

Example 1: Unsteady State Evaporation, the Arnold Cell

We wish to predict the rate at which a volatile liquid A evaporates into pure B in a tube of infinite length. The liquid level is maintained at $z = 0$ at all times. The temperature and pressure are assumed constant, and the vapors of A and B form an ideal gas mixture. Hence the molar density c is constant throughout the gas phase, and D_{AB} may be considered to be constant. It is further assumed that species B is insoluble in liquid A, and that the molar average velocity in the gas phase does not depend on the radial coordinate.

Solution:

C.E. for mixture $\frac{\partial c}{\partial t} = -\nabla \cdot (c v^*) + \sum_{\alpha=1}^N R_{\alpha}$

For a mixture with constant total concentration
 $c = \text{const.}$ and no reactions $\Rightarrow \nabla \cdot v^* = 0$

$\Rightarrow \frac{\partial v_z^*}{\partial z} = 0 \Rightarrow v_z^* = v_z^*(t) \neq f(z)$

@ $z=0$

From table 17.8-1 $v_z^* = \frac{N_{A20} + N_{B20}}{c}$

Table 17.8-2 $\rightarrow = -\frac{D_{AB}}{1-x_{A0}} \frac{\partial x_A}{\partial z} \Big|_{z=0}$ \downarrow
B insoluble

E 19.1-17: $c \left(\frac{\partial x_A}{\partial t} + v_z^* \cdot \nabla x_A \right) = c D_{AB} \nabla^2 x_A + (R_A + R_B)$

$\frac{\partial x_A}{\partial t} - v_z^* \frac{\partial x_A}{\partial z} = D_{AB} \frac{\partial^2 x_A}{\partial z^2}$

$\frac{\partial x_A}{\partial t} - \left(\frac{D_{AB}}{1-x_{A0}} \frac{\partial x_A}{\partial z} \Big|_{z=0} \right) \frac{\partial x_A}{\partial z} = D_{AB} \frac{\partial^2 x_A}{\partial z^2}$

- | | |
|------------------------|----------------|
| $t = 0$ | $x_A = 0$ |
| $z = 0$ | $x_A = x_{A0}$ |
| $z \rightarrow \infty$ | $x_A = 0$ |

similarity transformation: scaling

(2)

$$\frac{1}{t} \sim \frac{D_{AB}}{z^2} \Rightarrow z = \frac{z}{\sqrt{t D_{AB}}}$$

$$\frac{\partial x_A}{\partial t} = \frac{dx_A}{dz} \frac{\partial z}{\partial t} = -\frac{1}{2} \frac{z}{t} \frac{dx_A}{dz}$$

$$\frac{\partial x_A}{\partial z} = \frac{dx_A}{dz} \frac{\partial z}{\partial z} = \frac{1}{\sqrt{t D_{AB}}} \frac{dx_A}{dz}$$

$$\frac{\partial^2 x_A}{\partial z^2} = \frac{d^2 x_A}{dz^2} \left(\frac{\partial z}{\partial z} \right)^2 = \frac{1}{t D_{AB}} \frac{d^2 x_A}{dz^2}$$

$$-\frac{1}{2} \frac{z}{t} \frac{dx_A}{dz} - \left(\frac{D_{AB}}{1-x_{A0}} \frac{1}{\sqrt{t D_{AB}}} \frac{dx_A}{dz} \Big|_{z=0} \right) \frac{dx_A/dz}{\sqrt{t D_{AB}}} =$$

$$\frac{D_{AB}}{\sqrt{t D_{AB}}} \frac{d^2 x_A}{dz^2}$$

let $X = \frac{x_A}{x_{A0}}$,

$$\Rightarrow \frac{d^2 X}{dz^2} + \left[\frac{1}{2} z + \frac{x_{A0}}{1-x_{A0}} \frac{dx_A}{dz} \Big|_{z=0} \right] \frac{dX}{dz} = 0$$

$$\frac{d^2 X}{dz^2} + \frac{1}{2} (z - \beta) \frac{dX}{dz} = 0, \quad \beta = -\frac{2x_{A0}}{1-x_{A0}} \frac{dx_A}{dz} \Big|_{z=0}$$

$$z = 0$$

$$X = 1$$

$$z \rightarrow \infty$$

$$X = 0$$

$$\text{let } Y = \frac{dx}{d\eta} \Rightarrow \frac{dY}{d\eta} + \frac{1}{2}(2-\beta)Y = 0 \quad (3)$$

$$\Rightarrow \ln(Y) = -\frac{1}{2} \int (2-\beta) d\eta$$

$$\text{let } u = 2-\beta. \Rightarrow du = d\eta.$$

$$\Rightarrow \ln(Y) = -\frac{1}{4} (2-\beta)^2 + C_1'$$

$$\frac{dx}{d\eta} = Y = C_1 e^{-\frac{(2-\beta)^2}{4}}$$

$$x = C_1 \int_0^2 e^{-\frac{(\bar{\eta}-\beta)^2}{4}} d\bar{\eta} + C_2$$

$$\text{BC1} \Rightarrow C_2 = 1$$

$$\text{BC2} \Rightarrow C_1 = \frac{1}{\int_0^{\infty} e^{-\frac{(\bar{\eta}-\beta)^2}{4}} d\bar{\eta}}$$

