

First-Order System

The standard form for a first-order TF is:

$$\frac{Y(s)}{U(s)} = \frac{K}{\tau s + 1} \quad (5-16)$$

where:

K □ steady-state gain

τ □ time constant

Consider the response of this system to a step of magnitude, M :

$$U(t) = M \text{ for } t \geq 0 \quad \Rightarrow \quad U(s) = \frac{M}{s}$$

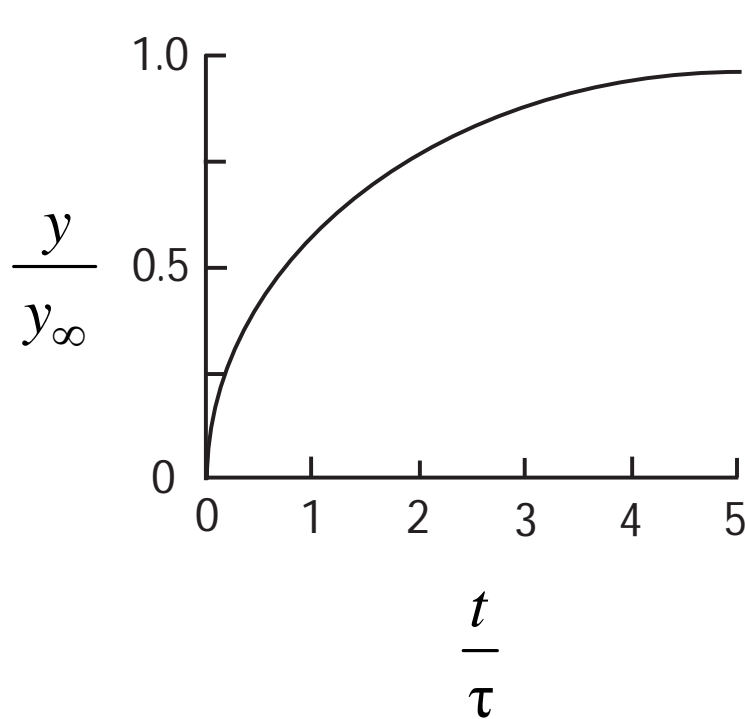
Substitute into (5-16) and rearrange,

$$Y(s) = \frac{KM}{s(\tau s + 1)} \quad (5-17)$$

Take L^{-1} (cf. Table 3.1),

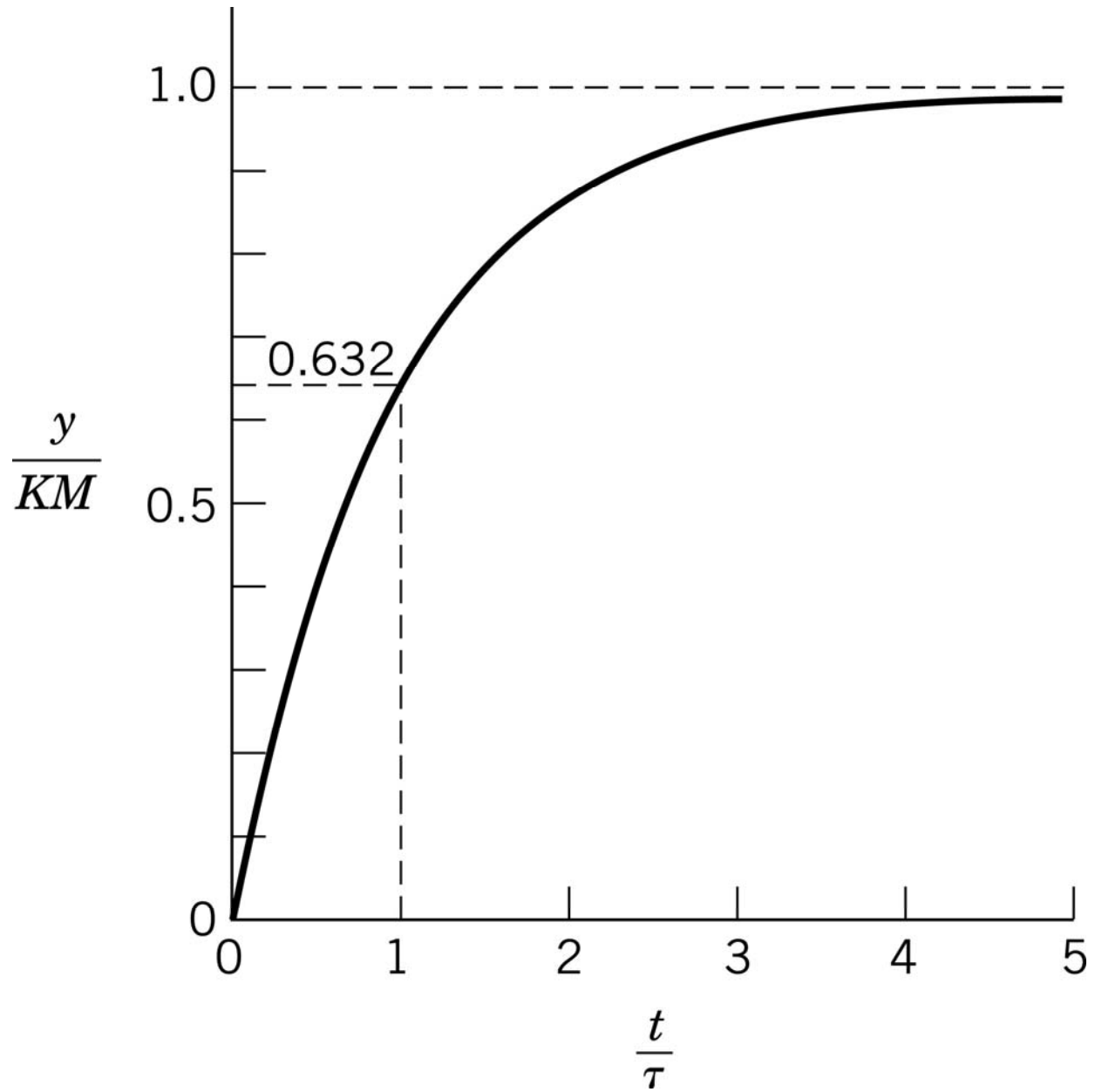
$$\boxed{y(t) = KM \left(1 - e^{-t/\tau}\right)} \quad (5-18)$$

