}, \quad \eta = \frac{\sqrt{\mu/\epsilon}}{[1 + (\sigma/\omega\epsilon)^2]^{1/4}} \exp[j \frac{1}{2} \tan^{-1}(\sigma/\omega\epsilon)],$$

$$\gamma = \alpha + j\beta = j\omega\sqrt{\mu\epsilon(1 - j\sigma/\omega\epsilon)}, \quad \alpha = \omega\sqrt{\frac{\mu\epsilon}{2}[\sqrt{1 + (\sigma/\omega\epsilon)^2} - 1]}, \quad \beta = \omega\sqrt{\frac{\mu\epsilon}{2}[\sqrt{1 + (\sigma/\omega\epsilon)^2} + 1]},$$

$$\delta = 1/\alpha,$$

$$\Gamma_{\perp} = \frac{\eta_2 \cos\theta_i - \eta_1 \cos\theta_t}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}, \quad \tau_{\perp} = \frac{2\eta_2 \cos\theta_i}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}, \quad 1 + \Gamma_{\perp} = \tau_{\perp}$$

$$\Gamma_{\parallel} = \frac{\eta_2 \cos\theta_t - \eta_1 \cos\theta_i}{\eta_2 \cos\theta_t + \eta_1 \cos\theta_i}, \quad \tau_{\parallel} = \frac{2\eta_2 \cos\theta_i}{\eta_2 \cos\theta_t + \eta_1 \cos\theta_i}, \quad 1 + \Gamma_{\parallel} = \tau_{\parallel} \left(\frac{\cos\theta_t}{\cos\theta_i}\right), \quad \beta_1 \sin\theta_i = \beta_2 \sin\theta_t,$$

$$\theta_r = \theta_i$$

For normal incidence,  $\theta_i = 0$

$$\text{Poynting's Vector} = \vec{E} \times \vec{H}, \quad \text{Average Poynting's Vector} = \frac{1}{2} \text{Re}(\vec{E}_s \times \vec{H}_s^*)$$

### Differentials:

$$d\vec{l} = \vec{a}_\rho d\rho + \vec{a}_\phi \rho d\phi + \vec{a}_z dz, \quad d\vec{s} = \vec{a}_\rho \rho d\phi dz + \vec{a}_\phi \rho dz + \vec{a}_z \rho d\rho d\phi, \quad dv = \rho d\rho d\phi dz$$

$$d\vec{l} = \vec{a}_r dr + \vec{a}_\theta r d\theta + \vec{a}_\phi r \sin\theta d\phi, \quad d\vec{s} = \vec{a}_r r^2 \sin\theta d\theta d\phi + \vec{a}_\theta r \sin\theta dr d\phi + \vec{a}_\phi r dr d\theta, \quad dv = r^2 \sin\theta dr d\theta d\phi$$