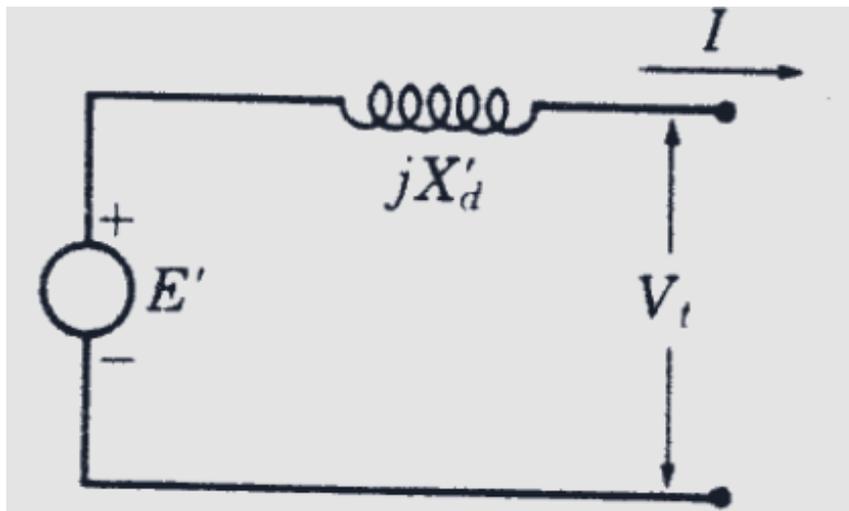


# The Equal Area Criterion

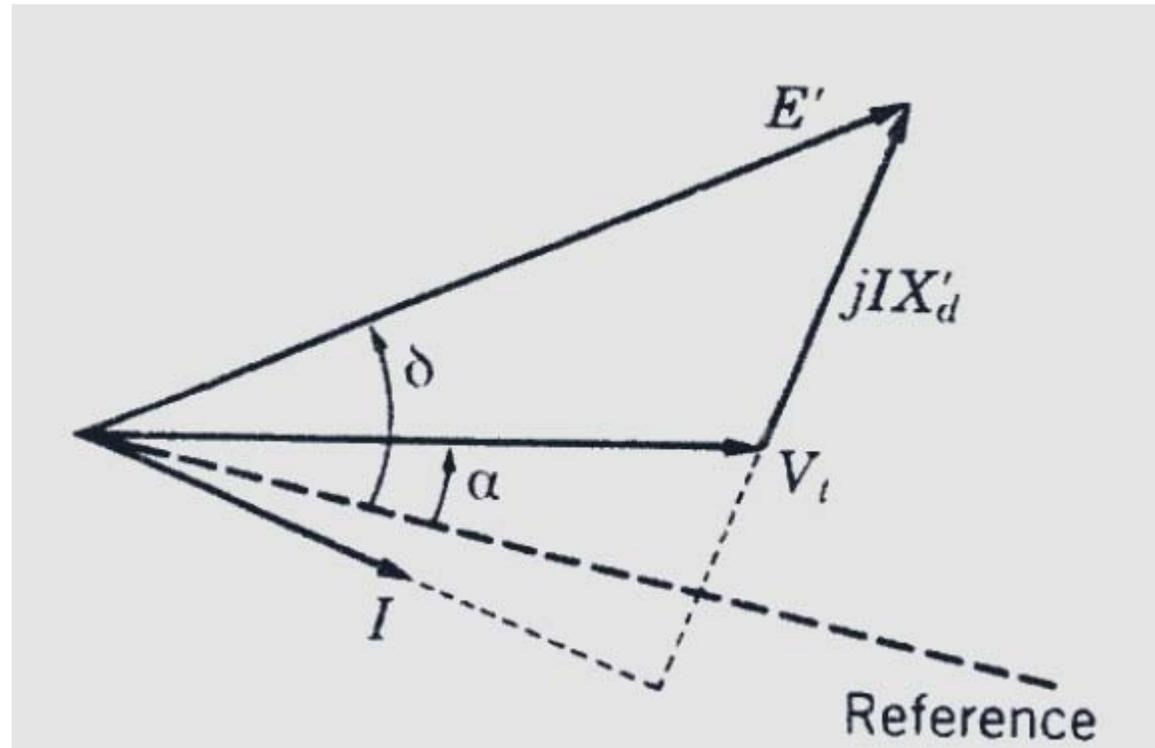
One of the methods of solving the swing equation is by graphical technique, and is applicable to one or two machines under the following assumptions:

1.  $P_m$ , the mechanical power input, does not change during the swing
2.  $P_e$ , the electrical power output, is obtained from the steady state solution of the system and is given by

$$P_e = \frac{E'V}{x_e} \sin \delta; \quad x_e = x'_d + x_{ext}$$
$$= P_{\max} \sin \delta$$

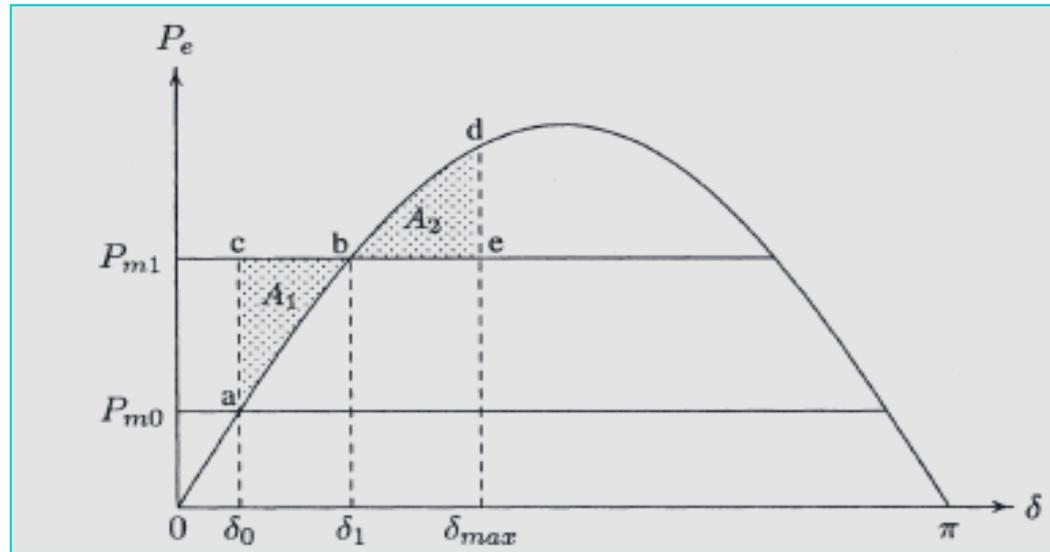


- The machines are represented by transient voltage  $E'$  behind the transient reactance  $x_d'$



- The rotor angle  $\delta$  is in phase with excitation voltage  $E'$
- Damping powers are negligible

Let us start with a one machine system connected to an infinite bus through reactance  $X_{\text{ext}}$ . Observe the power angle characteristic given below.