Let y_∞ \square steady-state value of $y(t)$. From (5-18), $y_\infty = KM$.



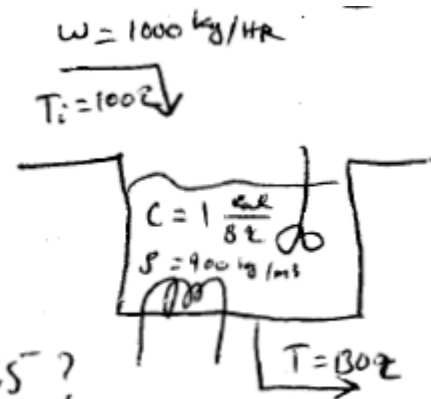
$\frac{t}{\tau}$	$\frac{y}{y_\infty}$
0	0
τ	0.632
2τ	0.865
3τ	0.950
4τ	0.982
5τ	0.993

Note: Large τ means a slow response.



Ex

- ① Steady state \dot{Q} ?
- ② +30% of \dot{Q} , how long to get to SS?
- ③ +20°C of T_i ; how long for T to reach 135°?



$$\textcircled{1} \quad \bar{Q} = \bar{W} C (\bar{T} - \bar{T}_i) = 3 \times 10^7 \frac{\text{cal}}{\text{hr}}$$

$$\textcircled{2} \quad K = \frac{1}{WC} = 10^{-6} \frac{\text{hr}}{\text{deg C}} \quad \tau = \frac{V\rho}{W} = 1.8 \text{ hr}$$

to reach SS it takes $5\tau = 9 \text{ hr}$

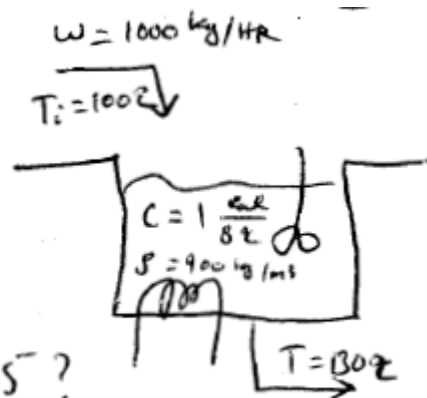
$$\text{also, F.V.T.} \quad \lim_{s \rightarrow 0} s \frac{K}{\tau s + 1} \frac{0.3 \bar{Q}}{s} = 9^\circ \text{C}$$

$$\Rightarrow \text{final } T = 130 + 9 = 139^\circ \text{C} \quad \text{after } +30\% \dot{W}$$

Or by looking into gain: $+30\% \dot{W} \rightarrow +0.3 \bar{Q} \text{ K in out}$

Ex

- ① Steady state Q ?
- ② +30% of Q , how long to get to SS?
- ③ +20°C of T_i ; how long for T to reach 135°?



