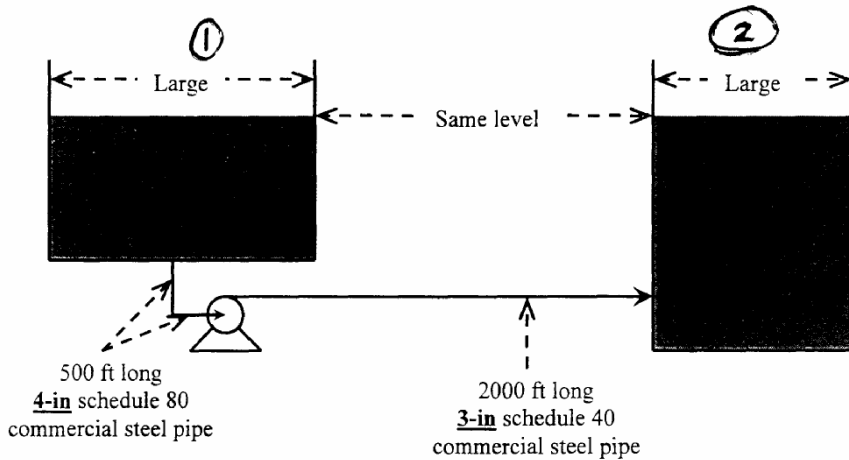


2<sup>nd</sup> Major Examination  
 Wednesday, December 15, 2004

**Q1. (25 points)**

Water ( $\rho = 62.4 \text{ lb}_m/\text{ft}^3$ ,  $\mu = 0.000672 \text{ lb}_m/\text{ft s}$ ) is pumped from one reservoir to another at a rate  $200 \text{ gpm}^s$  using a 70% efficient pump. The levels in the reservoirs are the same and both are open to atmosphere, see the figure below. Calculate the power requirement of the pump. Do not neglect the frictional losses in the pipes before and after the pump. <sup>s</sup>(gpm = 1 US gallon per minute)



MEB ① & ②

$$\frac{\Delta P}{\rho} + \frac{\Delta U^2}{2} + g\Delta z + w + f = 0$$

$$-w = +f$$

2 sections, after and before the pump.

Section 1: from Table 3.3  $D = 3.826 \text{ in}$   
 commercial steel pipe Table 3.2

$$E = 0.00015 \text{ ft}$$

$$E/D = \frac{0.00015}{3.826/12} = 0.00047$$

$$U = \frac{Q}{\frac{\pi}{4} D^2} = \frac{200 \frac{\text{gal}}{\text{min}} * \frac{4}{\pi} * \left(\frac{12 \text{ in}}{3.826 \text{ in}}\right)^2 * \frac{\text{ft}^3}{7.48 \text{ gal}} * \frac{\text{min}}{60 \text{ s}}}{}$$

$$u = 5.5816 \text{ ft/s}$$

$$Re = \frac{\rho u D}{\mu} = \frac{62.4 \frac{\text{lbm}}{\text{ft}^3} * 5.5816 \frac{\text{ft}}{\text{s}} * \frac{3.826 \text{ in}}{12 \frac{\text{in}}{\text{ft}}}}{0.000672 \frac{\text{lbm}}{\text{ft} \cdot \text{s}}}$$

$$Re = 165,249. = 1.7 * 10^5$$

Using Eq. 3.41 or Fig. 3.10

$$f_F \approx 0.0048$$

Using Eq. 3.37  $f = 2 f_F u^2 \frac{L}{D}$

$$f = 2 * 0.0048 * (5.5816)^2 \left(\frac{\text{ft}}{\text{s}}\right)^2 * \frac{500 \text{ ft}}{\frac{3.826 \text{ in}}{12 \frac{\text{in}}{\text{ft}}}}$$
$$\approx 469 \frac{\text{ft}^2}{\text{s}^2}$$

