

7.16. (a) $\Delta E_k = 0$ ($u_1 = u_2 = 0$)
 $\Delta E_p = 0$ (no elevation change)
 $\Delta P = 0$ (the pressure is constant since restraining force is constant, and area is constant)
 $W_s = P\Delta V$ (the only work done is expansion work)
 $\dot{H} = 34980 + 35.5T$ (J/mol), $V_1 = 785 \text{ cm}^3$, $T_1 = 400 \text{ K}$, $P = 125 \text{ kPa}$, $Q = 83.8 \text{ J}$
 $n = \frac{PV}{RT} = \frac{125 \times 10^3 \text{ Pa}}{8.314 \text{ m}^3 \cdot \text{Pa} / \text{mol} \cdot \text{K}} \cdot \frac{785 \text{ cm}^3}{400 \text{ K}} \cdot \frac{1 \text{ m}^3}{10^6 \text{ cm}^3} = 0.0295 \text{ mol}$
 $Q = \Delta H = n(\hat{H}_2 - \hat{H}_1) = 0.0295 \text{ mol}[34980 + 35.5T_2 - 34980 - 35.5(400\text{K})]$ (J/mol)
 $83.8 \text{ J} = 0.0295[35.5T_2 - 35.5(400)] \Rightarrow T_2 = 480 \text{ K}$

i) $V = \frac{nRT}{P} = \frac{0.0295 \text{ mol}}{125 \times 10^3 \text{ Pa}} \cdot \frac{8.314 \text{ m}^3 \cdot \text{Pa}}{\text{mol} \cdot \text{K}} \cdot \frac{10^6 \text{ cm}^3}{1 \text{ m}^3} \cdot 480 \text{ K} = 941 \text{ cm}^3$
 ii) $W = P\Delta V = \frac{125 \times 10^3 \text{ N}}{\text{m}^2} \cdot (941 - 785) \text{ cm}^3 \cdot \frac{1 \text{ m}^3}{10^6 \text{ cm}^3} = 19.5 \text{ J}$
 iii) $Q = \Delta U + P\Delta V \Rightarrow \Delta U = Q - \Delta PV = 83.8 \text{ J} - 19.5 \text{ J} = 64.3 \text{ J}$

(b) $\Delta E_p = 0$

7.18 (b) $\Delta \hat{H} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s$ (The system is the liquid stream.)

$$\begin{array}{l} \Delta \hat{E}_k = 0 \text{ (no change in } m \text{ and } u) \\ \Delta \hat{E}_p = 0 \text{ (no elevation change)} \\ \hat{W}_s = 0 \text{ (no moving parts or generated currents)} \\ \hline \Delta \hat{H} = \hat{Q}, \hat{Q} > 0 \end{array}$$

(c) $\Delta \hat{H} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s$ (The system is the water)

$$\begin{array}{l} \Delta \hat{H} = 0 \text{ (} T \text{ and } P \text{-constant)} \\ \Delta \hat{E}_k = 0 \text{ (no change in } m \text{ and } u) \\ \hat{Q} = 0 \text{ (no } \Delta T \text{ between system and surroundings)} \\ \hline \Delta \hat{E}_p = -\hat{W}_s, \hat{W}_s > 0 \text{ (for water system)} \end{array}$$

(d) $\Delta \hat{H} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s$ (The system is the oil)

$$\begin{array}{l} \Delta \hat{E}_k = 0 \text{ (no velocity change)} \\ \hline \Delta \hat{H} + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s, \hat{Q} < 0 \text{ (friction loss); } \hat{W}_s < 0 \text{ (pump work).} \end{array}$$

(e) $\Delta \hat{H} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s$ (The system is the reaction mixture)

$$\begin{array}{l} \Delta \hat{E}_k = \Delta \hat{E}_p = 0 \text{ (given)} \\ \Delta \hat{W}_s = 0 \text{ (no moving parts or generated current)} \\ \hline \Delta \hat{H} = \hat{Q}, \hat{Q} \text{ pos. or neg. depends on reaction} \end{array}$$

$$7.21 \text{ (a) } \hat{H} = aT + b \quad \left. \begin{aligned} a &= \frac{\hat{H}_2 - \hat{H}_1}{T_2 - T_1} = \frac{129.8 - 25.8}{50 - 30} = 5.2 \\ b &= \hat{H}_1 - aT_1 = 25.8 - (5.2)(30) = -130.2 \end{aligned} \right\} \Rightarrow \underline{\hat{H}(\text{kJ/kg}) = 5.2T(^{\circ}\text{C}) - 130.2}$$

$$\hat{H} = 0 \Rightarrow T_{\text{ref}} = \frac{130.2}{5.2} = \underline{25^{\circ}\text{C}}$$

