



# CHE 402 Kinetics & Reactor Design

*Dr. Eid Al-Mutairi*

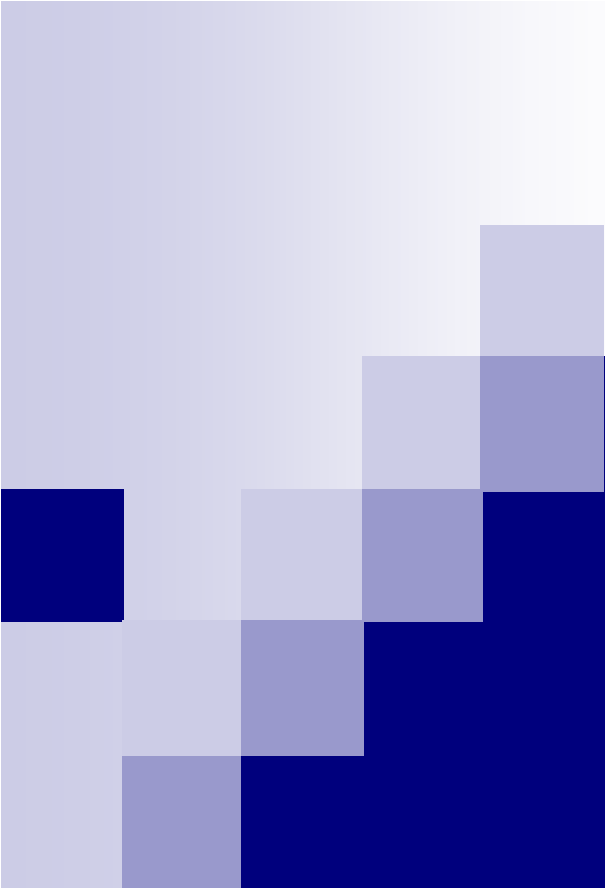
# Announcements

- **Quiz I**

**Oct. 29<sup>th</sup>**

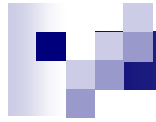
**Material: Chapters 1&2**

- **HW#2**



# Chapter 2: Conversion and Reactor Sizing

*Dr. Eid Al-Mutairi*



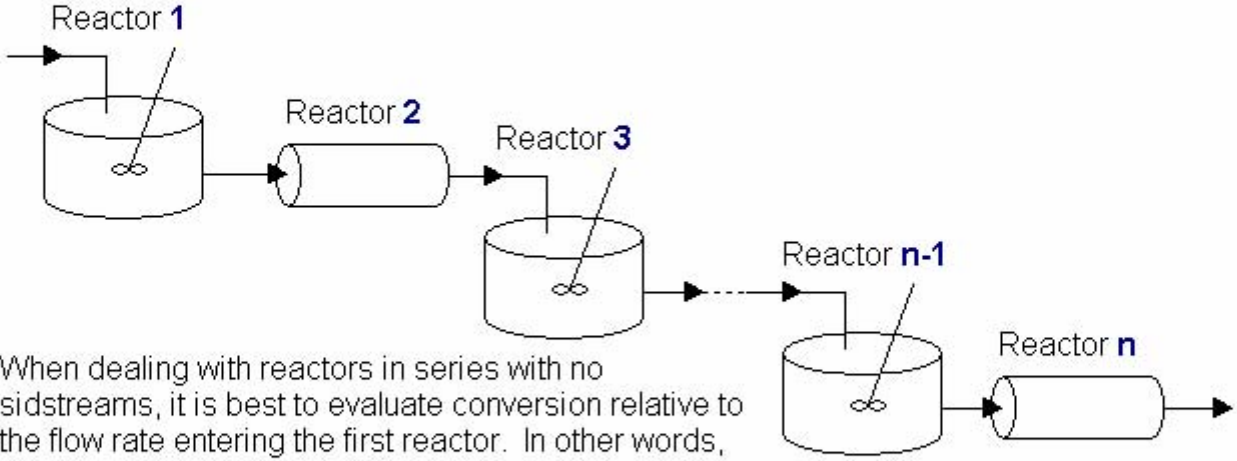
# ***Reactor Staging***

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### Reactor Staging

Many times, reactors are connected in series, so that the exit stream of one reactor is the feed stream of the next. One possible arrangement is shown below:



When dealing with reactors in series with no sidestreams, it is best to evaluate conversion relative to the flow rate entering the first reactor. In other words, the conversion at the  $n$ th reactor would be:

$$X_n = \frac{\text{total moles reacted up to point } n}{\text{moles of A fed to the first reactor}}$$