③ by looking to gain: final T is 150

$$\Rightarrow \frac{135 - 130}{150 - 130} = \frac{5}{20} = 25\%$$

from fig 5.4 $\Rightarrow \frac{t}{\tau} = 0.3 \Rightarrow t = 0.54 \text{ hr}$

OR $\frac{y(t)}{KM} = 1 - e^{-t/\tau} \Rightarrow \frac{5}{(1)(20)} = 1 - e^{-t/1.8}$

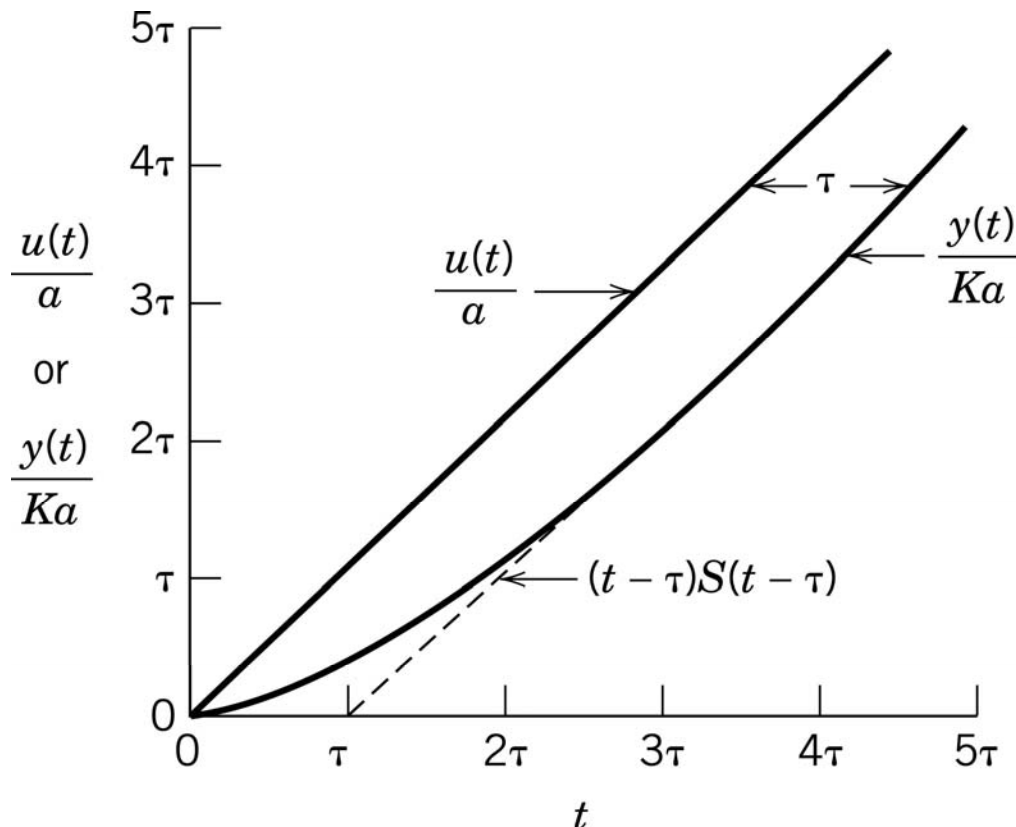
$$\Rightarrow t = 0.52 \text{ hr}$$

-Ramp $U(s) = \frac{K}{Ts+1} \frac{1}{s^2} = \frac{\alpha_1}{Ts+1} + \frac{\alpha_2}{s} + \frac{\alpha_3}{s^2}$

$$= \frac{KaT^2}{Ts+1} + \frac{KaT}{s} + \frac{Ka}{s^2}$$

$$\mathcal{L}^{-1} \Rightarrow y(t) = KaT(e^{-t/T} - 1) + Kat$$


@ $t \gg T$ $y(t) = Ka(t - T)$



- Sinusoidal Response: $Y(s) = \frac{K}{\tau s + 1} \frac{A\omega}{s^2 + \omega^2}$

$$Y(s) = \frac{KA}{\omega^2\tau^2 + 1} \left(\frac{\omega\tau^2}{\tau s + 1} + \frac{s\omega\tau}{s^2 + \omega^2} + \frac{\omega}{s^2 + \omega^2} \right)$$

$$\xrightarrow{\mathcal{L}^{-1}} y(t) = \frac{KA}{\omega^2\tau^2 + 1} \left(\omega\tau e^{-t/\tau} - \omega\tau \cos \omega t + \sin \omega t \right)$$

- fluctuation of flow around a value. 