Section 2

$$D = 3.068 \quad \epsilon = 0.00015$$

$$\epsilon/D = 0.0005867$$

$$u = 8.680 \quad Re = 206077 = 2. * 10^5$$

$$f_F \approx 4.81 * 10^{-3} \Rightarrow f = 5670$$

$$\therefore W = 5670 + 469 = 6140 \frac{\text{ft}^2}{\text{s}^2}$$

$$\text{Power} = \frac{m \dot{w}}{\eta} = \frac{Q P w}{\eta}$$

$$P = \frac{200 \text{ gal}}{\text{min}} * \frac{\text{ft}^3}{7.4805 \text{ gal}} * \frac{\text{min}}{60 \text{ s}} * 62.4 \frac{\text{lb}_m}{\text{ft}^3} * 6140 \frac{\text{ft}^2}{\text{s}^2}$$

$$0.7 * 32.2 \frac{\text{lb}_m \cdot \text{ft}}{\text{lb}_f \cdot \text{s}^2}$$

$$P = 7574 \frac{\text{lb}_f \cdot \text{ft}}{\text{s}} * \frac{1.341 * 10^{-3} \text{ hp}}{0.7376 \frac{\text{ft} \cdot \text{lb}_f}{\text{s}}}$$

$$P = 13.8 \text{ hp}$$

**Q2. (25 points)**

Calculate the drag coefficient for a dust particle of diameter 1 micron<sup>s</sup> and SG = 2 settling through air of density 1.2 kg/m<sup>3</sup> and viscosity 1.8\*10<sup>-5</sup> Pa/s.

<sup>s</sup>(1 micron = 1\*10<sup>-6</sup> meter)

$$C_D = \frac{4}{3} \frac{g D}{u_t^2} \frac{\rho_s - \rho_f}{\rho_f}$$

$$= \frac{4}{3} \frac{(9.8) (1 \times 10^{-6})}{u_t^2} \left( \frac{2000 - 1.2}{1.2} \right)$$

$$= \frac{0.02176}{u_t^2} \quad \dots \dots (5 \text{ points})$$

Find  $u_t$       assume laminar flow  $\Rightarrow C_D = \frac{24}{Re}$   
 $\uparrow$  ( $Re < 1$ )

$$\Rightarrow \frac{24}{\rho_f u_t D} = \frac{0.02176}{u_t^2} \quad \dots \dots (5 \text{ point})$$

$$\frac{24}{(1.2) (1 \times 10^{-6})} = \frac{0.02176}{u_t^2}$$

$$\frac{24}{1.8 \times 10^{-5}}$$

$$\Rightarrow u_t = 6.0458 \times 10^{-5} \left( \frac{m}{s} \right) \quad \dots \dots (3 \text{ po})$$

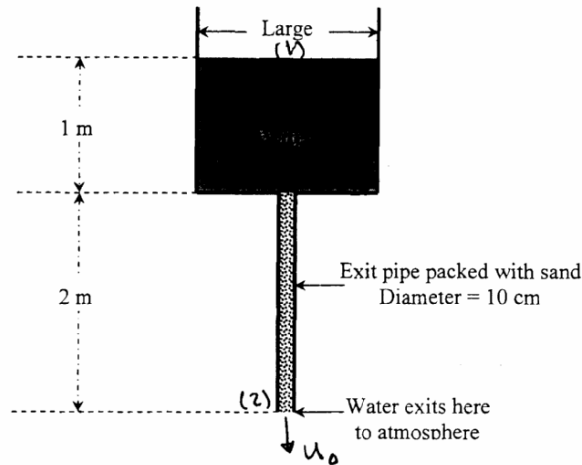
check  $Re$  =  $\frac{(1.2) (6.0458 \times 10^{-5}) (1 \times 10^{-6})}{1.8 \times 10^{-5}}$

(5 points) =  $4.0305 \times 10^{-6} < 1 \Rightarrow$  laminar assumption was correct

$$\Rightarrow C_D = \frac{0.02176}{(6.0458 \times 10^{-5})^2} = 5953211.9 \quad \leftarrow$$

**Q3. (25 points)**

Water drains from a tank by gravity through a pipe packed with sand. The system is sketched in the figure below. The sand particles are uniform with an average diameter of 0.2 mm and a void fraction of 0.3. Calculate the rate of water drainage in ml/min.



