

Transformation of Stress

Theory & Examples

* **Triaxial** states of stress are shown in Fig. (1).

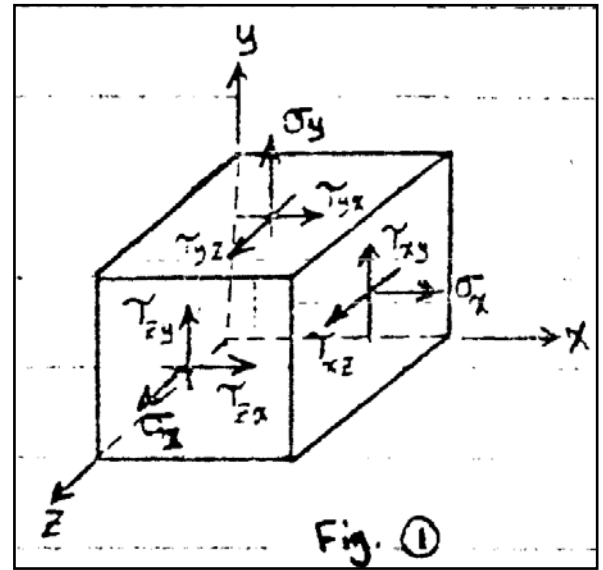
Only positive stresses on positive faces are shown

* **Biaxial** states of stress (Plane Stress):

When all stresses act in the same plane.

⇒ Work in 2-D as shown in Fig. (2) in the

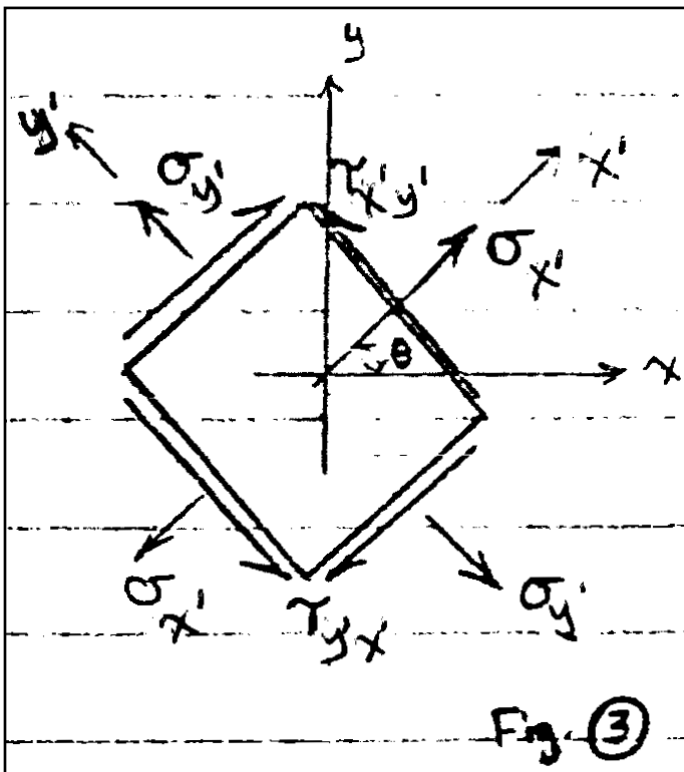
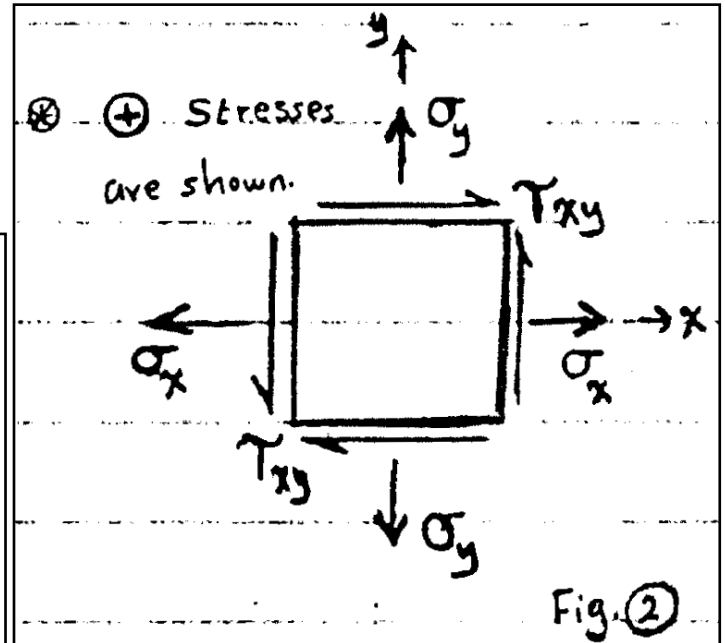
x-y directions.



It is possible to have the orientation in different

directions, as shown in Fig. (3) in the x'-y' directions.

Now, relationships between the stresses in the x-y and x'-y' directions are sought.



From Fig. (4), the sum of **forces** in the x' and y' directions must be zero.

* *Note that forces not stresses are added.*

(2 eqs. & 2 unks.)

$$\sum F_{x'} = 0 \text{ \& } \sum F_{y'} = 0 \quad \Rightarrow$$

$$\sigma_{x'} = \sigma_x \cos^2 \theta + \sigma_y \sin^2 \theta + 2 \tau_{xy} \sin \theta \cos \theta$$

$$\tau_{x'y'} = -(\sigma_x - \sigma_y) \sin \theta \cos \theta + \tau_{xy} (\cos^2 \theta - \sin^2 \theta)$$

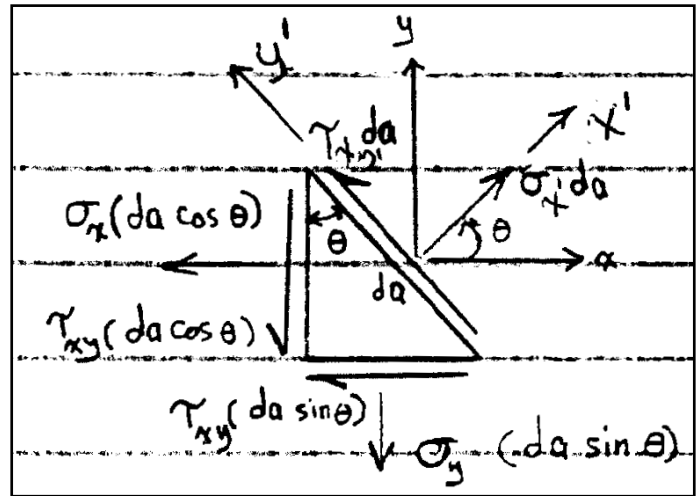


Fig. (4)

Recall that

$$\cos^2 \theta = (1 + \cos 2\theta)/2$$

$$\sin^2 \theta = (1 - \cos 2\theta)/2$$

$$\sin \theta \cos \theta = \sin 2\theta/2$$

$$\cos^2 \theta - \sin^2 \theta = \cos 2\theta$$

\Rightarrow

$$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta \quad [1]$$

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \quad [2]$$

Similarly,

$$\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta \quad [3]$$

$$\tau_{y'x'} = \tau_{x'y'} \quad [4]$$

* *Note that $\sigma_x + \sigma_y = \sigma_{x'} + \sigma_{y'} = I$ (Invariant with any θ)* \Leftarrow Use it to check.