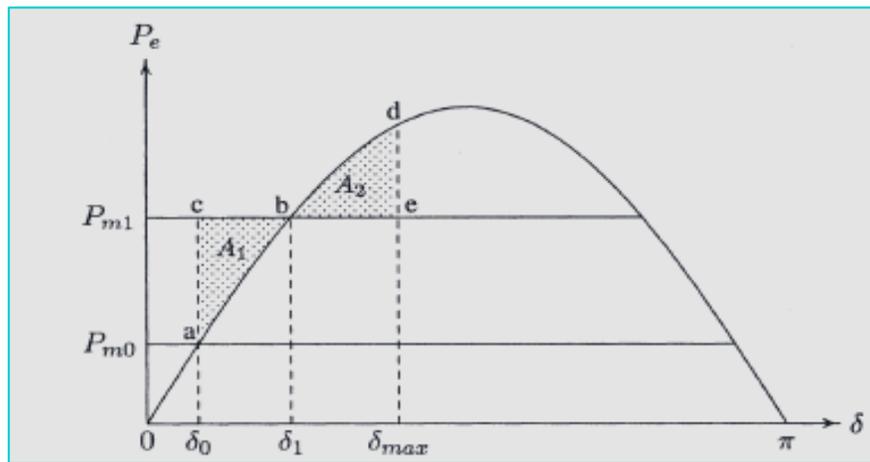


Let the machine operate initially at steady state with  $\delta = \delta_0$  corresponding to mechanical power  $P_{m0} = P_{e0}$  as shown in the figure. We know the electrical power output is given as,

$$P_e = P_{\max} \sin \delta$$

Consider a sudden step increase in input power to  $P_{m1}$ . Since  $P_{m1} > P_{e0}$ , the machine accelerates and  $\delta$  increases. The excess energy stored is the area  $A_1$ .

With increase in  $\delta$  electrical power increases and when  $\delta = \delta_1$  the electrical power matches the new input power  $P_{m1}$  and the acceleration ( $d^2 \delta / dt^2$ ) is zero.



Though the acceleration is zero, the machine runs above synchronous speed, hence  $\delta$  and electrical power continues to increase. Now  $P_m < P_e$  causing rotor to decelerate towards synchronous speed until  $\delta = \delta_{max}$ . At this point, the kinetic energy stored by the rotor while accelerating has been completely returned to the system. The energy given up is represented by the area  $A_2$ .

At d the rotor speed again synchronous although the rotor angle has advanced to  $\delta_{max}$ . The accelerating power is still negative (retarding) and so the rotor cannot remain at synchronous speed but must continue to slow down. The relative velocity is negative and rotor angle moves back from  $\delta_{max}$  along the power angle curve to point b at which point the rotor speed is less than synchronous (deceleration is zero). From b to a the machine accelerates until synchronous speed is achieved at a (the zero damping case). And the cycle continues to repeat.

The excess energy stored in the rotor inertia during acceleration of the rotor is shown in the shaded area  $A_1$ , and that returned during deceleration, as the shaded area  $A_2$ . For the net energy to be zero,  $A_1$  must be equal to  $A_2$ .

This is the equal area criterion.

Let us work this out mathematically. The swing equation is,

$$M \frac{d^2 \delta}{dt^2} = P_m - P_e = P_a$$

Multiply both sides by  $d\delta/dt$

$$M \frac{d\delta}{dt} \frac{d^2 \delta}{dt^2} = P_a \frac{d\delta}{dt}$$

Or,  $\frac{M}{2} \frac{d}{dt} \left[ \frac{d\delta}{dt} \right]^2 = P_a \frac{d\delta}{dt}$

Multiplying by  $dt$  and integrating from  $\delta_0$  to  $\delta_{\max}$

$$\frac{M}{2} \left[ \frac{d\delta}{dt} \right]^2 \Big|_{\delta_0}^{\delta_{\max}} = \int_{\delta_0}^{\delta_{\max}} (P_m - P_e) d\delta$$