$$\text{Table B.1} \Rightarrow (S.G.)_{\text{C}_6\text{H}_{14}(\text{l})} = 0.659 \Rightarrow \hat{V} = \frac{1 \text{ m}^3}{659 \text{ kg}} = 1.52 \times 10^{-3} \text{ m}^3/\text{kg}$$

$$\hat{U}(\text{kJ/kg}) = \hat{H} - P\hat{V} = (5.2T - 130.2) \text{ kJ/kg}$$

$$\begin{array}{c|c|c|c|c|c} \frac{1 \text{ atm}}{1} & \frac{1.0132 \times 10^5 \text{ N/m}^2}{1} & \frac{1.52 \times 10^{-3} \text{ m}^3}{1} & \frac{1 \text{ J}}{1 \text{ N} \cdot \text{m}} & \frac{1 \text{ kJ}}{10^3 \text{ J}} & \\ \hline & \text{atm} & \text{kg} & & & \end{array}$$

$$\Rightarrow \underline{\hat{U}(\text{kJ/kg}) = 5.2T - 130.4}$$

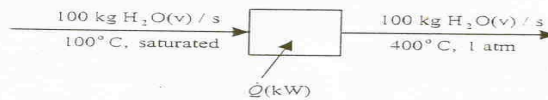
$$(b) \text{ Energy balance: } \frac{Q}{\Delta E_k, \Delta E_p, W=0} = \Delta U = \frac{20 \text{ kg}}{1} \left[\frac{[(5.2 \times 20 - 130.4) - (5.2 \times 30 - 130.4)] \text{ kJ}}{\text{kg}} \right] = -6240 \text{ kJ}$$

$$\underline{\text{Average rate of heat removal}} = \frac{6240 \text{ kJ}}{5 \text{ min}} \left| \frac{1 \text{ min}}{60 \text{ s}} \right| = \underline{20.8 \text{ kW}}$$

$$7.24 \text{ (a) } \Delta \hat{H} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}_s; \Delta \hat{E}_k, \Delta \hat{E}_p, \hat{W}_s = 0 \Rightarrow \Delta \hat{H} = \hat{Q}$$

$$\hat{H}(400^{\circ}\text{C}, 1 \text{ atm}) = 3278 \text{ kJ/kg (Table B.6)}$$

$$\hat{H}(100^{\circ}\text{C}, \text{sat'd} \Rightarrow 1 \text{ atm}) = 2676 \text{ kJ/kg (Table B.5)}$$



$$\hat{Q} = \frac{100 \text{ kg}}{\text{s}} \left| \frac{(3278 - 2676.0) \text{ kJ}}{\text{kg}} \right| \left| \frac{10^3 \text{ J}}{1 \text{ kJ}} \right| = \underline{6.02 \times 10^7 \text{ J/s}}$$

$$(b) \Delta U + \Delta E_k + \Delta E_p = Q - W; \Delta E_k, \Delta E_p, W = 0 \Rightarrow \Delta U = Q$$

$$\hat{U}(100^{\circ}\text{C}, 1 \text{ atm}) = 2507 \text{ kJ/kg} \quad \hat{U}(400^{\circ}\text{C}, 1 \text{ atm}) = 2968 \text{ kJ/kg (Tables B.5 & B.7)}$$

$$\Rightarrow Q = \Delta U = m\Delta \hat{U} = 100 \text{ kg} [(2968 - 2507) \text{ kJ/kg}] (10^3 \text{ J/kJ}) = \underline{4.61 \times 10^7 \text{ J}}$$

The difference is the net energy needed to move the fluid through the system (flow work).

CHE 203
HW # 2

7.31 Basis: 1 kg of 30°C stream



(a) $T_f = \frac{1}{3}(30^\circ\text{C}) + \frac{2}{3}(90^\circ\text{C}) = 70^\circ\text{C}$

(b) Internal Energy of feeds: $\hat{U}(30^\circ\text{C, liq.}) = 125.7 \text{ kJ/kg}$
 $\hat{U}(90^\circ\text{C, liq.}) = 376.9 \text{ kJ/kg}$

(Table B.5 - neglecting effect of P on \hat{H})

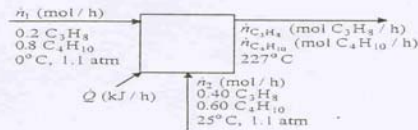
Energy Balance: $Q - W = \Delta U + \Delta E_p + \Delta E_k \xrightarrow{Q=W=\Delta E_p=\Delta E_k=0} \Delta U = 0$

$\Rightarrow 3\hat{U}_f - (1 \text{ kg})(125.7 \text{ kJ/kg}) - (2 \text{ kg})(376.9 \text{ kJ/kg}) = 0$

$\Rightarrow \hat{U}_f = 293.2 \text{ kJ/kg} \Rightarrow T_f = 70.05^\circ\text{C}$ (Table B.5)

Diff. = $\frac{70.05 - 70.00}{70.05} \times 100\% = 0.07\%$ (Any answer of this magnitude is acceptable).