When σ & τ on any two orthogonal faces are known, the stress components on all (any) faces (plane stress) can be calculated.

Principal Normal Stresses:

$\sigma_{x'} = f(\theta) \Rightarrow$ to get $\sigma_{x'_{max}}$, set $\frac{d\sigma_{x'}}{d\theta} = 0 \Rightarrow$ find $\theta_p \Rightarrow \sigma_{x'_{max}}$

$$\frac{d\sigma_{x'}}{d\theta} = -(\sigma_x - \sigma_y) \sin 2\theta_p + 2\tau_{xy} \cos 2\theta_p = 0$$

Dividing by $\cos 2\theta$,
$$\tan 2\theta_p = \frac{2\tau_{xy}}{\sigma_x - \sigma_y} = \frac{\tau_{xy}}{(\sigma_x - \sigma_y)/2} \quad [5]$$

From the equation above, Fig. (5) shown can be constructed.

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \quad [6]$$

$$\sin 2\theta_{p1} = \frac{\tau_{xy}}{R}$$

$$\cos 2\theta_{p1} = \frac{(\sigma_x - \sigma_y)/2}{R}$$

$$\sin 2\theta_{p2} = \frac{-\tau_{xy}}{R} \quad ; \quad \cos 2\theta_{p2} = \frac{-(\sigma_x - \sigma_y)/2}{R}$$

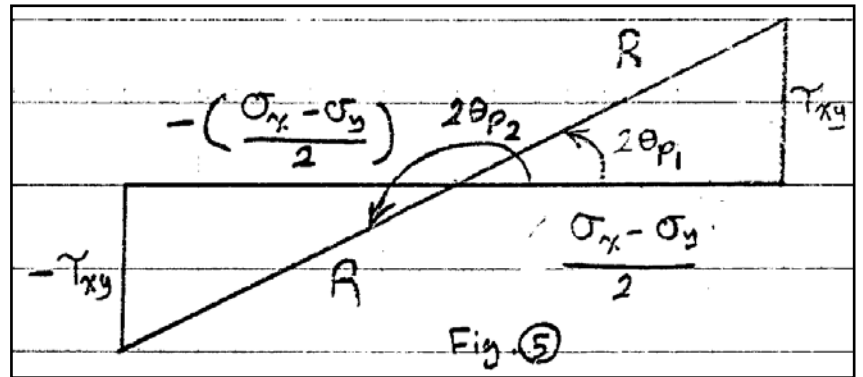
$$\Rightarrow \sigma_{\max/\min} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = \frac{\sigma_x + \sigma_y}{2} \pm R \quad [7]$$

↑ Principal Normal Stresses

The directions are given by θ_{p1} and θ_{p2}

Note that $2\theta_{p2} = 2\theta_{p1} + \pi \Rightarrow \theta_{p1} \perp \theta_{p2}$

Also note that $\tau_{x'y'} = 0$ on the planes which the principal normal stresses act.



maximum Shear Stresses: \Leftarrow sometimes called **principal τ**

$\tau_{x'y'} = f(\theta) \Rightarrow$ The value of θ_s can be obtained by setting $\frac{d\tau_{x'y'}}{d\theta} = 0$.

$$\Rightarrow \tan 2\theta_s = \frac{-\left(\frac{\sigma_x - \sigma_y}{2}\right)}{\tau_{xy}} \quad [8]$$

[Fig. (6)]

There are 2 possible values for θ_s

$$\Rightarrow \sin 2\theta_{s1} = \frac{(\sigma_x - \sigma_y) / 2}{R}$$

$$\cos 2\theta_{s1} = \frac{-\tau_{xy}}{R}$$

$$\sin 2\theta_{s2} = \frac{-(\sigma_x - \sigma_y) / 2}{R} \quad ; \quad \cos 2\theta_{s2} = \frac{\tau_{xy}}{R}$$

$$\Rightarrow \tau_{\max/\min} = \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = \pm R \quad [9]$$

\uparrow **Maximum (Principal) Shear Stresses**

$$\sigma_{x'} = \sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} \quad [10]$$

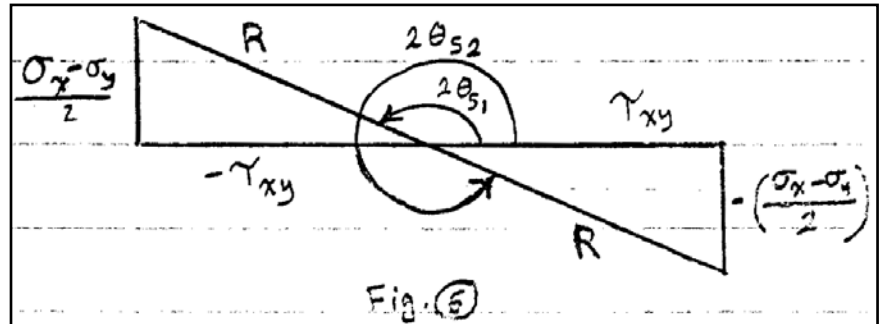
\uparrow *Normal Stresses on the Planes of Maximum (Principal) Shear Stresses*

Note that $2\theta_{s2} = 2\theta_{s1} + \pi \Rightarrow \theta_{s1} \perp \theta_{s2}$

Also note that $\tan 2\theta_p$ is the negative reciprocal of $\tan 2\theta_s$: $\tan 2\theta_p = -1/\tan 2\theta_s$

$$\Rightarrow 2\theta_s = 2\theta_p + \pi/2 \Rightarrow \theta_s = \theta_p + 45^\circ \quad [11]$$

Thus, there is a 45° -angle between the planes of principal normal and maximum shear stresses.



