

CHE 203
HW # 5

- 9.4 a. Endothermic. The reactor will have to be heated to keep the temperature constant. The temperature would decrease under adiabatic conditions. The energy required to break the reactant bonds is more than the energy released when the product bonds are formed.

$$b. \quad \Delta \hat{U}_r^0 = \Delta \hat{H}_r^0 - RT \left[\sum_{\text{gaseous products}} \nu_i - \sum_{\text{gaseous reactants}} \nu_i \right] = 69.36 \frac{\text{kJ}}{\text{mol}} - \frac{8.314 \text{ J}}{\text{mol} \cdot \text{K}} \left| \frac{1 \text{ kJ}}{10^3 \text{ J}} \right| \frac{298 \text{ K}}{1} (7-0)$$

$$= \underline{52.0 \text{ kJ/mol}}$$

$\Delta \hat{U}_r^0$ is the change in internal energy when 1 g-mole of $\text{CaC}_2(\text{s})$ and 5 g-moles of $\text{H}_2\text{O}(\text{l})$ at 25°C and 1 atm react to form 1 g-mole of $\text{CaO}(\text{s})$, 2 g-moles of $\text{CO}_2(\text{g})$ and 5 g-moles of $\text{H}_2(\text{g})$ at 25°C and 1 atm.

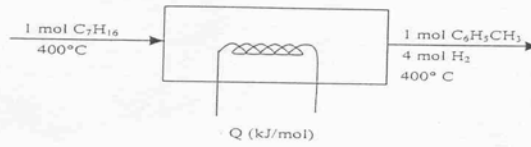
$$c. \quad Q = \Delta U = \frac{n_{\text{CaC}_2} \Delta \hat{U}_r^0}{\nu_{\text{CaC}_2}} = \frac{150 \text{ g CaC}_2}{64.10 \text{ g}} \left| \frac{1 \text{ mol}}{1 \text{ mol CaC}_2} \right| \frac{52.0 \text{ kJ}}{1 \text{ mol CaC}_2} = \underline{121.7 \text{ kJ}}$$

Heat must be transferred to the reactor.

- 9.5 a. Given reaction = (1) - (2) $\xrightarrow{\text{Hess's law}} \Delta \hat{H}_r^0 = \Delta \hat{H}_{r1}^0 - \Delta \hat{H}_{r2}^0 = (1226 - 18,935) \text{ Btu/lb-mole} = \underline{-17,709 \text{ Btu/lb-mole}}$
- b. Given reaction = (1) - (2) $\xrightarrow{\text{Hess's law}} \Delta \hat{H}_r^0 = \Delta \hat{H}_{r1}^0 - \Delta \hat{H}_{r2}^0 = (-121,740 + 104,040) \text{ Btu/lb-mole} = \underline{-17,700 \text{ Btu/lb-mole}}$

- 9.8 a. $\Delta \hat{H}_{r1}^0 = (\Delta \hat{H}_f^0)_{\text{C}_2\text{H}_5\text{Cl}_4(\text{l})} - (\Delta \hat{H}_f^0)_{\text{C}_2\text{H}_6(\text{g})} \Rightarrow (\Delta \hat{H}_f^0)_{\text{C}_2\text{H}_5\text{Cl}_4(\text{l})} = -385.76 + 52.28 = \underline{-333.48 \text{ kJ/mol}}$
 $\Delta \hat{H}_{r2}^0 = (\Delta \hat{H}_f^0)_{\text{C}_2\text{HCl}_3(\text{l})} + (\Delta \hat{H}_f^0)_{\text{HCl}(\text{g})} - (\Delta \hat{H}_f^0)_{\text{C}_2\text{H}_2\text{Cl}_4(\text{l})} = -276.2 - 92.31 + 333.48 = \underline{-35.03 \text{ kJ/mol}}$
- b. Given reaction = (1) + (2) $\Rightarrow -385.76 - 35.03 = \underline{-420.79 \text{ kJ/mol}}$
- c. $Q = \Delta \hat{H} = \frac{300 \text{ mol C}_2\text{HCl}_3}{\text{h}} \left| \frac{-420.79 \text{ kJ}}{\text{mol}} \right| = \underline{-1.26 \times 10^5 \text{ kJ/h}} (= -35 \text{ kW})$
 Heat is evolved.

- 9.14 a. $C_7H_{16}(g) \rightarrow C_6H_5CH_3(g) + 4H_2(g)$
 Basis: 1 mol C_7H_{16}



b.