$$Q = \frac{\pi}{4} D^2 u_0$$

M.E.B. (1) and (2):  $\frac{\Delta P}{\rho} + \frac{\Delta u^2}{2} + g \Delta z + \cancel{W} + F = 0$   $= 0$  ( $P_1 = P_2 = P_{atm}$ )  $= 0$  (No shaft work)

$$\Rightarrow \frac{u_0^2}{2} + g \Delta z + F = 0 \quad (1) \quad \text{+10}$$

$$F = \frac{150 \mu L (1-\epsilon)^2}{\rho D_p^2 \epsilon^3} + 1.75 \frac{u_0^2 L (1-\epsilon)}{D_p \epsilon^3} \quad \leftarrow (4.25) \text{ in the text}$$

$$\text{or } F = a u_0 + b u_0^2$$

$$a = \frac{150 \mu L (1-\epsilon)^2}{\rho D_p^2 \epsilon^3} \quad , \quad b = \frac{1.75 L (1-\epsilon)}{D_p \epsilon^3}$$

Substituting in (1) gives:

$$\frac{u_0^2}{2} + a u_0 + b u_0^2 + c = 0 \quad \left\{ c = g \Delta z \right.$$

$$\Rightarrow \left(\frac{1}{2} + b\right) u_0^2 + a u_0 + c = 0$$

$$\text{or } u_0^2 + a' u_0 + c' = 0 \quad \left\{ \begin{array}{l} a' = \frac{a}{(\frac{1}{2} + b)} \\ c' = \frac{c}{\frac{1}{2} + b} \end{array} \right.$$

one equation in one unknown ( $u_0$ )

$$\Rightarrow u_0 = -\frac{a'}{2} + \frac{1}{2} \sqrt{a'^2 - 4c'} \quad \text{+S}$$

$$a' = \frac{150 \mu\text{L}}{8 D_p^2} \frac{(1-\varepsilon)^2}{\varepsilon^3}$$

$$\rho = 1000 \frac{\text{kg}}{\text{m}^3}, \quad \mu = 0.001 \frac{\text{kg}}{\text{m}\cdot\text{s}}$$

$$L = 2 \text{ m}, \quad D_p = 0.2 \times 10^{-3} \text{ m}, \quad \varepsilon = 0.3$$

$$\Rightarrow a = 136,111 \text{ m/s}$$

$$b = \frac{1.75 L}{D_p \varepsilon^3} (1-\varepsilon) \Rightarrow b = 453,704$$

$$c = g \Delta z = -3 * 9.81 = -29.43 \text{ m}^2/\text{s}^2$$

$$a' = \frac{a}{\frac{1}{2} + b} = 0.30$$

$$c' = \frac{c}{\frac{1}{2} + b} = -6.49 \times 10^{-5}$$

$$u_0 = \frac{1}{2} \sqrt{a'^2 - 4c'} - \frac{a'}{2} = 2.16 \times 10^{-4} \text{ m/s}$$

$$Q = \frac{\pi}{4} D^2 u_0 = \frac{\pi}{4} * (0.1)^2 * 2.16 \times 10^{-4} = 1.70 \times 10^{-6} \frac{\text{m}^3}{\text{s}}$$

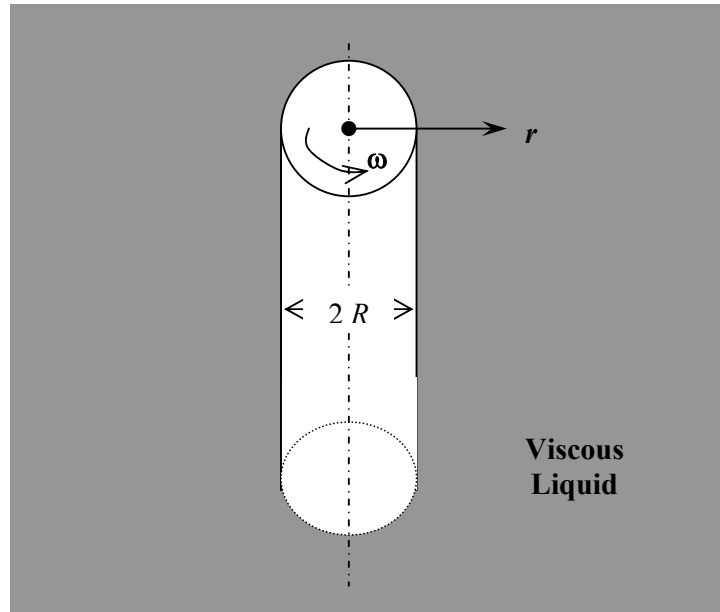
$$\text{or } Q = 1.70 \times 10^{-6} \frac{\text{m}^3}{\text{s}} * \frac{1000 \text{ L}}{1 \text{ m}^3} * \frac{1000 \text{ mL}}{1 \text{ L}} * \frac{60 \text{ s}}{1 \text{ min}}$$

$$\Rightarrow \boxed{Q = 102 \frac{\text{mL}}{\text{min}}}$$

Q4. (25 points)

A long vertical cylindrical rod of radius  $R$  is steadily rotated counterclockwise with angular velocity  $\omega$  in a very large volume of an incompressible Newtonian liquid. The liquid extends from the surface of the rod effectively to infinity, where it may be considered at rest.