Example 1:**Given:**

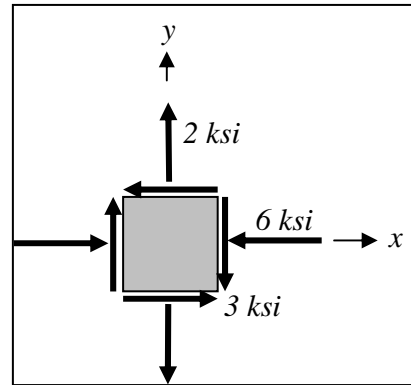
The state of stress shown

Req'd:

- The principal stresses & directions
- σ & τ associated with an element oriented 10° cw of the element shown.

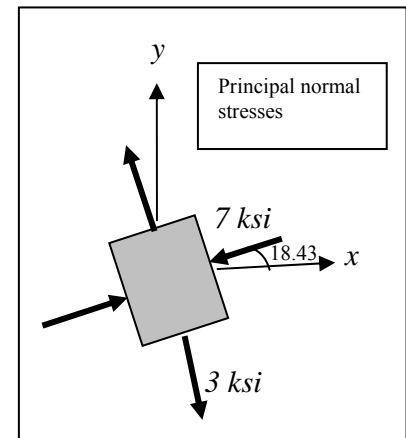
Show the results on properly oriented elements.

Use the equations for the solution.

**Solution:**

$$\begin{aligned} \sigma_{\max/\min} &= \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \\ \text{a)} \quad &= \frac{-6 + 2}{2} \pm \sqrt{\left(\frac{-6 - 2}{2}\right)^2 + (-3)^2} = -2 \pm 5 \end{aligned}$$

$$\Rightarrow \sigma_{\max} = 3 \text{ ksi} \quad ; \quad \sigma_{\min} = -7 \text{ ksi}$$



$$\tan 2\theta_p = \frac{2\tau_{xy}}{\sigma_x - \sigma_y} = \frac{2(-3)}{-6 - 2} = 0.75 \Rightarrow 2\theta_{p1} = 36.87^\circ, \quad 2\theta_{p2} = 216.87^\circ \quad (-143.13^\circ)$$

$$\Rightarrow \theta_{p1} = 18.43^\circ \quad ; \quad \theta_{p2} = 108.43^\circ \quad (-71.57^\circ)$$

To see θ_{p1} corresponds to σ_{\max} or σ_{\min} , substitute θ in Eq. [1] by $\theta_{p1} = 18.4349^\circ$

$$\Rightarrow \sigma_{x'} = \frac{-6 + 2}{2} + \frac{-6 - 2}{2} \cos 36.87^\circ - 3 \sin 36.87^\circ = -7 \text{ ksi}$$

$\Rightarrow \theta_{p1}$ is the direction of σ_{\min} as shown.

$$\tau_{\max/\min} = \pm R \Rightarrow \tau_{\max} = 5 \text{ ksi} \quad ; \quad \tau_{\min} = -5 \text{ ksi}$$

$$\sigma_{x'} = \sigma_{y'} = \frac{-6 + 2}{2} = -2 \text{ ksi}$$

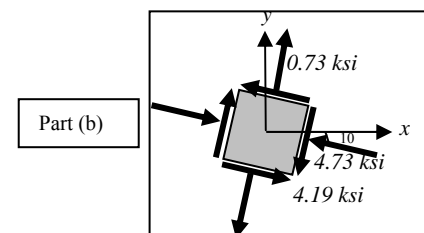
$$\tan 2\theta_s = -1/0.75 \Rightarrow \theta_{s1} = -26.57^\circ \quad ; \quad \theta_{s2} = 63.43^\circ \quad ; \quad \tau(-26.57^\circ) = -5 \text{ ksi} = \tau_{\min} \leftrightarrow \theta_{s1}$$

$$\text{b) From Eqs. [1] to [4],} \quad \sigma_{x'}(-10^\circ) = -4.73 \text{ ksi} \quad ;$$

$$\sigma_{y'}(-10^\circ) = 0.73 \text{ ksi}$$

Note that $\sum \sigma_i = -4$ (always)

$$\tau_{x'y'}(-10^\circ) = \tau_{y'x'}(-10^\circ) = -4.19 \text{ ksi} \quad (\pm)$$



Mohr's Circle:

The general equation of the circle is

$$(x-a)^2 + (y-b)^2 = R^2 \quad [12]$$

By rearranging equation [1] and squaring both sides of equations [1] & [2], and then adding, the following equation is obtained:

$$\left(\sigma_{x'} - \frac{\sigma_x + \sigma_y}{2} \right)^2 + \tau_{x'y'}^2 = \left(\frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2 \quad [13]$$

By comparing eq. [13] with eq. [12], it can be seen that

$$x = \sigma_{x'}$$

$$a = (\sigma_x + \sigma_y)/2 = \sigma_{average}$$

$$y = \tau_{x'y'}$$

$$b = 0$$

$$R^2 = \left(\frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2$$

Thus, by constructing a circle with the properties above, and by referring to Fig. (5), the values of $\sigma_{x'}$, $\sigma_{y'}$, and $\tau_{x'y'}$ with any θ can be found; this includes the principal stresses and their directions. This circle is called Mohr's Circle because Mohr brought the idea of such a circle. It has several applications, other than stresses.

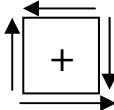
Steps for constructing Mohr's circle and determining the principal stresses & directions and σ & τ with any θ :