References: $C(s), H_2(g)$ at $25^\circ C$

substance	n_{in} (mol)	\hat{H}_{in} (kJ/mol)	n_{out} (mol)	\hat{H}_{out} (kJ/mol)
C_7H_{16}	1	\hat{H}_1	—	—
$C_6H_5CH_3$	—	—	1	\hat{H}_2
H_2	—	—	4	\hat{H}_3

$$C_7H_{16}(g, 400^\circ C): \hat{H}_1 = (\Delta \hat{H}_f^\circ)_{C_7H_{16}(g)} + \left[\int_{25}^{400} \overset{\text{Table 9.2}}{\hat{C}_p} dT \right]$$

$$= (-187.8 + 104.1) \text{ kJ/mol} = \underline{-83.7 \text{ kJ/mol}}$$

$$C_6H_5CH_3(g, 400^\circ C): \hat{H}_2 = (\Delta \hat{H}_f^\circ)_{C_6H_5CH_3(g)} + \left[\int_{25}^{400} \overset{\text{Table 9.2}}{\hat{C}_p} dT \right]$$

$$= (+50 + 60.2) \text{ kJ/mol} = \underline{110.2 \text{ kJ/mol}}$$

$$H_2(g, 400^\circ C): \hat{H}_3 = \hat{H}_{H_2}(400^\circ C) = \overset{\text{Table 9.2}}{\int_{25}^{400}} \hat{C}_p dT = \underline{10.89 \text{ kJ/mol}}$$

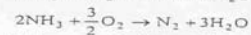
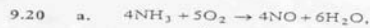
c.

1 mol C_7H_{16} reacted $\Rightarrow \xi = 1 \text{ mol}$

$$Q = \Delta H = \xi \Delta \hat{H}_r^\circ + \sum_{out} n_i \hat{H}_i - \sum_{in} n_i \hat{H}_i$$

$$= \{ (1)(237.8) + [(1)(60.2) + (4)(10.86)] - (1)(104.1) \} \text{ kJ} = 237.3 \text{ kJ (transferred to reactor)}$$

d. $\Delta \hat{H}_r(400^\circ C) = \frac{237.3 \text{ kJ}}{1 \text{ mol } C_7H_{16} \text{ react}} = \underline{237.3 \text{ kJ/mol}}$



References: $\text{N}_2(\text{g})$, $\text{H}_2(\text{g})$, $\text{O}_2(\text{g})$, at 25°C

Substance	\dot{n}_{in} (mol/min)	\dot{H}_{in} (kJ/mol)	\dot{n}_{out} (mol/min)	\dot{H}_{out} (kJ/mol)
NH_3	100	\dot{H}_1	-	-
Air	900	\dot{H}_2	-	-
NO	-	-	90	\dot{H}_3
H_2O	-	-	150	\dot{H}_4
N_2	-	-	716	\dot{H}_5
O_2	-	-	69	\dot{H}_6

$$\dot{H}_i = \Delta\dot{H}_i^0 + \int_{25}^T C_{p,i} dT$$

$$\text{NH}_3(\text{g}, 25^\circ\text{C}): \dot{H}_1 = (\Delta\dot{H}_f^0)_{\text{NH}_3} \stackrel{\text{Table B.1}}{=} \underline{\underline{-46.19 \text{ kJ/mol}}}$$

$$\text{Air}(\text{g}, 150^\circ\text{C}): \dot{H}_2 \stackrel{\text{Table B.8}}{=} \underline{\underline{3.67 \text{ kJ/mol}}}$$

$$\text{NO}(\text{g}, 700^\circ\text{C}): \dot{H}_3 = 90.37 + \int_{25}^{700} C_p dT \stackrel{\text{Table B.1, Table B.2}}{=} \underline{\underline{111.97 \text{ kJ/mol}}}$$

$$\text{H}_2\text{O}(\text{g}, 700^\circ\text{C}): \dot{H}_4 \stackrel{\text{Table B.1, Table B.3}}{=} \underline{\underline{-216.91 \text{ kJ/mol}}}$$

$$\text{N}_2(\text{g}, 700^\circ\text{C}): \dot{H}_5 \stackrel{\text{Table B.8}}{=} \underline{\underline{20.59 \text{ kJ/mol}}}$$

$$\text{O}_2(\text{g}, 700^\circ\text{C}): \dot{H}_6 \stackrel{\text{Table B.8}}{=} \underline{\underline{21.86 \text{ kJ/mol}}}$$

b. $\dot{Q} = \Delta\dot{H} = \sum_{\text{out}} \dot{n}_i \dot{H}_i - \sum_{\text{in}} \dot{n}_i \dot{H}_i = -4890 \text{ kJ/min} \times (1 \text{ min} / 60\text{s}) = \underline{\underline{-81.5 \text{ kW}}}$
(heat transferred from the reactor)

c. If molecular species had been chosen as references for enthalpy calculations, the extents of each reaction would have to be calculated and Equation 9.5-1b used to determine $\Delta\dot{H}$. The value of \dot{Q} would remain unchanged.