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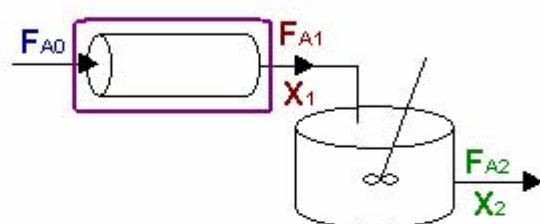
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## Staging

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The relationships between conversion and molar flow rates are:



Exiting the PFR:  
 $F_{A1} = F_{A0} - F_{A0}X_1$

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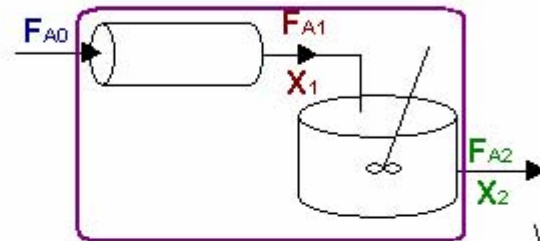
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# Staging

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The relationships between conversion and molar flow rates are:



Exiting the PFR:

$$F_{A1} = F_{A0} - F_{A0}X_1$$

Exiting the CSTR:

$$F_{A2} = F_{A0} - F_{A0}X_2$$

Where  $X_2 = \frac{\text{Total moles reacted up to point 2}}{\text{moles of A fed to the first reactor}}$

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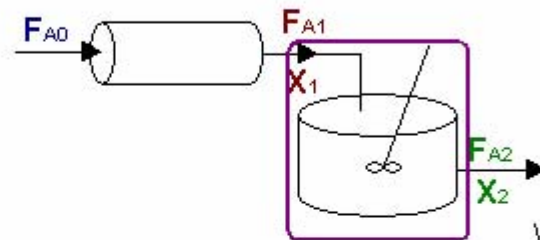
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The relationships between conversion and molar flow rates are:



Exiting the PFR:

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Exiting the CSTR:

$$F_{A2} = F_{A0} - F_{A0}X_2$$

Where  $X_2 = \frac{\text{Total moles reacted up to point 2}}{\text{moles of A fed to the first reactor}}$

A mole balance on the CSTR gives:

$$\text{in} - \text{out} + \text{generation} = 0$$

$$F_{A1} - F_{A2} + V_2 r_{A|2} = 0$$

Remember:

The reaction rate inside a CSTR is constant, and hence the reaction rate at the exit of the reactor is the same as the reaction rate inside the reactor.

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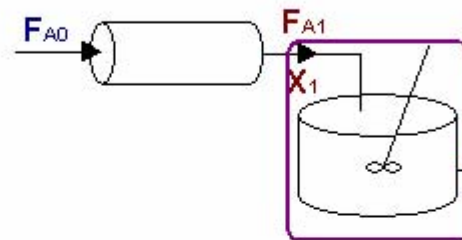


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Where  $X_2 = \frac{\text{Total moles reacted up to point 2}}{\text{moles of A fed to the first reactor}}$

A mole balance on the CSTR gives:

$$F_{A1} - F_{A2} + V_2 r_{A2} = 0$$

$$V_2 = \frac{F_{A1} - F_{A2}}{-r_{A2}}$$

Now substituting for  $F_{A1}$  and  $F_{A2}$ .

Remember:

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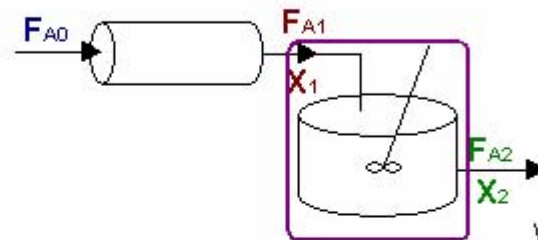
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A mole balance on the CSTR gives:

$$F_{A1} - F_{A2} + V_2 r_{A|2} = 0$$

$$V_2 = \frac{F_{A0} - F_{A0}X_1 - (F_{A0} - F_{A0}X_2)}{-r_{A|2}}$$

Rearranging...