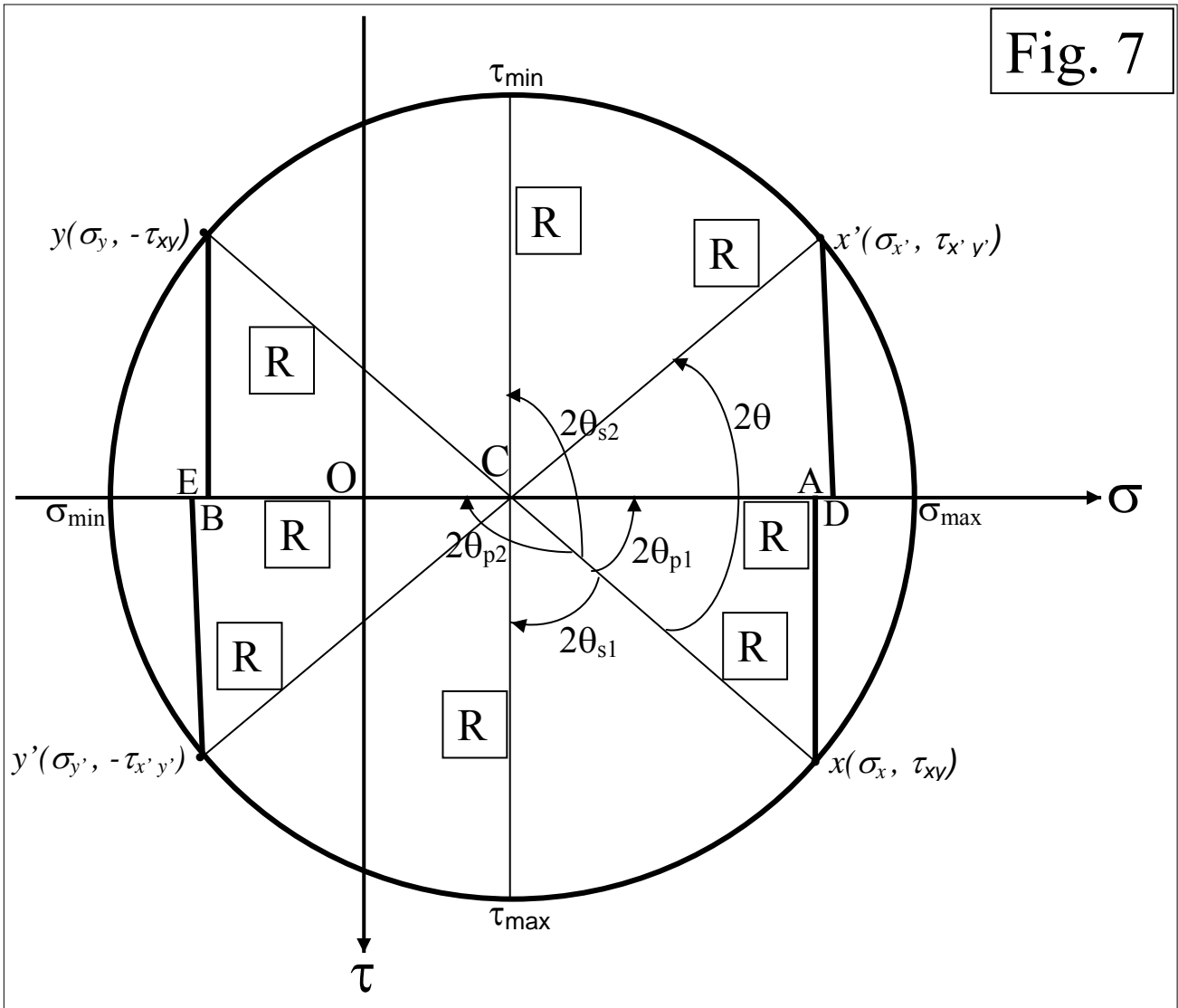
- (1) Draw the σ - τ axes in the x - y (i.e., horizontal-vertical) directions with "appropriate" scale. Note the direction of $+\tau$ (down).
- (2) Put the points x (σ_x, τ_{xy}) and y ($\sigma_y, -\tau_{xy}$) on the figure.
- (3) Connect the two points x and y by a straight line. The point of intersection of the line xy and the σ -axis is the center of the circle C , and Cx & Cy are two radii of such a circle.
- (4) Construct the circle with C as its center and Cx (or Cy) the radius.
- (5) The points of intersection of the circle and the σ -axis are the principal normal stresses; the one to the right is the maximum, and the one to the left is the minimum.
- (6) The radius of the circle is τ_{max} , and $\tau_{min} = -R$.
- (7) The angle measured from the x -axis to σ_{max} gives $2\theta_{p1}$ (or $p2$) (i.e., double the angle), and the angle measured from x to σ_{min} is $2\theta_{p2}$ (or $p1$).
- (8) The angle measured from x to τ_{max} is $2\theta_{s1}$ (or $s2$) and the angle from x to τ_{min} is $2\theta_{s2}$ (or $s1$).
- (9) The similar triangles show in Fig. (7) are used to calculate the required values (stresses and their directions).
- (10) To calculate the stresses on planes oriented θ° from the x -axis on the real plane, go 2θ from the x -axis on the imaginary plane (Mohr's circle), and then draw a straight line passing through C . Use the triangles shown in Fig. (7) to determine the stress values.

Remember:

* **Start from x, Double the angle**

- * Some books use $+\tau$ as up (not down as done here). If it is so, then all angles will be in the **opposite** directions. You can go in the same direction (not the opposite) if one of the following is done:

- (1) Reverse the "sign convention" for shear. \Rightarrow 
- (2) Plot $x(\sigma_x, -\tau_{xy})$, $y(\sigma_y, \tau_{xy})$.
- (3) Plot $+\tau$ axis down (as done here).



$$OC = \frac{OE + OD}{2} = \frac{2 - 6}{2} = -2$$

Using the triangle CxD or CyE, R and $2\theta_p$ can be calculated. \Rightarrow

$$\tan 2\theta_{p1} = \frac{xD}{CD} = \frac{|xD|}{|OD| - |OC|}$$

$$= \frac{3}{6 - 2} = 0.75$$

$$\Rightarrow 2\theta_{p1} = 36.87^\circ \Rightarrow$$

$$\Rightarrow \theta_{p1} = 18.43^\circ \text{ ccw } (\curvearrowright) \text{ measured from the x-axis to the axis of } \sigma_{\min}$$

* Remember: Double the angle measured from x

$$\Rightarrow 2\theta_{p2} = 180^\circ - 2\theta_{p1}$$

$$\Rightarrow \theta_{p2} = 71.57^\circ \text{ CW } (\curvearrowleft) \text{ measured from x to } \sigma_{\max}$$

$$R = Cx = Cy = |xD| / \sin 2\theta_{p1} = 3 / \sin 36.87^\circ = 5$$

$$\sigma_{\max} = OB = CB - |OC| = R - |OC| = 5 - 2 \Rightarrow \underline{\sigma_{\max} = 3 \text{ ksi}}$$

$$\sigma_{\min} = -|OA| = -(|OC| + |CA|) = -(|OC| + R) = -(2 + 5) \Rightarrow \underline{\sigma_{\min} = -7 \text{ ksi}}$$

Take care of the signs by inspection.

