CIVIL ENGINEERING DEPARTEMNT - KFUPM CE 202 Statics and Strength of Materials

First Semester: '101 Instructor: Dr. Salah Al-Dulaijan

HOME WORK ASSIGNMENT NO. 10.

- Subject material covered: Flexural Formula, shear formula, and combined loadings
- DUE DATE: Wednesday, January 19th, 2011.
 - **1.** If the beam has a square cross-section of 9 in. on each side, determine the absolute maximum bending stress in the beam.





Absolute Maximum bending Stress: The maximum moment is $M_{max} = 44.8$ kip.ft as indicated on the bending moment diagram. Applying the flexural formula

$$\sigma_{max} = \frac{M_{max}c}{I} = \frac{44.8 \times 12 \times 4.5}{1/12 \times 9 \times 9^3} = 4.42 \, ksi$$

2. The rod is supported by smooth journal bearings at A and B that only exert vertical reactions on the shaft. Determine its smallest diameter d if the allowable bending stress is $\sigma_{allow} = 180$ MPa.



Mmax = 8.37 KNm @1.38m

$$\sigma_{allow} = \frac{M_{max}c}{I} \quad ; \quad c = r_{min} = \frac{\sigma_{allow}\pi r^4}{4M_{max}} \quad , \quad or \quad r_{min} = \left(\frac{4M_{max}}{\pi\sigma_{allow}}\right)^{\frac{1}{3}}$$

$$d_{min} = 2r_{min} = 2\left(\frac{4 \times 8.37 \times 10^3}{\pi \times 180 \times 10^6}\right)^{\frac{1}{3}} = 2 \times 0.03898 \, m \approx 78 \, mm$$

3. The T-beam is subjected to the loading shown. Determine the maximum transverse shear stress in the beam at the critical section.



Internal Shear Force: As shown on Shear diagram, $V_{\text{max}} = 24.57 \text{ kN}.$

Section Properties:

$$\bar{y} = \frac{\Sigma \ \bar{y}A}{\Sigma A} = \frac{0.01(0.1)(0.02) + 0.07 \ (0.1)(0.02)}{0.1(0.02) + 0.1(0.02)}$$

= 0.0400 m
$$I_{NA} = \frac{1}{12}(0.1) \left(0.02^{3} \right) + 0.1(0.02) \left(0.0400 - 0.01 \right)^{2}$$

$$+ \frac{1}{12}(0.02) \left(0.1^{3} \right) + (0.02)(0.1) \left(0.07 - 0.0400 \right)^{2}$$

= 5.3333 (10⁻⁶) m⁴

$$Q_{\text{max}} = \bar{y}'A' = 0.04(0.02)(0.08) = 64.0(10^{-6}) \text{ m}^3$$

Maximum Shear Stress: Maximum shear stress occurs at the point where the neutral axis passes through the section. Applying the shear formula

$$\tau_{\max} = \frac{VQ_{\max}}{It}$$
$$= \frac{24.57(10^3)\,64.0(10^{-6})}{5.3333(10^{-6})(0.02)} = 14.7 \text{ MPa}$$



0.02 m

4. The beam is made from three plastic pieces glued together at the seams A and B. If it is subjected to the loading shown, determine the shear stress developed in the glued joints at the critical section. The supports at C and D exert only vertical reactions on the beam.



Support Reactions: As shown on FBD.

Internal Shear Force: As shown on shear diagram, $V_{max} = 800$ lb.

Section Properties:

$$I_{NA} = \frac{1}{12}(8)(12^3) - \frac{1}{12}(6)(8^3) = 896 \text{ in}^4$$
$$Q_A = \bar{y}'A' = 5(8)(2) = 80.0 \text{ in}^3$$

Shear Stress: Applying the shear formula

$$\tau_A = \frac{VQ_A}{It} = \frac{800(80.0)}{896(2)} = 35.7 \text{ psi}$$

5. The bar has a diameter of 40 mm. If it is subjected to a force of 800 N as shown, determine the stress components that act at points A and B.