- Using the proper simplifying assumptions, derive an equation for the fluid velocity,  $v_\theta$ , around the rod as a function of the radial coordinate.
- Derive an expression for the shear stress,  $\tau_{r\theta}$ , at the surface of the rod.
- If the length of the rod is  $L$ , derive an expression for the torque required to rotate the rod.



a)

Assumptions: 1) steady state, 2) Newtonian, incompressible fluid  
 3) Axisymmetry, 4)  $v_r = v_z = 0$ , 5)  $v_\theta \neq f(z \text{ or } \theta)$

$\Rightarrow v_\theta = f(r)$ .

Momentum Balance: { Equation 5.75 in the text }

only  $\theta$ -direction is needed:

$$\rho \left( \frac{\partial v_\theta}{\partial t} + v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_r v_\theta}{r} + v_\theta \frac{\partial v_\theta}{\partial z} \right) = -\frac{1}{r} \frac{\partial p}{\partial \theta}$$

$+ \mu \left[ \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial (r v_\theta)}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_\theta}{\partial \theta^2} + \frac{2}{r^2} \frac{\partial v_r}{\partial \theta} + \frac{\partial^2 v_\theta}{\partial z^2} \right] + \rho g_\theta$

$\Rightarrow \mu \left[ \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial (r v_\theta)}{\partial r} \right) \right] = 0$

$\frac{d}{dr} \left( \frac{1}{r} \frac{d}{dr} (r v_\theta) \right) = 0$

*Annotations:*  
 -  $v_r = 0, v_z = 0$   
 -  $v_\theta \neq f(\theta)$   
 -  $\rho \neq f(\theta)$   
 -  $g_\theta = 0$  (gravity has no effect in the  $\theta$  direction)  
 - Axisymmetry

$$\begin{cases} \Rightarrow \frac{1}{r} \frac{d}{dr} (r v_\theta) = c_1 \\ \Rightarrow \frac{d}{dr} (r v_\theta) = C_1 r \\ \Rightarrow r v_\theta = C_1 \frac{r^2}{2} + C_2 \\ \Rightarrow v_\theta = C_1 \frac{r}{2} + \frac{C_2}{r} \end{cases}$$

$$\begin{cases} \text{Boundary conditions:} & \text{at } r = R & v_\theta = \omega R \\ & r \rightarrow \infty & v_\theta = 0 \\ \therefore C_1 = 0 & (\text{for finite solution}) \\ \therefore \omega R = \frac{C_2}{R} & \Rightarrow C_2 = \omega R^2 \\ \therefore v_\theta = \omega R^2 / r \end{cases}$$

$$\begin{cases} \text{b)} & \tau_{r\theta} = \mu \left\{ r \frac{\partial}{\partial r} \left( \frac{v_\theta}{r} \right) + \frac{1}{r} \frac{\partial v_r}{\partial \theta} \right\} \quad \{\text{eq. 5.63 in the text}\} \\ \therefore \tau_{r\theta} = \mu \left\{ r \frac{d}{dr} \left( \frac{v_\theta}{r} \right) \right\} \\ \frac{v_\theta}{r} = \frac{\omega R^2}{r^2} \Rightarrow \frac{d}{dr} \left( \frac{v_\theta}{r} \right) = -2\omega R^2 / r^3 \\ \Rightarrow \tau_{r\theta} = -2\omega \mu R^2 / r^2 \Rightarrow \tau_{r\theta} \Big|_{r=R} = -2\omega \mu \end{cases}$$

$$\begin{cases} \text{c)} & T = -\tau_{r\theta} \Big|_{r=R} * (2\pi R L) * R \\ & = -2\pi R^2 L * \tau_{r\theta} \Big|_{r=R} \\ \Rightarrow T = 4\pi R^2 L \omega \mu \end{cases}$$