$$\tau_{\max} = \pm R \Rightarrow \underline{\tau_{\max} = 5 \text{ ksi}} ; \quad \underline{\tau_{\min} = -5 \text{ ksi}}$$

$$2\theta_{s1} = 90^\circ - 2\theta_{p1} = 90 - 36.87^\circ \Rightarrow \underline{\theta_{s1} = 26.57^\circ \text{ cw } (\curvearrowleft) \text{ measured from x to } \tau_{\min}}$$

$$2\theta_{s2} = 90^\circ + 2\theta_{p1} = 90 + 36.87^\circ \Rightarrow \underline{\theta_{s2} = 63.43^\circ \text{ ccw } (\curvearrowright) \text{ measured from x to } \tau_{\max}}$$

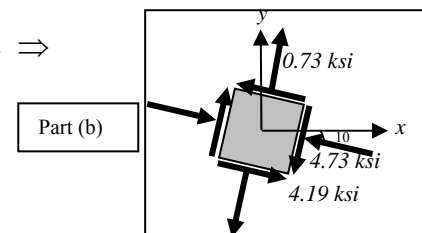
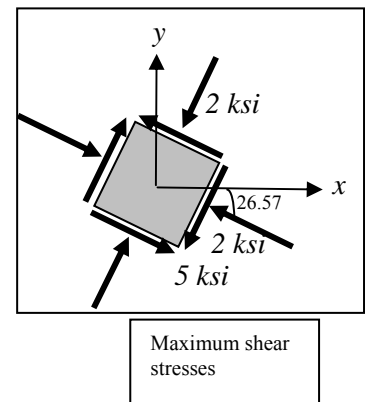
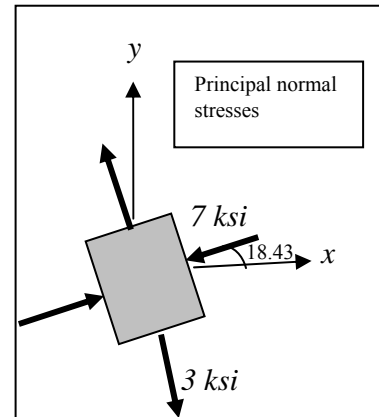
$$b) \sigma_{x'}(-10^\circ) = OF = -(|OC| + |CF|) = -[|OC| + R \cos(2\theta_{p1} + 20^\circ)] = -[2 + 5 \cos(56.87^\circ)] \Rightarrow$$

$$\underline{\sigma_{x'}(-10^\circ) = -4.73 \text{ ksi}}$$

$$\sigma_{y'}(-10^\circ) = OG = R \cos(2\theta_{p1} + 20^\circ) - |OC| = 5 \cos(56.87^\circ) - 2 \Rightarrow$$

$$\underline{\sigma_{y'}(-10^\circ) = 0.73 \text{ ksi}}$$

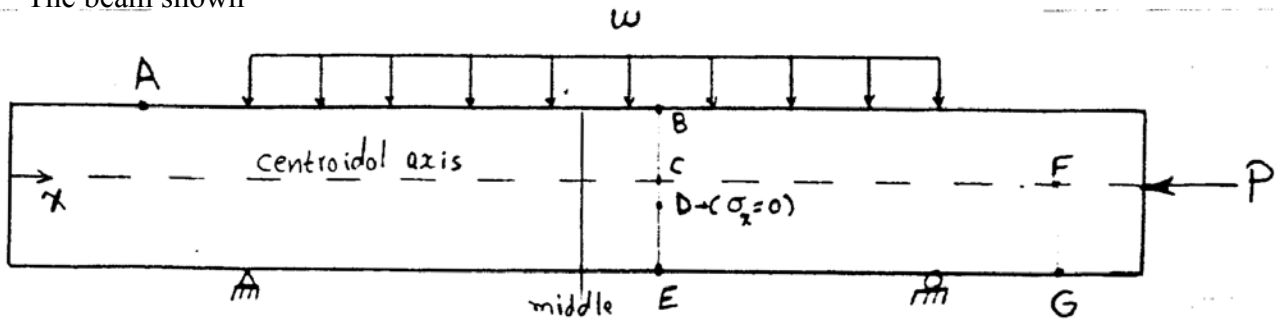
$$\tau_{x'y'} = \pm R \sin(56.87^\circ) \Rightarrow \underline{\tau_{x'y'}(-10^\circ) = \pm 4.19 \text{ ksi}}$$



Example 3:

Given:

The beam shown

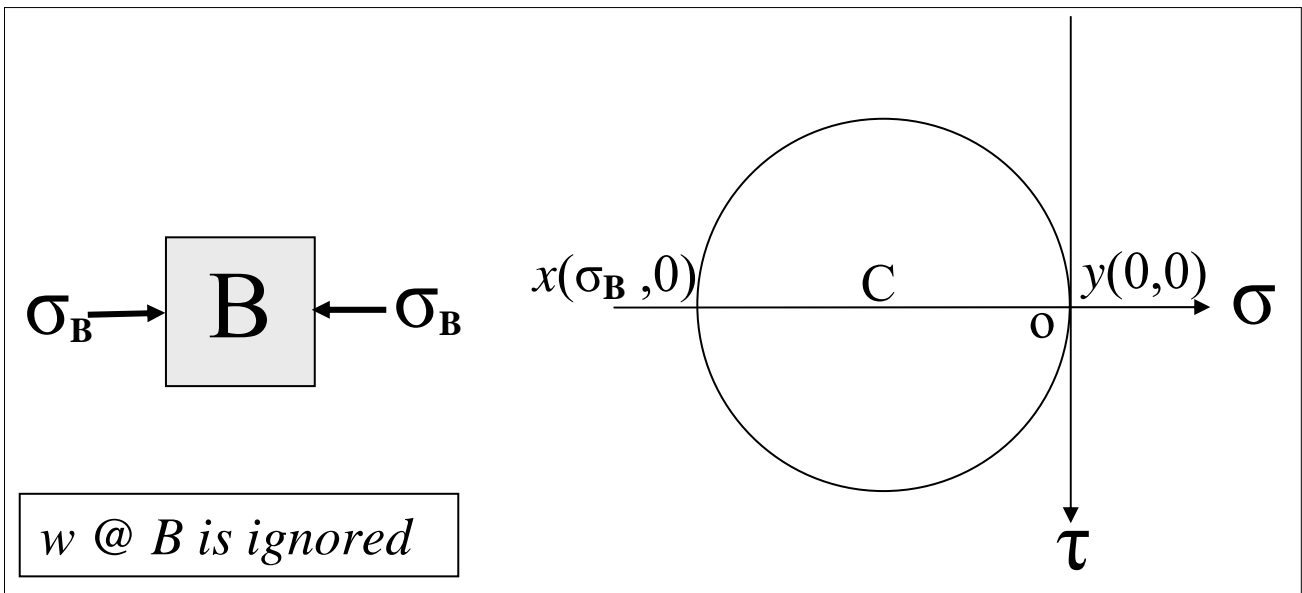
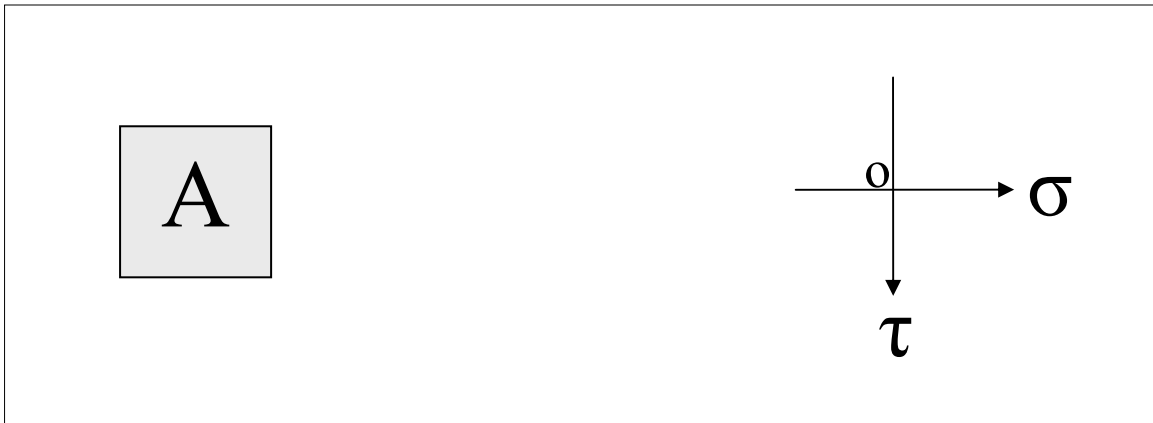