Remember:

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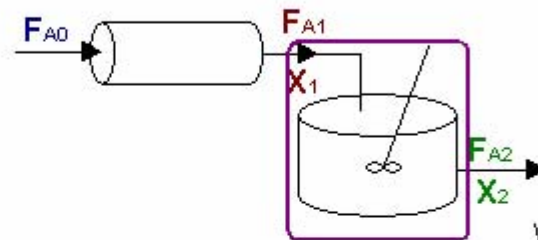
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Where  $X_2 = \frac{\text{Total moles reacted up to point 2}}{\text{moles of A fed to the first reactor}}$

A mole balance on the CSTR gives:

$$F_{A1} - F_{A2} + V_2 r_{A|2} = 0$$

$$V_2 = \frac{\cancel{F_{A0}} - F_{A0}X_1 - \cancel{F_{A0}} + F_{A0}X_2}{-r_{A|2}}$$

Then  
eliminating

Remember:

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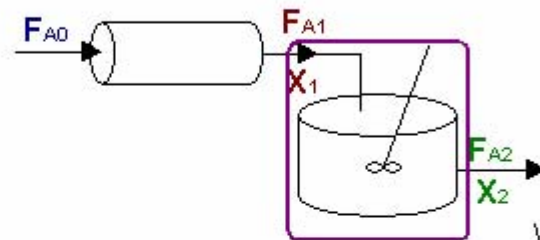
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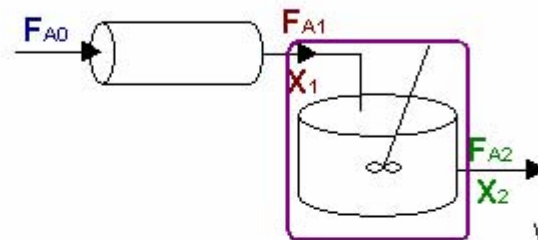
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A mole balance on the CSTR gives:

$$F_{A1} - F_{A2} + V_2 r_{A|2} = 0$$

$$V_2 = \frac{F_{A0}(X_2 - X_1)}{-r_{A|2}}$$

Design Equation  
CSTR in Series

Remember:

The reaction rate inside a CSTR is constant, and hence the reaction rate at the exit of the reactor is the same as the reaction rate inside the reactor.

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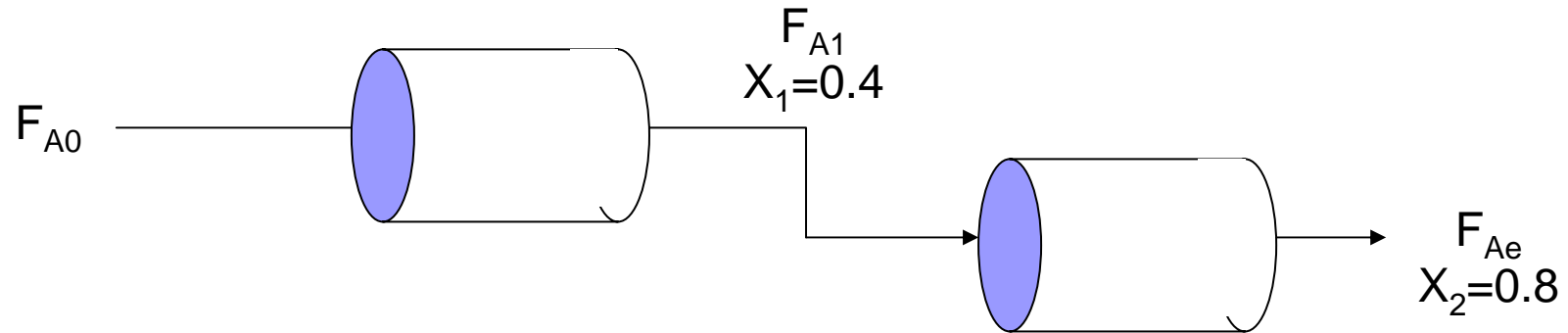
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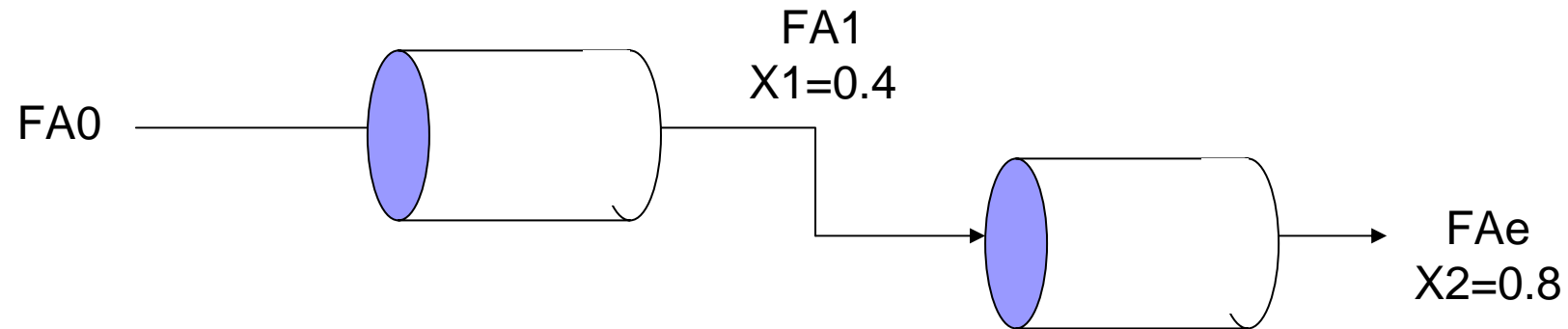