7.40 Basis: Given feed rates



Molar flow rates of feed streams:

$\dot{n}_1 = \frac{300 \text{ L}}{\text{hr}} \left| \frac{1.1 \text{ atm}}{1 \text{ atm}} \right| \left| \frac{1 \text{ mol}}{22.4 \text{ L(STP)}} \right| = 14.7 \text{ mol/h}$

$\dot{n}_2 = \frac{200 \text{ L}}{\text{hr}} \left| \frac{273 \text{ K}}{298 \text{ K}} \right| \left| \frac{1.1 \text{ atm}}{1 \text{ atm}} \right| \left| \frac{1 \text{ mol}}{22.4 \text{ L(STP)}} \right| = 9.00 \text{ mol/h}$

Propane balance $\Rightarrow \dot{n}_{C_3H_8} = \frac{14.7 \text{ mol}}{\text{h}} \left| \frac{0.20 \text{ mol } C_3H_8}{\text{mol}} \right| + \frac{9.00 \text{ mol}}{\text{h}} \left| \frac{0.40 \text{ mol } C_3H_8}{\text{mol}} \right|$
 $= 6.54 \text{ mol } C_3H_8/\text{h}$

Total mole balance: $\dot{n}_{C_4H_{10}} = (14.7 + 9.00 - 6.54) \text{ mol } C_4H_{10}/\text{h} = 17.16 \text{ mol } C_4H_{10}/\text{h}$

Energy balance: $\Delta \hat{E}_p, \dot{W}_s = 0$, neglect $\Delta \hat{E}_k \Rightarrow \dot{Q} = \Delta \hat{H}$

$\dot{Q} = \Delta \hat{H} = \sum_{\text{out}} \dot{N}_i \hat{H}_i - \sum_{\text{in}} \dot{N}_i \hat{H}_i = \frac{6.54 \text{ mol } C_3H_8}{\text{h}} \left| \frac{20.685 \text{ kJ}}{\text{mol}} \right| + \frac{17.16 \text{ mol } C_4H_{10}}{\text{h}} \left| \frac{27.442 \text{ kJ}}{\text{mol}} \right|$
 $- \frac{(0.40 \times 9.00) \text{ mol } C_3H_8}{\text{h}} \left| \frac{1.772 \text{ kJ}}{\text{mol}} \right| - \frac{(0.60 \times 9.00) \text{ mol } C_4H_{10}}{\text{h}} \left| \frac{2.394 \text{ kJ}}{\text{mol}} \right| = 587 \text{ kJ/h}$

($\hat{H}_i = 0$ for components of 1st feed stream)

7.53 (a). $\dot{V}(\text{m}^3/\text{s}) = A_1(\text{m}^2)u_1(\text{m/s}) = A_2(\text{m}^2)u_2(\text{m/s}) \Rightarrow u_2 = u_1 \frac{A_1}{A_2} \xrightarrow{A_1=4A_2} \underline{u_2 = 4u_1}$

(b). Bernoulli equation ($\Delta z = 0$)

$$\frac{\Delta P}{\rho} + \frac{\Delta u^2}{2} = 0 \Rightarrow \Delta P = P_2 - P_1 = -\frac{\rho(u_2^2 - u_1^2)}{2}$$

↓ Multiply both sides by -1

Substitute $u_2^2 = 16u_1^2$

↓ Multiply top and bottom of right-hand side by A_1^2

note $\dot{V}^2 = A_1^2 u_1^2$

$$\underline{P_1 - P_2 = \frac{15\rho\dot{V}^2}{2A_1^2}}$$

(c) $P_1 - P_2 = (\rho_{\text{Hg}} - \rho_{\text{H}_2\text{O}})gh = \frac{15\rho_{\text{H}_2\text{O}}\dot{V}^2}{2A_1^2} \Rightarrow \dot{V}^2 = \frac{2A_1^2 gh}{15} \left(\frac{\rho_{\text{Hg}}}{\rho_{\text{H}_2\text{O}}} - 1 \right)$

$$\dot{V}^2 = \frac{2[\pi(7.5)^2]^2 \text{cm}^4}{15} \left| \frac{1}{10^8} \frac{\text{m}^4}{\text{cm}^4} \right| \left| \frac{9.8066 \text{ m}}{\text{s}^2} \right| \left| \frac{38 \text{ cm}}{10^2} \right| \left| \frac{1 \text{ m}}{10^2} \frac{\text{cm}}{\text{cm}} \right| (13.6 - 1) = 1.955 \times 10^{-3} \frac{\text{m}^6}{\text{s}^2}$$

$$\Rightarrow \dot{V} = 0.044 \text{ m}^3/\text{s} = \underline{44 \text{ L/s}}$$