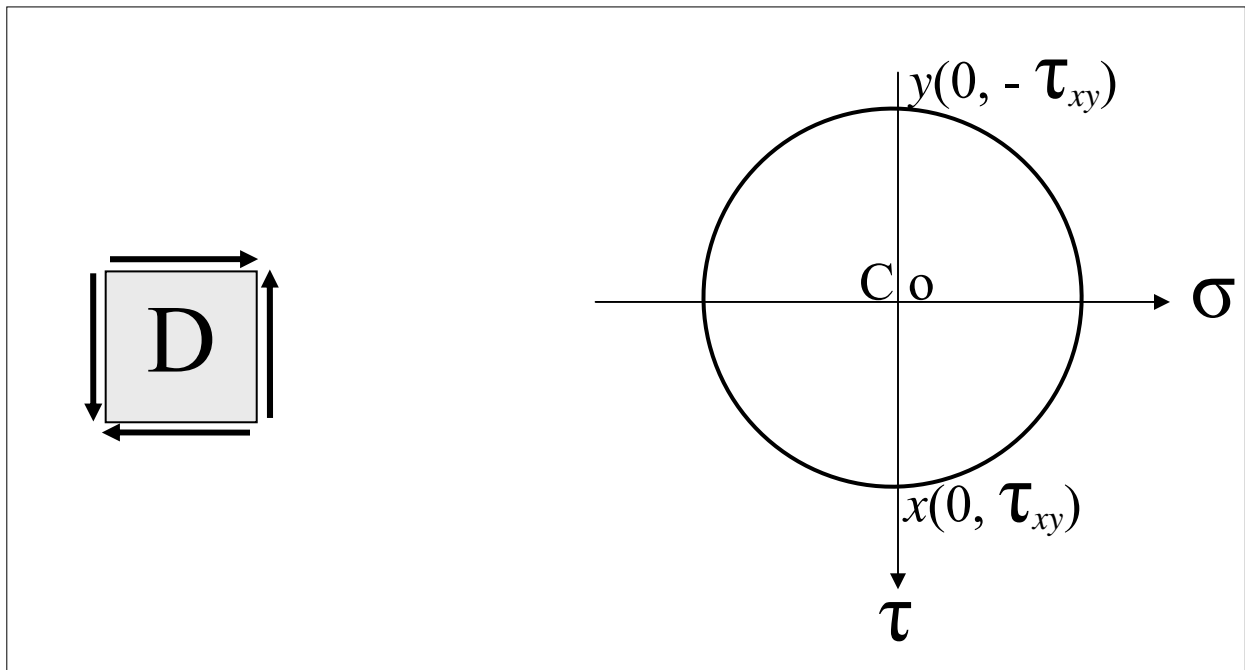
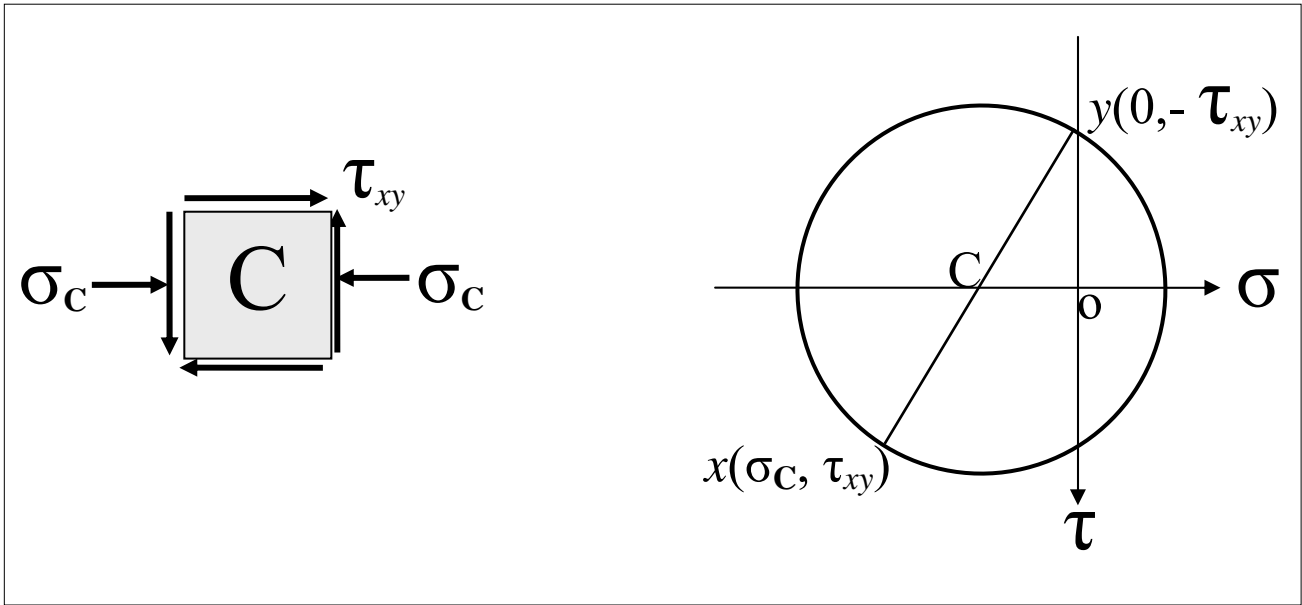
Req'd.:

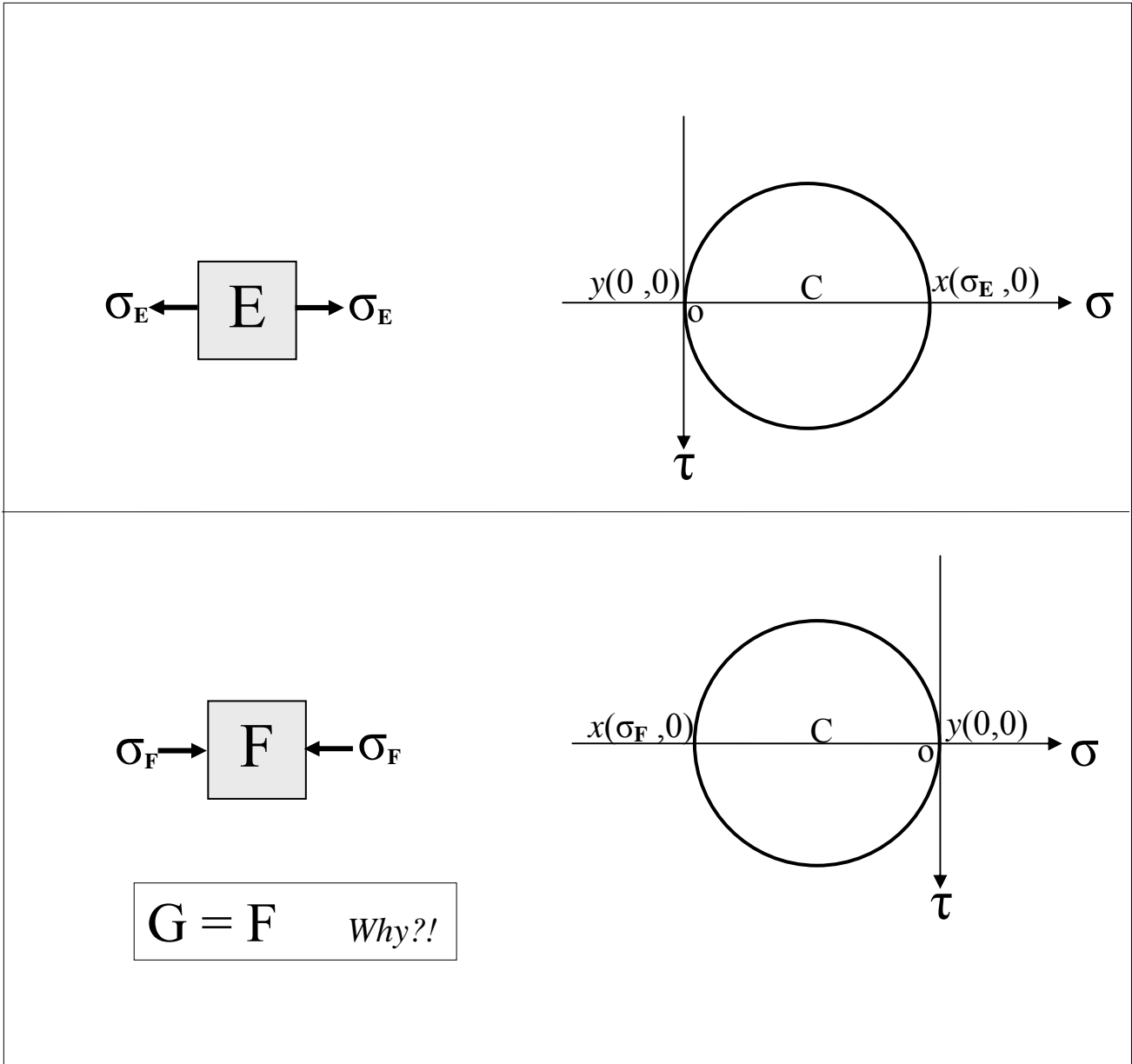
Qualitatively, sketch the **state of stress** and **Mohr's circle** for each of the **points A to G**.

Solution:

Note that σ_y is always assumed **zero** (ignored) in beams.