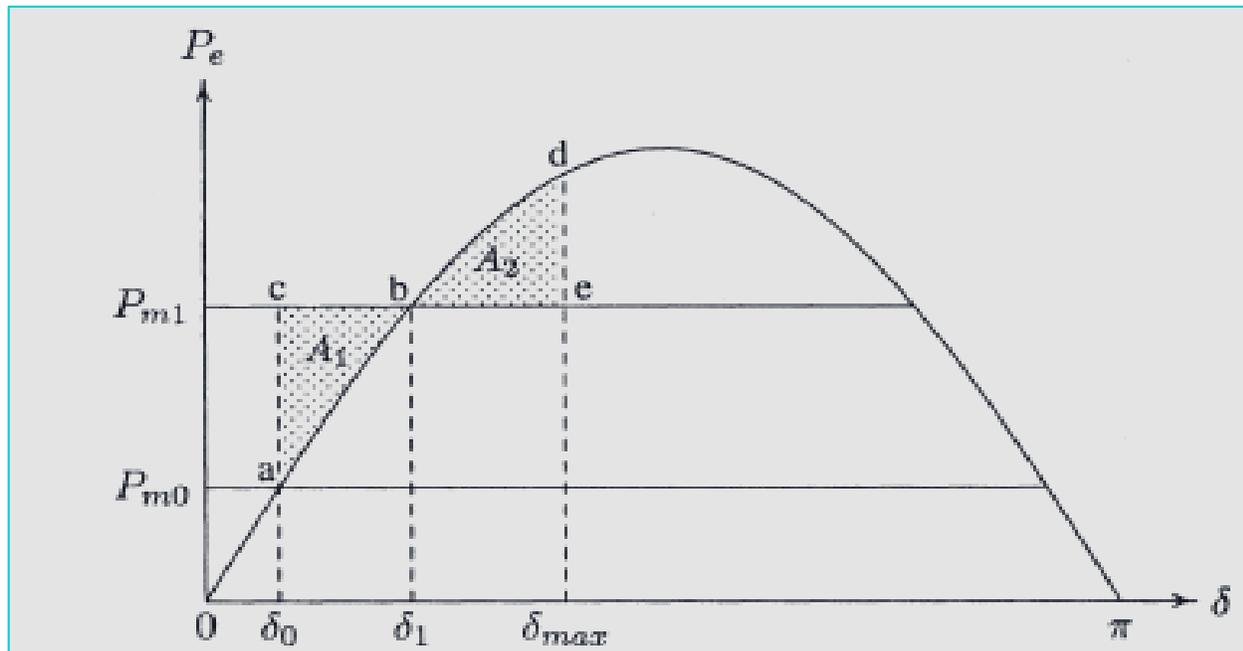
The rotor speed  $d\delta/dt=0$  at  $\delta_0$  as well as at  $\delta_{\max}$  (synch. speed), giving the left hand side to be zero. Or,

$$\int_{\delta_o}^{\delta_{\max}} (P_m - P_e) d\delta = 0$$

$$\text{Or, } \int_{\delta_o}^{\delta_1} (P_m - P_e) d\delta + \int_{\delta_1}^{\delta_{\max}} (P_m - P_e) d\delta = 0$$