$$I = \frac{1}{4} \pi r^{4} = \frac{1}{4} (\pi)(0.02^{4}) = 0.1256637 (10^{5}) \text{ m}^{4}$$

$$A = \pi r^{2} = \pi (0.02^{2}) = 1.256637 (10^{3}) \text{ m}^{2}$$

$$Q_{A} = \bar{y}' A = (\frac{4 (0.02)}{3\pi})(\frac{\pi (0.02)^{2}}{2}) = 5.3333 (10^{6}) \text{ m}^{3}$$

$$\sigma_{A} = \frac{P}{A} + \frac{Mz}{1}$$

$$= \frac{400}{1.256637 (10^{3})} + 0 = 0.318 \text{ MPa}$$

$$\tau_{A} = \frac{VQ_{A}}{I_{I}} = \frac{692.82 (5.3333) (10^{6})}{0.1256637 (10^{6}) (0.04)} = 0.735 \text{ MPa}$$

$$I = \frac{1}{4} \pi r^{4} = \frac{1}{4} (\pi)(0.02^{4}) = 0.1256637 (10^{-6}) \text{ m}^{4}$$

$$A = \pi r^{2} = \pi (0.02^{2}) = 1.256637 (10^{-3}) \text{ m}^{2}$$

$$Q_{B} = 0 \quad ; \ \tau_{B} = 0$$

$$\sigma_{B} = \frac{P}{A} - \frac{Mc}{I} = \frac{400}{1.256637 (10^{-3})} - \frac{138.56 (0.02)}{0.1256637 (10^{-6})}$$

$$= -21.7 \text{ MPa}$$

6. The frame supports a centrally applied distributed load of 1.8 kip/ft. Determine state of stress developed at points A and B on member CD. The pins at C and D are at the same location as the neutral axis for the cross-section.



Part	Ai	y i	A _i y _i	A _i (y _i - <u>y</u> i)^2	l _{xi}
1	10.5	0.75	7.875	19.5247934	1.96875
2	6	4.5	27	34.1683884	18
Σ	16.5 in ²		34.875	53.6931818	19.96875

 \underline{y} = 2.113636in I_x = 73.66 in⁴

Neutral axis = 2.11 in from the top (A)

So $y_A=2.11$ in and $y_B = (6+1.5-2.11) = 5.39$ in

The stresses at any section of member CD consist of tensile stress (σ^a) from the truss action and bending stresses (σ^b) from the bending action, both resulting from the distributed load on this member.

Points A and B are both at points where Q = 0, so $\tau_A = \tau_B = VQ/It = 0$

Bending Stresses, σ^b : $R_C = R_C = 1.8 \times 16 \times 0.5 = 14.4$ Kips

 $M_{A-B} = 14.4 \times 5 - 1.8 \times 5 \times 2.5 = 49.5 Kip - ft$

Top fibres of member CD are in compression $(so, \sigma_A^b = -ve)$, while the bottom fibres of are in tension $(so, \sigma_A^b = -ve)$.

$$\sigma_A^b = -\frac{My_A}{I} = -\frac{49.5 \times 12 \times 2.11}{73.66} = -17.0152 \text{ Ksi},$$
$$\sigma_B^b = +\frac{My_B}{I} = \frac{49.5 \times 12 \times 5.39}{73.66} = +43.4654 \text{ Ksi}$$

Axial Stresses, σ^a :

Let $\langle CDE = \beta$, then Sin $\beta = 0.6$ and Cos $\beta = 0.8$ Equilibrium of joint D gives

$$F_{DE} = \frac{R_D}{\sin\beta} = \frac{14.4}{0.6} = 24 \text{ Kips}, \quad \text{and}$$

$$F_{CD} = F_{DE} \cos\beta = 24 \times 0.6 = 19.2 \text{ Kips}.$$

$$\sigma_A^a = \sigma_B^a = \sigma^a = \frac{F_{CD}}{A_{CD}} = \frac{19.2 \text{ Kips}}{16.5 \text{ in}^2} = +1.1636 \text{ Ksi (tension)}$$

$$\sigma_A = \sigma_A^b + \sigma_A^a = -17.0152 + 1.1636 = -15.8516 \text{ Ksi} \approx -15.85 \text{ Ksi}$$

$$\sigma_B = \sigma_B^b + \sigma_B^a = 43.4654 + 1.1636 = +44.629 \text{ Ksi} \approx +44.63 \text{ Ksi}$$

Therefore The states of stress

at A, $(\sigma_A, \tau_A) = (-15.85 \text{ Ksi}, 0.00 \text{ Ksi})$, and at B, $(\sigma_B, \tau_B) = (+44.63 \text{ Ksi}, 0.00 \text{ Ksi})$

Sketch each one on an element