# Example 2-5

# PFRs in series



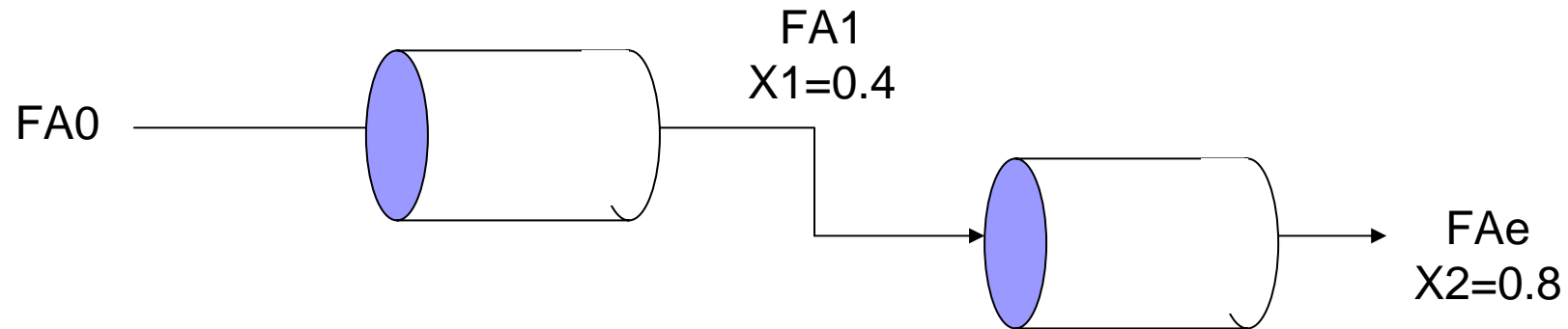
# PFRs in series



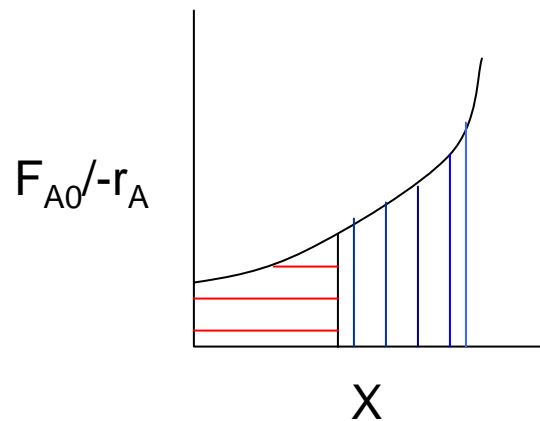
$$\int_0^{x_2} F_{A_0} \frac{dX}{-r_A} = \int_0^{x_1} F_{A_0} \frac{dX}{-r_A} + \int_{x_1}^{x_2} F_{A_0} \frac{dX}{-r_A}$$



# PFRs in series



$$\int_0^{x_2} F_{A_0} \frac{dX}{-r_A} = \int_0^{x_1} F_{A_0} \frac{dX}{-r_A} + \int_{x_1}^{x_2} F_{A_0} \frac{dX}{-r_A}$$





# Example 2-6

# PFRs, CSTRs reactor volumes and sequencing

## **Space time**

*time necessary to process one reactor volume of fluid based on entrance conditions*

$$\tau = \frac{V}{v_0}$$

## **Space velocity**

**- LHSV**

**- GHSV**

$$SV = \frac{v_0}{V} = \frac{1}{\tau}$$

**Typical Space time for Industrial Reactors**

Reactor Type	Mean Residence Time Range	Production Capacity
Batch	15 min – 20 h	Few kg/h to 100,000 tons/yr
CSTR	10 min-4h	10 - 3M tons/yr
Tubular	0.5 s-1 h	50- 5M tons/yr