$$\Rightarrow X = 1 - \frac{\int_0^2 e^{-\frac{(\bar{\eta}-\beta)^2}{4}} d\bar{\eta}}{\int_0^{\infty} e^{-\frac{(\bar{\eta}-\beta)^2}{4}} d\bar{\eta}}$$

$$\alpha = \frac{2-\beta}{2}$$

$$X = 1 - \frac{\int_{-\frac{\beta}{2}}^{\frac{2-\beta}{2}} e^{-\alpha^2} d\alpha}{\int_{-\infty}^{\infty} e^{-\alpha^2} d\alpha}$$

$$X(\eta) = 1 - \frac{\text{erf}\left(\frac{\eta-\beta}{2}\right) + \text{erf}\left(\frac{\beta}{2}\right)}{\text{erf}\left(\frac{\eta-\beta}{2}\right) + \text{erf}\left(\frac{\beta}{2}\right)}$$

$$= \frac{1 + \text{erf}\left(\frac{\beta}{2}\right) - \text{erf}\left(\frac{\eta-\beta}{2}\right) - \text{erf}\left(\frac{\beta}{2}\right)}{1 + \text{erf}\left(\frac{\beta}{2}\right)}$$

$$= \frac{1 - \text{erf}\left(\frac{\eta-\beta}{2}\right)}{1 + \text{erf}\left(\frac{\beta}{2}\right)}$$

recall $\beta = - \frac{2 X_{A0}}{1 - X_{A0}} \left. \frac{dX_A}{d\eta} \right|_{\eta=0}$

$$= - \frac{2 X_{A0}}{1 - X_{A0}} \cdot \frac{-1}{1 + \text{erf}\left(\frac{\beta}{2}\right)} \left[\frac{d}{d\eta} \left(\text{erf}\left(\frac{\eta-\beta}{2}\right) \right) \right]_{\eta=0}$$

$$= \frac{2 X_{A0}}{1 - X_{A0}} \cdot \frac{1}{1 + \text{erf}\left(\frac{\beta}{2}\right)} \cdot \frac{2}{\sqrt{\pi}} \left(e^{-\left(\frac{\eta-\beta}{2}\right)^2} \right)_{\eta=0}$$

$$\beta = \frac{2 X_{A0}}{1 - X_{A0}} \cdot \frac{1}{1 + \text{erf}\left(\frac{\beta}{2}\right)} \cdot \frac{1}{\sqrt{\pi}} e^{-\frac{\beta^2}{4}}$$

Example 2: Gas absorption with Chemical Rapid Chemical Reaction

Gas A is absorbed by a stationary liquid solvent S, the latter containing solute B. Species A reacts with B in an instantaneous irreversible reaction according to the equation $aA + bB \rightarrow \text{Products}$. It may be assumed that Fick's second law adequately describes the diffusion processes, since A, B, and the reaction products are present in S in low concentrations. Obtain expressions for the concentration profiles.

Solution:

In this problem there will be a plane parallel to the interface at a distance z_R inside the liquid, which separates two regions one containing only A and another containing only B. Also,

$z_R = f(t)$. For A & B:

$$\frac{\partial C_A}{\partial t} = D_{AS} \frac{\partial^2 C_A}{\partial z^2} \quad 0 \leq z \leq z_R(t)$$

$$\frac{\partial C_B}{\partial t} = D_{BS} \frac{\partial^2 C_B}{\partial z^2} \quad z_R \leq z < \infty$$

$$t = 0 \quad C_B = C_{B\infty} \quad C_A = 0$$

$$z = 0 \quad C_A = C_{A0}$$

$$z = z_R \quad C_A = C_B$$

$$z = z_R \quad -\frac{1}{a} D_{AS} \frac{\partial C_A}{\partial z} = \frac{1}{b} D_{BS} \frac{\partial C_B}{\partial z}$$

$$z \rightarrow \infty \quad C_B = C_{B\infty}$$

⑥

$$\frac{C_A}{C_{A0}} = C_1 + C_2 \operatorname{erf}\left(\frac{z}{\sqrt{4D_Ast}}\right) \quad 0 \leq z \leq z_R.$$

$$\frac{C_B}{C_{B00}} = C_3 + C_4 \operatorname{erf}\left(\frac{z}{\sqrt{4D_Bst}}\right) \quad z_R \leq z < \infty$$

see 12.1-3 for solution.

applying BC (this will be next HW!).

0
0
0

$$\frac{C_A}{C_{A0}} = 1 - \frac{\operatorname{erf}(z/\sqrt{4D_Ast})}{\operatorname{erf}(z_R/\sqrt{4D_Ast})}$$

$$\frac{C_B}{C_{B00}} = 1 - \frac{1 - \operatorname{erf}(z/\sqrt{4D_Bst})}{1 - \operatorname{erf}(z_R/\sqrt{4D_Bst})}$$

and BC3 gives:

$$1 - \operatorname{erf}\sqrt{\frac{\gamma}{D_Bs}} = \frac{a C_{B00}}{b C_{A0}} \sqrt{\frac{D_Bs}{D_As}} \operatorname{erf}\sqrt{\frac{\gamma}{D_As}} \exp\left(\frac{\gamma}{D_As} - \frac{\gamma}{D_Bs}\right)$$

where $\gamma = \frac{z_R^2}{4t}$.

see Fig 20.1-2