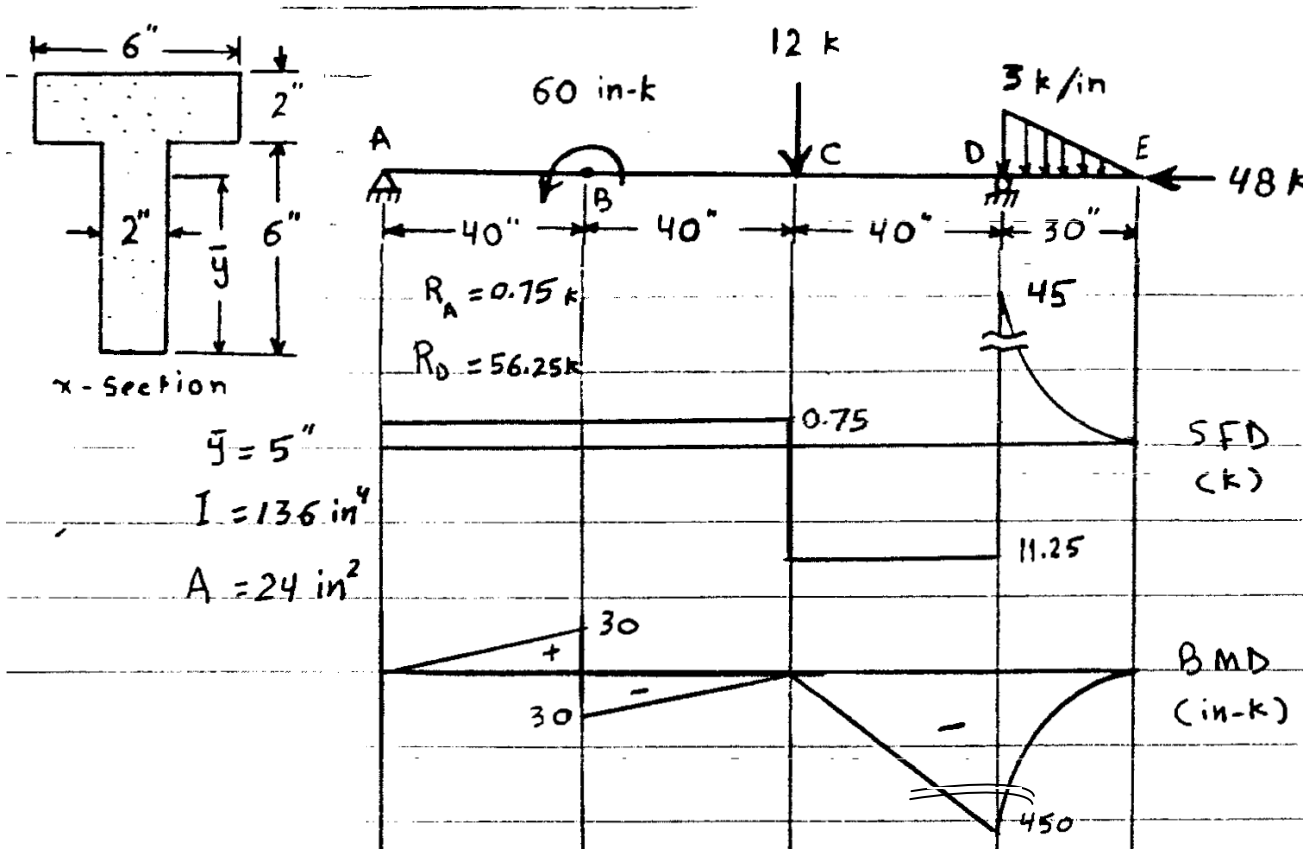




Example 4:

Given:

The beam shown



Req'd.:

The principal normal and shear stresses and their directions at the point(s) of maximum stresses.

Sol'n.:

$$M_{\max} = 450 \text{ in-k} \quad \left(\frac{T}{c} \right) @ D$$

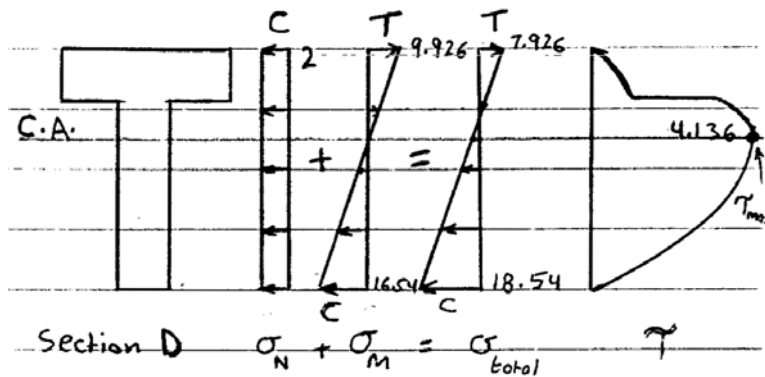
This M will give σ_{\max} (both T & C)

$$V_{\max} = 45 \text{ k} @ D \text{ also}$$

$$\sigma = \sigma_N + \sigma_M = \pm \frac{N}{A} \pm \frac{My}{I}$$

$$\sigma_{\text{top}} = \frac{-48}{24} + \frac{450(3)}{136} = -2 + 9.926$$

$$= 7.926 \text{ ksi (T)}$$



$$\sigma_{\text{bottom}} = -\frac{48}{24} - \frac{450(5)}{136} = -2 - 16.54$$

$$= \mathbf{18.54 \text{ ksi} \quad (C)}$$

$$\sigma_{\text{C.A.}} = \frac{-48}{24} + 0 = 2 \text{ ksi} \quad (C)$$

$$\tau_{\text{top}} = \tau_{\text{bottom}} = 0$$

$$\tau_{\text{C.A.}} = \tau_{\text{max}} = \frac{VQ}{Ib} = 45 (5 \times 2 \times 2.5) / 136(2) = \mathbf{4.136 \text{ ksi}}$$

σ 's above are all σ_x .

$\sigma_y = 0$ at all points (always the case in beam theory)

We need to calculate the principal stresses at 3 points (top, bottom, and N.A. of section D).

\Rightarrow Choose the maximum normal (T & C) and shear stresses.

1) Top of D : (**Mohr's circle** is used for the max/min stress values below, *not shown*)

$$\sigma_x = 7.926 \text{ ksi} \quad , \quad \sigma_y = 0 \quad , \quad \tau_{xy} = 0$$

$$\Rightarrow \sigma_{\text{max}} = 7.926 \text{ ksi} \quad , \quad \sigma_{\text{min}} = 0 \quad , \quad \tau_{\text{max}} = 3.963 \text{ ksi} \quad , \quad \tau_{\text{min}} = -3.963 \text{ ksi}$$

2) Bottom of D: $\sigma_x = -18.54 \text{ ksi} \quad , \quad \sigma_y = 0 \quad , \quad \tau_{xy} = 0$

$$\Rightarrow \sigma_{\text{max}} = 0 \quad , \quad \sigma_{\text{min}} = -18.54 \text{ ksi} \quad , \quad \tau_{\text{max}} = 9.27 \text{ ksi} \quad , \quad \tau_{\text{min}} = -9.27 \text{ ksi}$$

3) Centroidal Axis: $\sigma_x = -2 \text{ ksi} \quad , \quad \sigma_y = 0 \quad , \quad \tau_{xy} = 4.136 \text{ ksi}$

$$\Rightarrow \sigma_{\text{max}} = 3.2 \text{ ksi} \quad , \quad \sigma_{\text{min}} = -5.2 \text{ ksi} \quad , \quad \tau_{\text{max}} = 4.2 \text{ ksi} \quad , \quad \tau_{\text{min}} = -4.2 \text{ ksi} \quad \Rightarrow$$

$\sigma_{\text{max}}^T = \mathbf{7.926 \text{ ksi}}$	 @ D (Top)
$\sigma_{\text{max}}^C = \mathbf{18.54 \text{ ksi}}$	 @ D (Bottom)
$\tau_{\text{max}} = \mathbf{9.27 \text{ ksi}}$	 @ D (Bottom)

* **Important note:** When τ_{xy} is zero at a point, then σ_x and σ_y are themselves principal stresses at that particular point (as seen above).