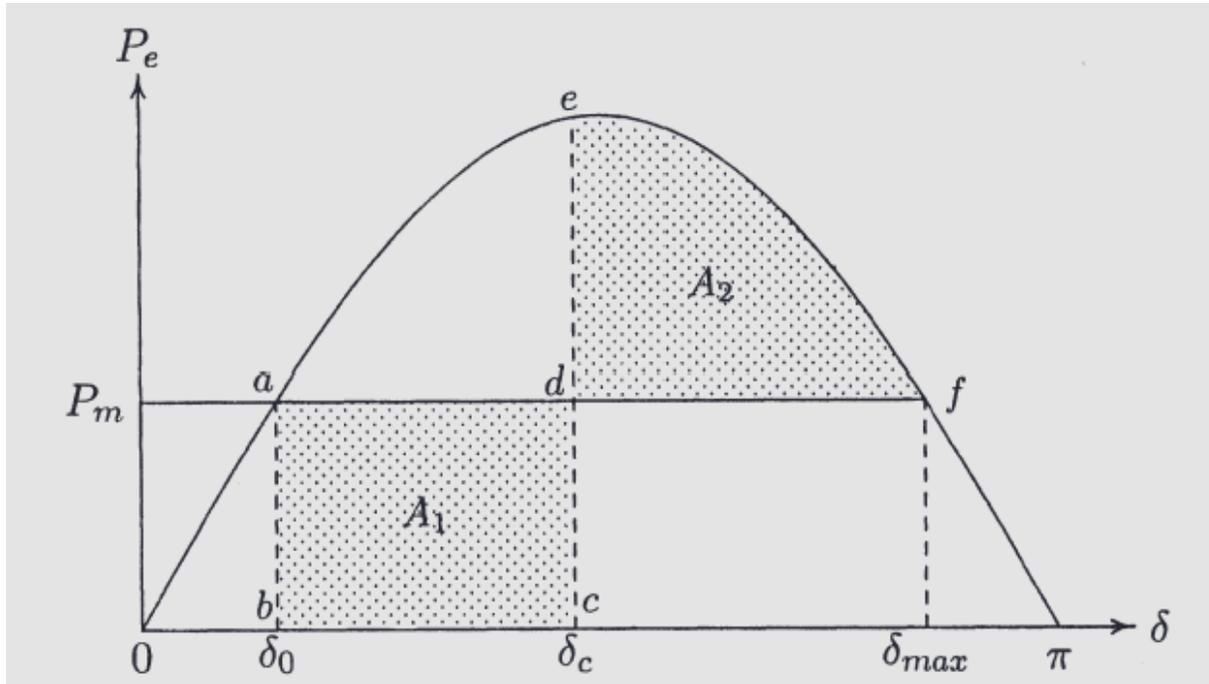
$$\text{Or, } \int_{\delta_o}^{\delta_1} (P_m - P_e) d\delta = \int_{\delta_1}^{\delta_{\max}} (P_e - P_m) d\delta$$

$$\text{Or, } A_1 = A_2$$



# The Critical Clearing Time

Consider a symmetrical three phase fault at the generator terminal cleared by it-self and the original system conditions are restored. The power angle characteristic is shown below. The steady state power is  $P_m$  when the fault is applied.



The shaded area ( $A_1$ ) representing the kinetic energy is dependent upon the time taken to clear the fault. If  $\delta_c$  is increased,  $A_1$  is increased. Equal area criterion requires  $A_2$  to be increased. If the delay in clearing is prolonged so that  $\delta$  swings past  $\delta_m$ , the rotor speed is more than synchronous and again accelerating power is encountered. This will lead to further increase in  $\delta$  and hence instability will result. Therefore, there is a critical angle for clearing the fault in order to satisfy the requirements for equal area criterion for stability. This angle, called critical clearing angle ( $\delta_c$ ) and corresponding critical clearing time ( $t_c$ ) is obtained as follows.

The area  $A_1$  is,

$$A_1 = \int_{\delta_o}^{\delta_c} P_m d\delta = P_m (\delta_c - \delta_o)$$

While area  $A_2$  is,

$$\begin{aligned} A_2 &= \int_{\delta_c}^{\delta_m} (P_{\max} \sin \delta - P_m) d\delta \\ &= P_{\max} (\cos \delta_c - \cos \delta_m) - P_m (\delta_m - \delta_c) \end{aligned}$$

Equating the expression for  $A_1$  and  $A_2$ ,

$$\cos \delta_c = \frac{P_m}{P_{\max}} (\delta_m - \delta_o) + \cos \delta_m$$

From the power angle curve,  $\delta_m = \pi - \delta_o$ , and  $P_m = P_{\max} \sin \delta_o$

Substituting,

$$\delta_c = \cos^{-1} [(\pi - 2\delta_o) \sin \delta_o - \cos \delta_o]$$

$\delta_c$  and  $t_c$  are related by,

$$\delta_c = \frac{\omega_s P_m}{4H} t_c^2 + \delta_o$$

$$\text{Or, } t_c = \sqrt{\frac{4H(\delta_c - \delta_o)}{\omega_s P_m}}$$

In a 2 machine system, if the fault occurs on the machine bus there will be no power transfer. However, if fault occurs on some section of a double circuit line, power transfer may be possible. Clearing the fault may not restore original circuit conditions. The equal area criterion can be applied to such cases also. The figure below shows such a scenario.