For a sine input (1st order process)

$$U(s) = \frac{\omega}{s^2 + \omega^2}$$

output is...

$$Y(s) = \frac{K_p}{\tau s + 1} \cdot \frac{\omega}{s^2 + \omega^2} = \frac{\alpha_0}{\tau s + 1} + \frac{\alpha_1 s}{s^2 + \omega^2} + \frac{\alpha_2}{s^2 + \omega^2}$$

By partial fraction decomposition,

$$\alpha_0 = \frac{\omega K_p \tau^2}{\omega^2 \tau^2 + 1}$$

$$\alpha_1 = \frac{-\omega K_p \tau}{\omega^2 \tau^2 + 1}$$

$$\alpha_2 = \frac{\omega K_p}{\omega^2 \tau^2 + 1}$$

Inverting,

this term dies out for large t

$$y(t) = \frac{K_p \omega \tau}{\omega^2 \tau^2 + 1} e^{-t/\tau} + \frac{K_p}{\sqrt{\omega^2 \tau^2 + 1}} \sin(\omega t + \phi)$$

$$\phi = -\arctan(\omega \tau)$$

note: ϕ is not a function of t but of τ and ω .

For large t, $y(t)$ is also sinusoidal,
output sine is attenuated by...

$$\frac{1}{\sqrt{\omega^2 \tau^2 + 1}} \quad (\text{fast vs. slow } \omega)$$

Integrating Process

Not all processes have a steady-state gain. For example, an “integrating process” or “integrator” has the transfer function:

$$\frac{Y(s)}{U(s)} = \frac{K}{s} \quad (K = \text{constant})$$

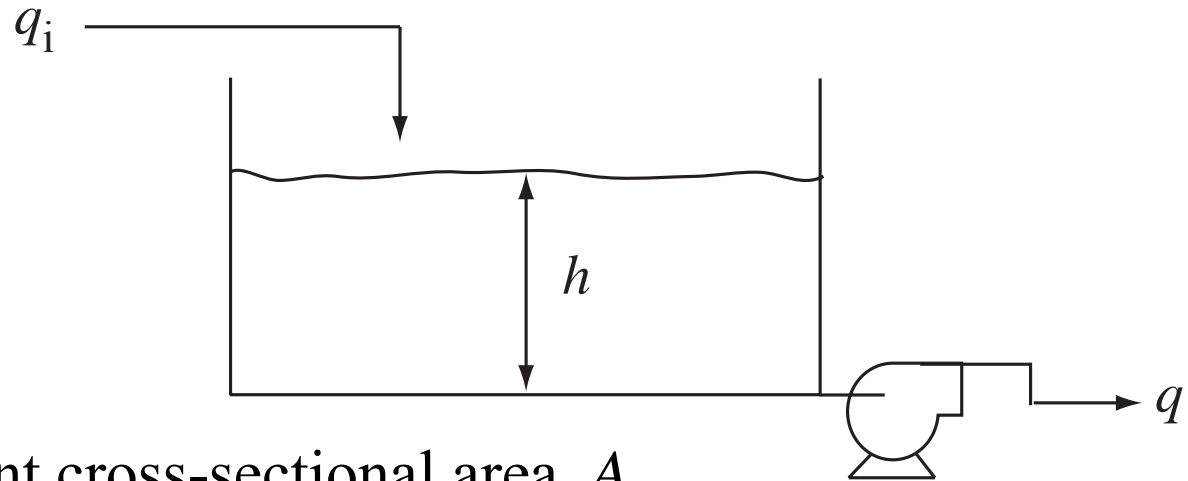
Consider a step change of magnitude M . Then $U(s) = M/s$ and,

$$Y(s) = \frac{KM}{s^2} \stackrel{\mathcal{L}^{-1}}{\Rightarrow} y(t) = KMt$$

Thus, $y(t)$ is unbounded and a new steady-state value does *not* exist.

Common Physical Example:

Consider a liquid storage tank with a pump on the exit line:



- Assume:

1. Constant cross-sectional area, A .

2. $q \neq f(h)$

- Mass balance: $A \frac{dh}{dt} = q_i - q$ (1) $\Rightarrow 0 = \bar{q}_i - \bar{q}$ (2)

- Eq. (1) – Eq. (2), take L , assume steady state initially,

$$H'(s) = \frac{1}{As} [Q'_i(s) - Q'(s)]$$

- For $Q'(s) = 0$ (constant q),

$$\boxed{\frac{H'(s)}{Q'_i(s)} = \frac{1}{As}}$$